Wireless World

RADIO AND ELECTRONICS

APRIL 1948

1/6

Vol. LIV. No. 4

IN THIS ISSUE :

SURVEY OF RADIO COMPONENTS

World Radio History

Remember the ROLA G.12?

now it's back - the G12plus

Remember the Rola G.12, most famous of all pre-war 12" speakers? Now, the G.12 is back with all the special features that made it so popular before, *plus* the more powerful Alcomax 11 magnet and *plus* special dustproof suspension completely protecting the coil and magnet gap. Thanks to the new magnet and up-to-the-minute manufacturing techniques Rola are able to offer you in the new G.12 a speaker of even greater sensitivity and tonal brilliance than its predecessor combining more compact design with cleaner lines.

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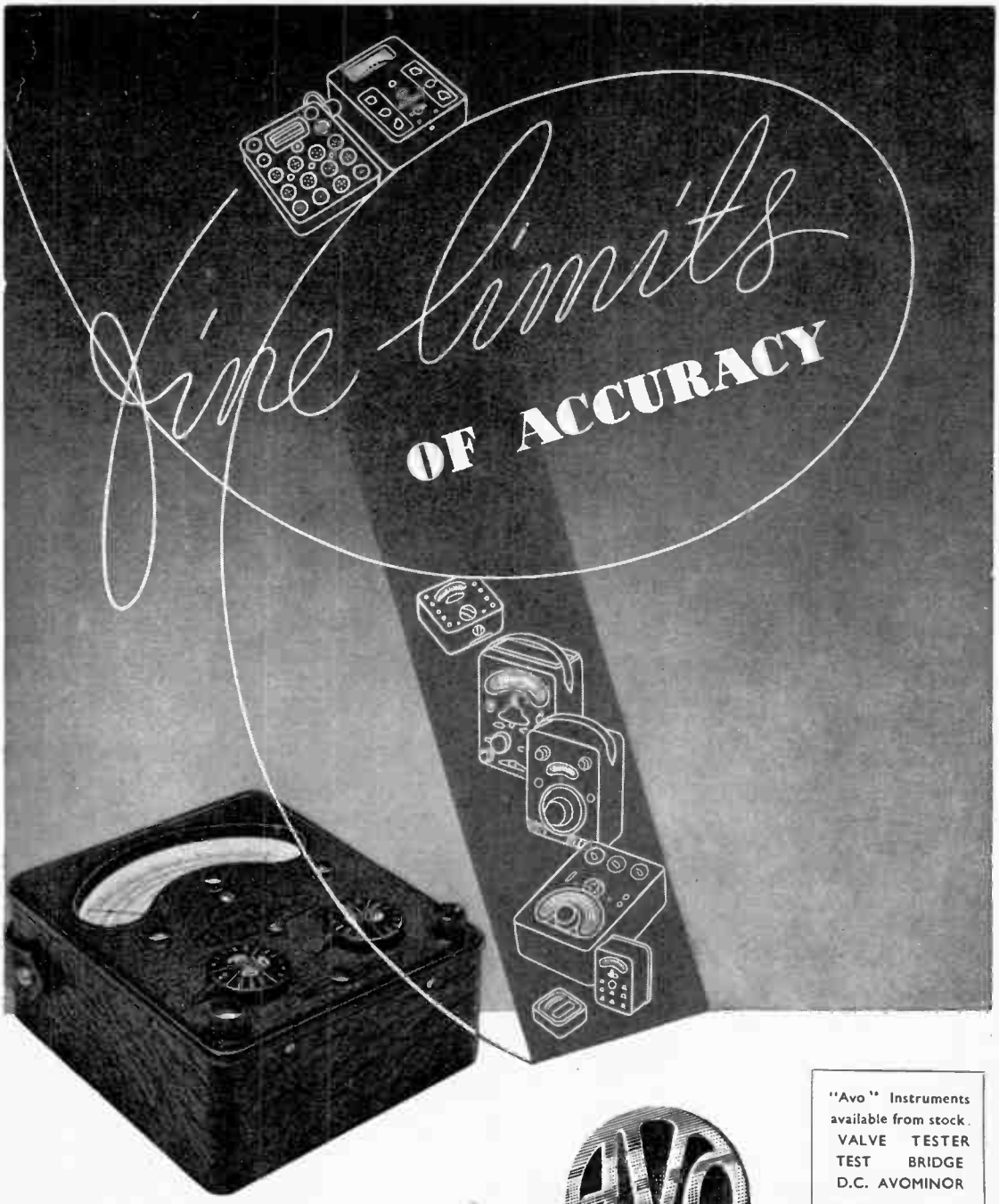

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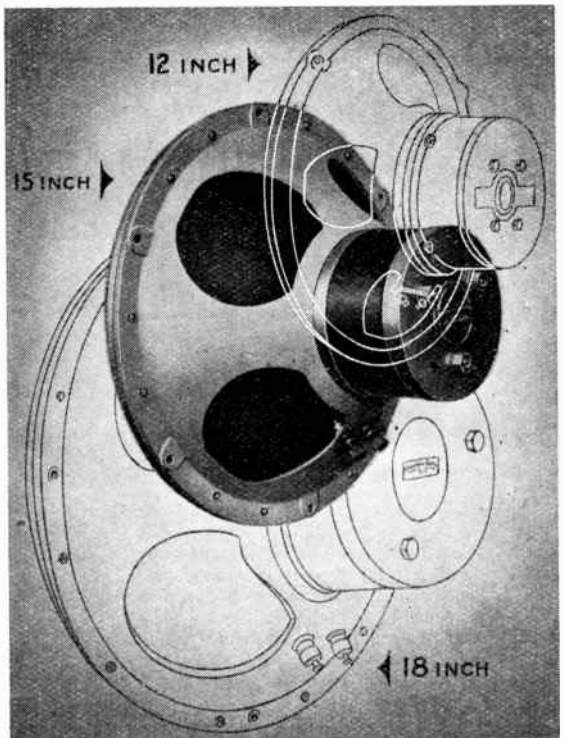

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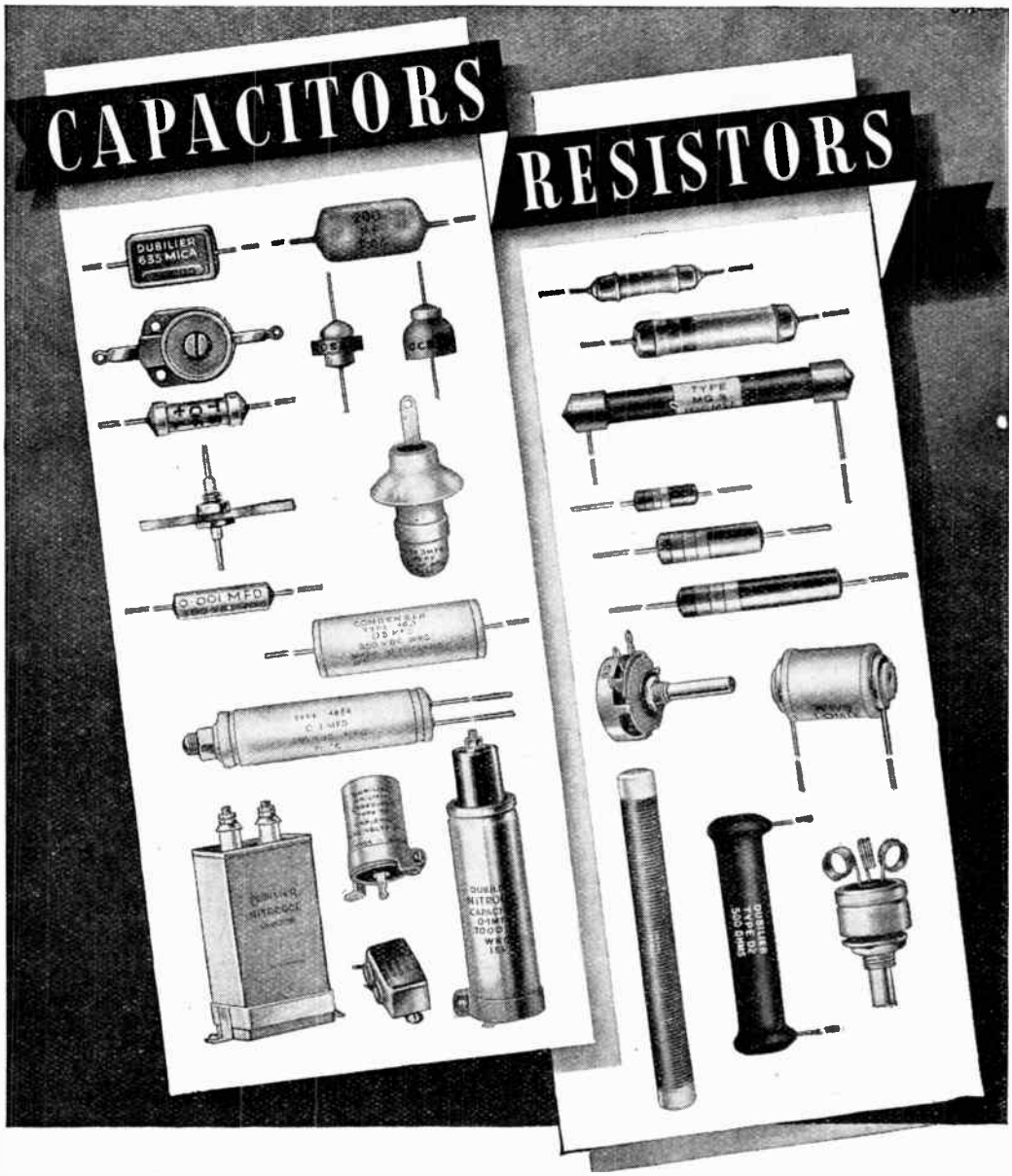

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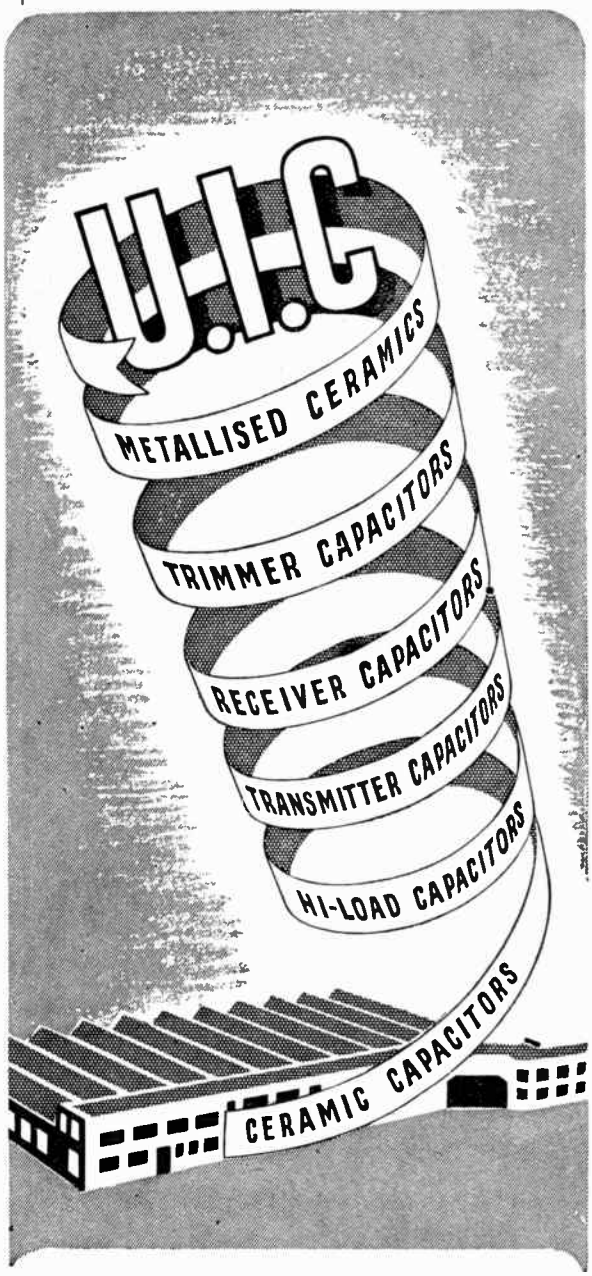

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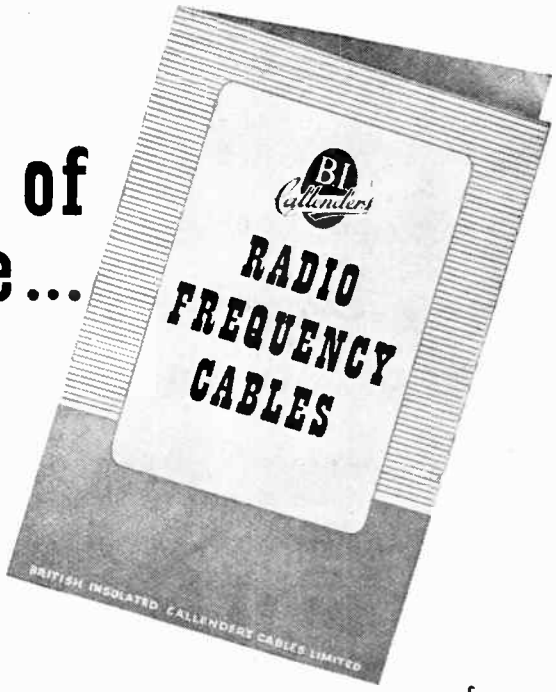
A matter of Balance...



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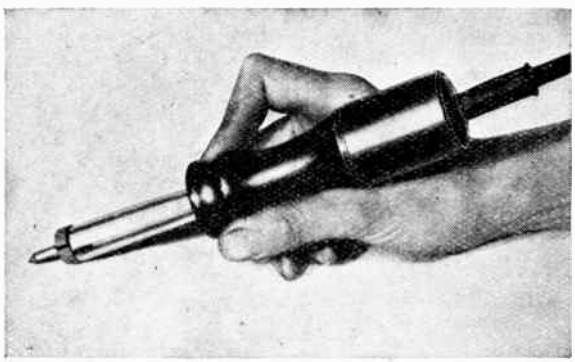

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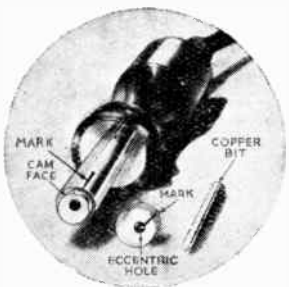

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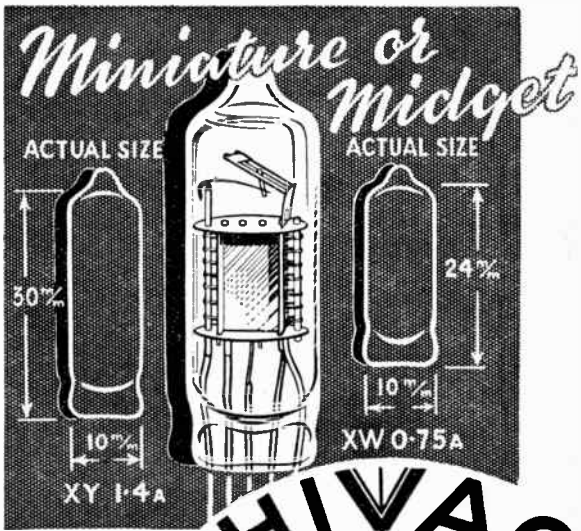

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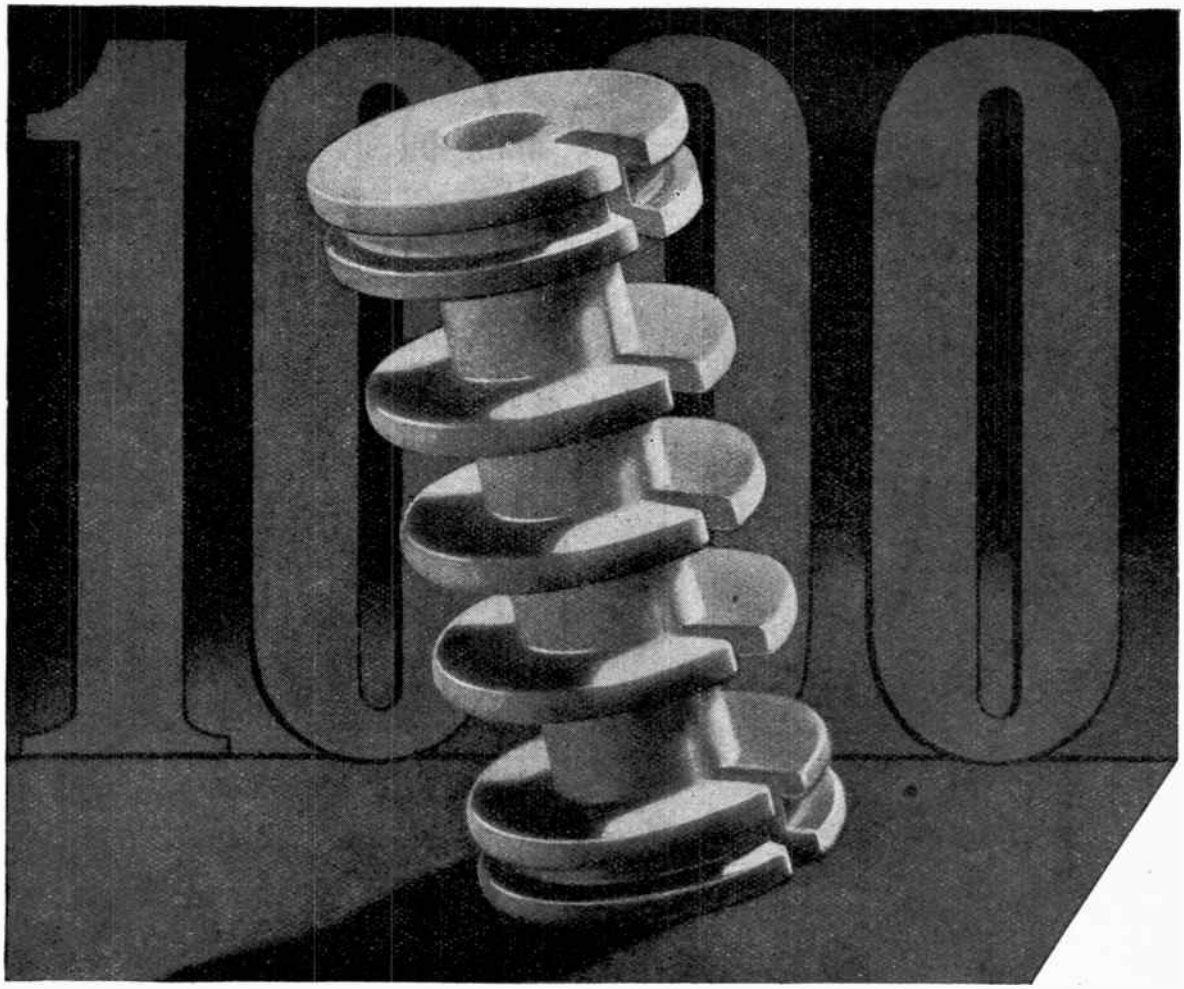

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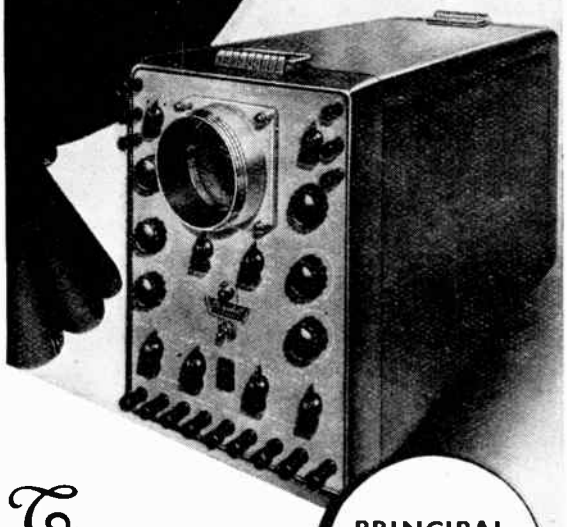
Presenting the New Model D



The Type 1684 series of Oscilloscopes is already well known. The new Model retains the desirable features of this series—d.c. shift controls, response flat to video frequencies, d.c. coupled symmetrical amplifiers on both axes, semi-automatic synchronisation of the time base, etc. It incorporates many new features of design, both electrical and mechanical. One such improvement is that the grids of the input stages of both amplifiers are available at Earth potential enabling the instrument to be used more easily for d.c. measurement.

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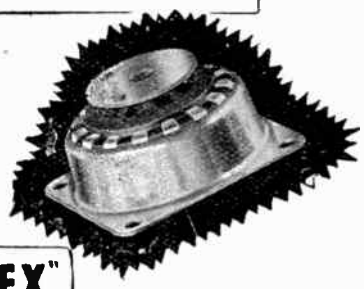

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TECHNICAL TOPICS

for Amplifier designers

● Single, or push-pull circuits.

The simplest output circuit uses a single power valve, and indeed modern valves, particularly pentode and beam tetrodes, are designed to give adequate power as a single unit. With low impedance triodes or indirectly heated pentodes or tetrodes wired as triodes, a push-pull arrangement is usually desirable to minimise 2nd harmonic distortion.

Push-pull circuits are popular in high quality amplifiers because of the increased available power and the tendency to 'balance out' 2nd harmonic distortion. It must be remembered however that the push-pull circuit has the same overall sensitivity as the single valve, that is for double the output, the total grid input must be doubled. The load impedance will vary with conditions of use, whether 'Class A', 'Class B' or 'Class AB', and for all conditions except for 'Class A' (where the grid bias is the same as for a single valve), and the equivalent anode to anode load double, good 'regulation' of the H.T. supply is essential.

Output power for typical valves in single and push-pull arrangements are shown below.

TYPE OF OUTPUT VALVE	Approx. power (watts)	
	Single Valve	Push Pull
KT2 (2 volt)	0.5	1.0
KT76 (DC/AC)	2.0	4.8
KT33C (DC/AC)	5.0	15.5
KT63	3.0	6.0
KT61	4.3	11.5
KT61 (Triode connected)	—	6.0
KT66	7.25	up to 50
KT66 (Triode connected)	5·8	up to 14.5
PX4	4·5	up to 13.5
PX25	8·5	up to 25

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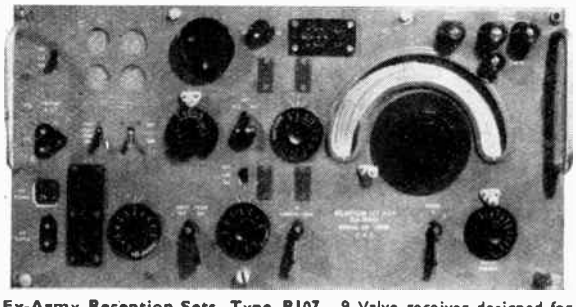

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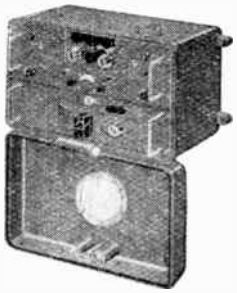

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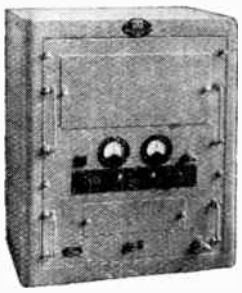

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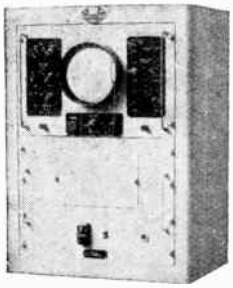

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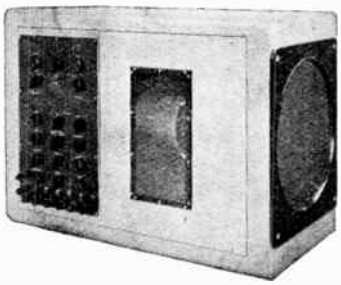

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Demonstrator and student alike will acclaim the features of this equipment — 15" tube with glare removing filter, 2 beam switch for simultaneous delineation of two recurrent wave forms, or their "addition" to produce a single resultant trace. Provision is made for setting up from rear of instrument.

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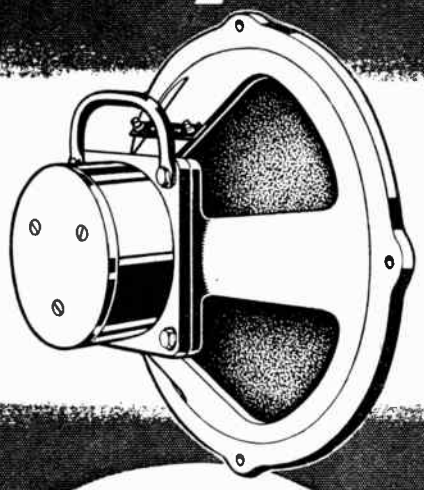

Rigid diecast chassis ; square casting for the magnet seating, secured with large hexagon head bolts ; centre pole and bottom plate all in one forging ; ring-clamped cone ; diecast centring ring ; practical construction matched by excellent response and high sensitivity — all made for Heavy Duty. The Truvox 12" P.M. Speaker will convince your most critical friends that your latest amplifier "has something." Truvox leaflet SH/152 gives all the technical detail — a postcard brings it to you.

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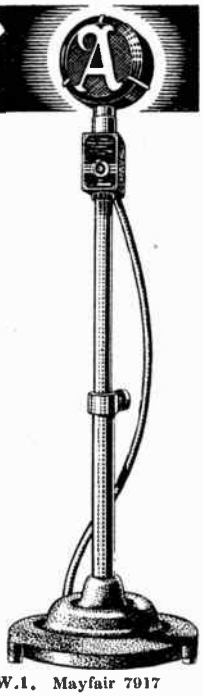

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DEPENDABILITY

SP61*

RATING:

Heater Voltage	6.3
Heater Current (amps)	0.6
Maximum Anode Voltage	250
Maximum Screen Voltage	250
‡*Mutual Conductance (ma/V)*	8.5

‡ *Taken at Va=200: Vs=200: Vg=1.5*

GENERAL:

The SP61 is a high slope screened H.F. Pentode designed for use on A.C. mains in the H.F. and I.F. stages of a Television receiver.
Other uses are:

1. Video amplifier in circuits where the capacity across the output load is low.
2. Frequency changer in conjunction with a separate oscillator valve such as the P61.
3. Certain classes of audio amplification work where gains of over 150 can be realised.

The valve is fully metallised and is fitted with a Mazda octal base.

* *Also made with 4v. heater and known as SP41*

LIST PRICE 10/6 (plus 3/5d. purchase tax)

P61†

RATING:

Heater Voltage	6.3
Heater Current (amps)	0.6
Maximum Anode Voltage	250
§*Mutual Conductance (ma/V)*	8.0
§*Amplification Factor*	17
Maximum Peak Anode Current (mA)	30
Maximum Anode Dissipation (watts)	4.0

§ *Taken at Va=100: Vg=0*

GENERAL:

The P61 is a triode and has been primarily designed for use as an oscillator in television receivers. It may also be used as an oscillator in all-wave receivers where a single valve frequency changer is not employed.
The valve is fully metallised and is fitted with a Mazda octal base.

† *Also made with 4v. heater and known as P41*

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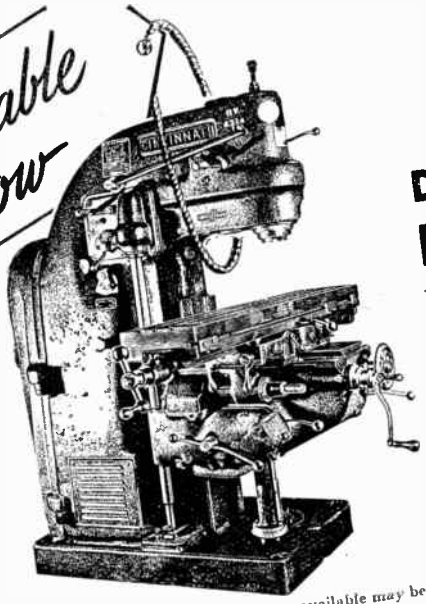

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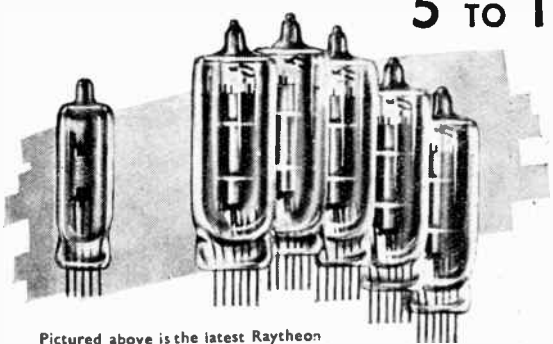
Little valve outlasts big one...

5 TO 1



Pictured above is the latest Raytheon Flat Hearing Aid Valve . . . the CK512AX . . . and a group of the earliest Raytheon Hearing Aid valves.

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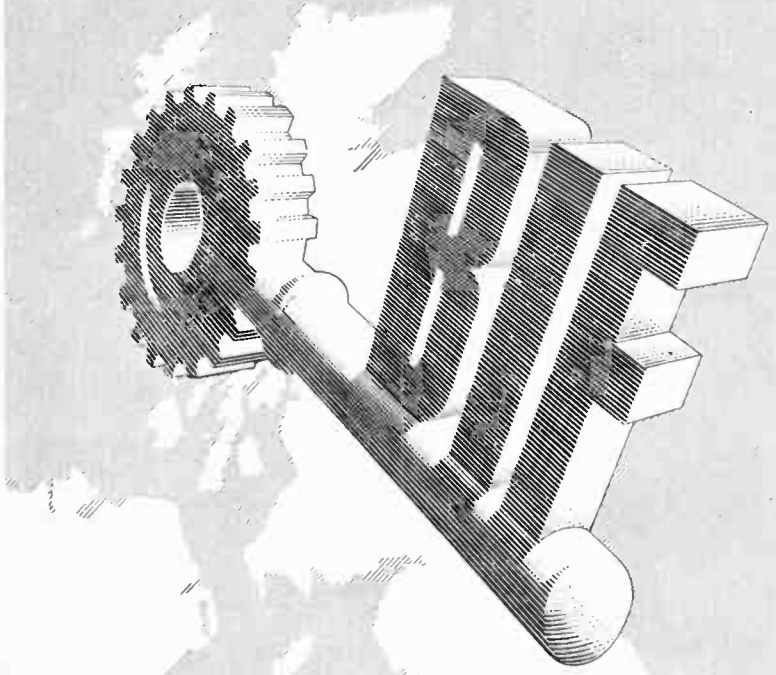

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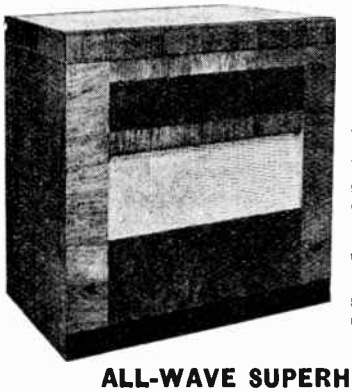

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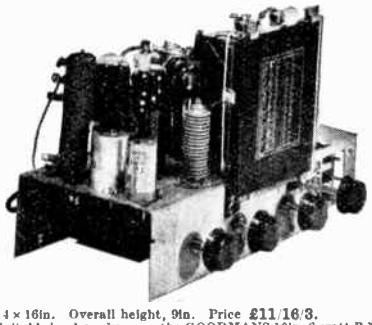

A Kit of Parts to build a 6-valve (plus rectifier) receiver, covering 16-50 metres. Medium and Long-wave bands. Valve line-up 6K8, 6K7, 6Q7, 6J7, two 25A6 in push-pull. Metal Rectifiers are incorporated for H.T. supply. Output impedance is for 3 and 15 ohms. The latest Wearite Coil Pack incorporating Iron Dust Coils is used, making construction and alignment extremely simple. A pick-up position on the wavechange switch and pick-up terminals is provided. A complete kit including valves but without speaker or cabinet. Chassis size 14 × 16in. Overall height, 9in. Price £11/16/3.
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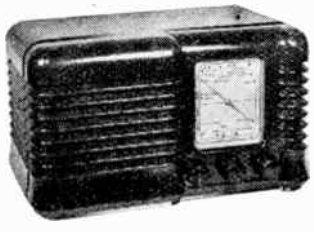

Build your own midget radio. A complete set of parts, including valves, loudspeaker and instructions. In fact, everything except cabinet necessary to build 4-valve Medium and Long Wave T.R.F. radio operating on 200-250 v. A/C-D/C or A/C only. Please state which is required. Wavelengths covered 200-557 and 700-2,000. Size 10 × 6 × 6in. Completely drilled chassis. Price, including tax, £8/0/11.
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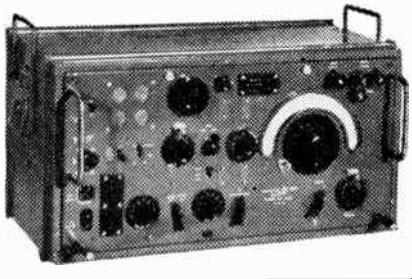

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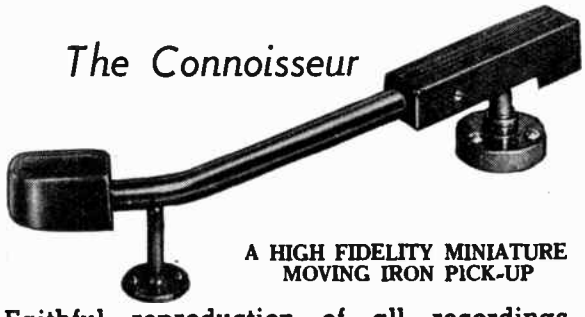

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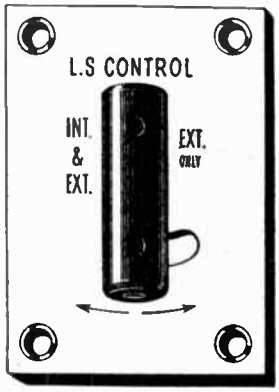

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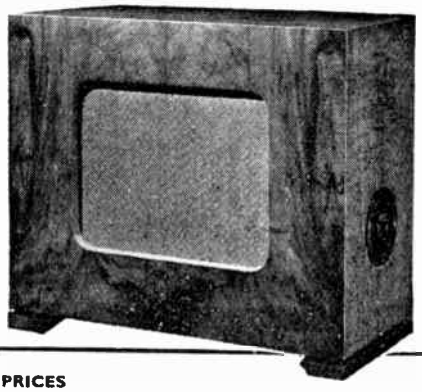

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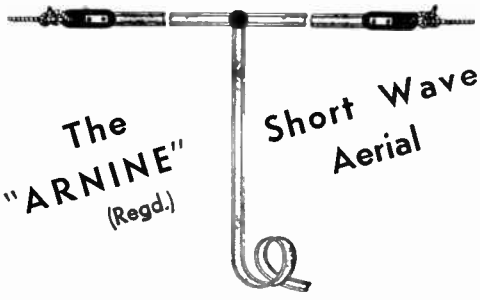

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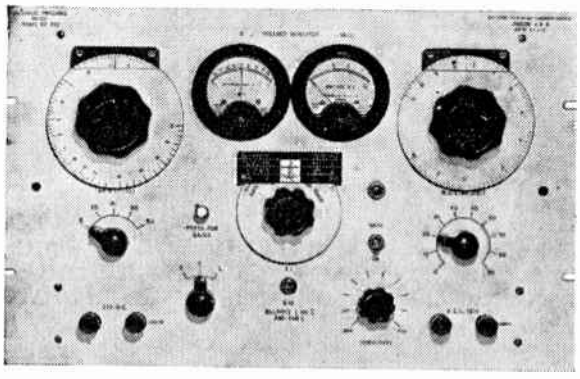

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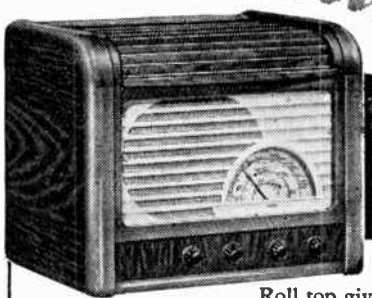

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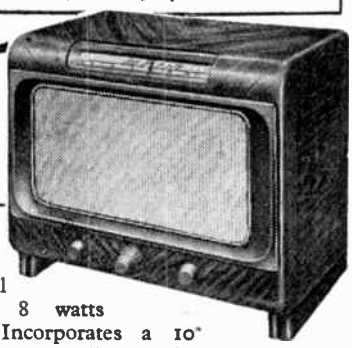
SOBELL MODEL 717 7-VALVE RECEIVER



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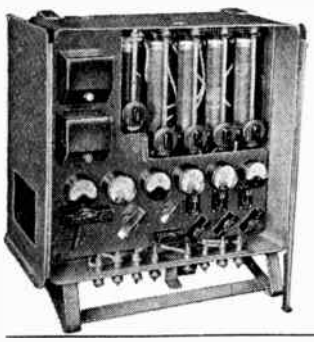

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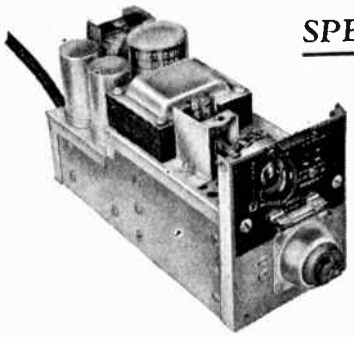
Control Panels Only as illustrated

24 v., 1,260 watts. Includes five 1½in. moving coil ammeters (1, 0-40 a., 4, 0-15 a.). One moving coil voltmeter 0-40 v. Five heavy duty sliding resistances, etc., complete in metal case as shown with fold-back doors. Size, 18 × 17 × 8½ins. Offered at less than half the component value. Price, carr. 12/6 extra **£4.19.6**



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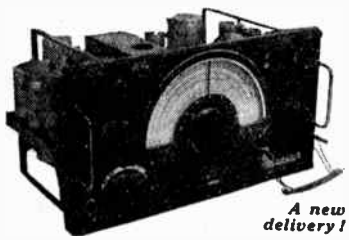
Complete with Vibrator

Output approx 200 v., 60 ma. Size 9 × 5 × 3½in. A first-class job. Price **£1.17.6**

VIBRATORS

2-v. input. Self-rectifying type. Output approx. 200 v., 60 ma. Price **7/6**

10-VALVE COMMUNICATION RECEIVER—Type R1155



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These sets are as new. Need only a power pack for immediate use (see "W.W." July, 1946). Freq. range 7.5 mc/s 75 kc/s in five wavebands. Complete with 10 valves including magic eye. Enclosed in metal case. Every receiver is aerial tested. Set only **£12.10.0**

Complete with Power Pack and Loudspeaker, for A.C. mains 200-250 v. ..... **£20** (Carr. and pkg. 10/6 extra.)

FREE with each receiver! Complete circuit, description and modifications for civil use, reprinted from "W.W." July, 1946.

Please Note: All carriage charges relate to the British Isles only • We do not issue lists or catalogues.

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Closed Thur: 1 p.m. Open all day Sat. and weekdays 9 a.m.—6 p.m.

LOWEST EVER attenuation & capacitance

CO-AX CABLES *for RADIO FREQUENCIES*

LOW ATTEN. TYPES	IMPED. OHMS.	ATTEN. db/100ft. at 100 Mc/s.	LOADING K/M	O.D.
A1	74	1.7	0.11	0.36"
A2	74	1.3	0.24	0.44"
† A34	73	0.6	1.5	0.88"

LOW CAPAC. TYPES	CAPAC. mmf/ft.	IMPED OHMS.	ATTEN. db/100ft 100 Mc/s.	O.D.
C 1	7.3	150	2.5	0.36"
★ PC 1	10.2	132	3.1	0.36"
C 11	6.3	173	3.2	0.36"
C 2	6.3	171	2.15	0.44"
C 22	5.5	184	2.8	0.44"
C 3	5.4	197	1.9	0.64"
C 33	4.8	220	2.4	0.64"
C 44	4.1	252	2.1	1.03"

† *Bending Radius 5"*
★ *Photocell Cable.*

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"Cyldon"

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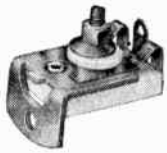
Type No. 19



Type No. 22

SYDNEY S. BIRD & *Sons, Ltd.*

CAMBRIDGE ARTERIAL ROAD, ENFIELD. MIDDX.

'Phone: Enfield 2071-2 'Grams: Capacity, Enfield.

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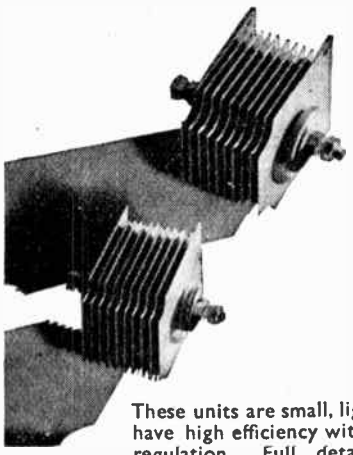

RECTIFIERS for AC/DC RECEIVERS

These units are small, light and have high efficiency with good regulation. Full details are given in publication M.R.14 Suppt. 1, a copy of which may be obtained from Dept. W.W.

Type	Normal Output		Max. Input Volts AC/DC	Reservoir condenser		Circuit	Dimensions			Approx Weight Ozs.
	Volts	mA		mFd.	Wkg. Volts		Ht.	Wdth	Lgth.	
HT.46* 4A79	240	120	250	16	350	Half-wave	2½"	2¼"	4⅜"	8¾
HT.47* 14A46	260	60	250	16	350	Half-wave	2½"	2¼"	3⅝"	6¼
HT.48* 15B46	260	30	250	8	350	Half-wave	1 15/16"	1¾"	3 3/16"	3¾

* Units available to bona-fide manufacturers, who should ask for Data Sheet 49

WESTINGHOUSE BRAKE & SIGNAL CO. LTD., 82, York Way, King's Cross, London, N.1

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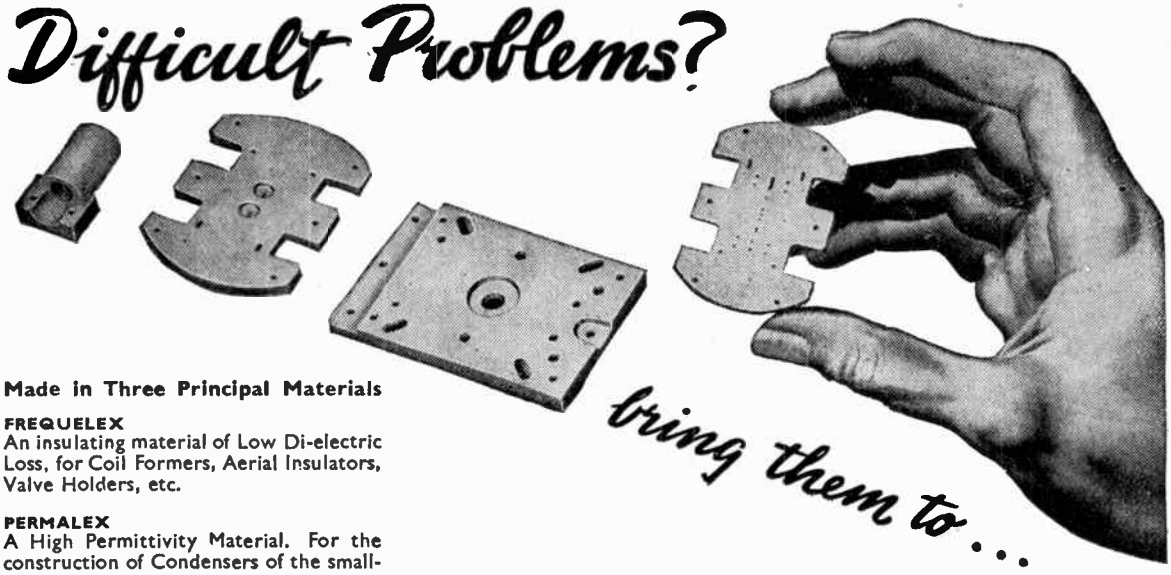

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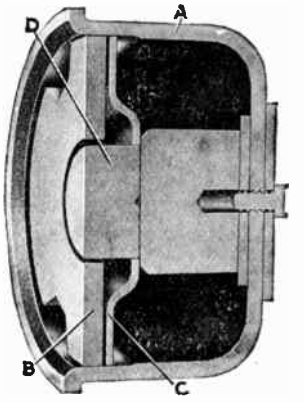
R&A



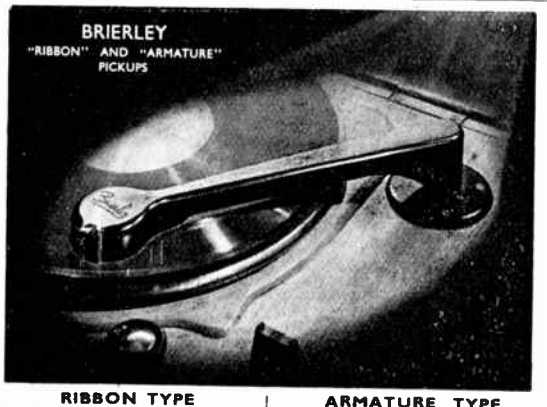
'Co-axial Construction . . .'

THE magnet assembly of the "700" Series is unique in design, enabling approximately 25% more of the available energy in a given weight of magnet to be usefully employed in the gap. Assemblies of from 7,000 to 10,000 Gauss may be obtained with magnets of different height and weights.

The main body of assembly "A" is machined in the bore and on the outside diameter to limits of ± .00075". The outer pole "B" has its bore and outside diameter machined simultaneously to limits of ± .0005" as are also the outside diameter and bore of the centre pole centralising member "C", whilst the inner pole "D" is produced from precision ground bar of the same tolerances.

Whilst the assembly of this unit is extremely simple, it will be obvious that by virtue of the design and the limits on diameters to which each part is held, the inner and outer poles must be concentric within extremely close limits and, further, cannot be displaced from their relative positions by shock.

Reproducers & Amplifiers Ltd., Wolverhampton



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Fixed point pressure of ½ oz. Output Voltage 10 to 15 mV. Price in U.K. including special Mumetal screened transformer and Purchase Tax. £10 2s. 4d.

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Fixed point pressure of ¼ oz. Output voltage, ½ to 1v. Price in U.K. including special Mumetal screened transformer and Purchase Tax. £8 15s. 9d.

The Ribbon Pickup now being produced has a new *unbreakable ribbon*. Whilst the mass has been reduced, the effective damping has been increased without increasing the point stiffness. This feature in conjunction with a modified magnetic circuit has resulted in an increased output and an audibly better response at high frequencies putting this pickup even further ahead of any type hitherto available.

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Our new Laboratory Power Supplies, Series 101, are based on our well-known Model 101-A, but incorporate a number of improvements and refinements.

DETAILS ON REQUEST.

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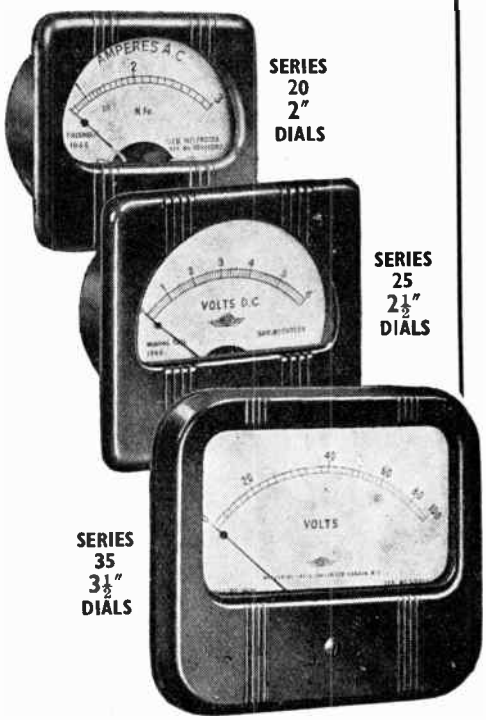

SERIES 20 2″ DIALS

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We can give early delivery—write for details.

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MINIATURE INSTRUMENTS

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AUTOMATIC COIL WINDING MACHINE

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This machine is the most modern on the market and it possesses many exclusive refinements including :

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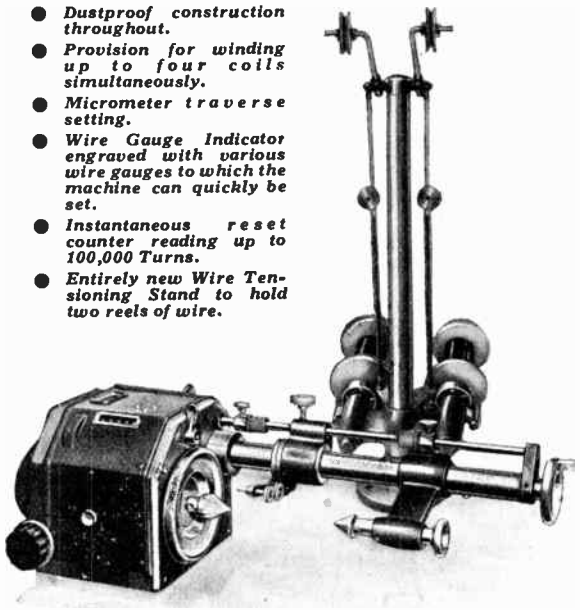
- ***Wire Gauge Indicator engraved with various wire gauges to which the machine can quickly be set.***
- ***Instantaneous reset counter reading up to 100,000 Turns.***
- ***Entirely new Wire Tensioning Stand to hold two reels of wire.***



We will be pleased to send you an illustrated leaflet giving a full technical specification, on request.

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BIMETALS

A COMPLETE RANGE NOW AVAILABLE TO MEET ALL REQUIREMENTS

PHYSICAL CHARACTERISTICS OF AVAILABLE TYPES

TYPE	COMPOSITION		Deflection Constant* per °C. (d)	Resistivity michrohms/cm. cube at 20°C.	Maximum Working Tem. °C.
	Low Expansion % Ni	High Expansion % Ni			
BIMETAL 140	38	20	14.0×10^{-6}	75	300
BIMETAL 160	36	20	$15.6 \times$ „	78	250
BIMETAL 400	42	20	$11.0 \times$ „	70	400
BIMETAL 15	36	100	$9.7 \times$ „	15	200

* The deflection constant (d) is defined as the deflection of a strip of unit length and unit thickness for each °C. rise in temperature over the linear part of the deflection curve.

Further details on application.

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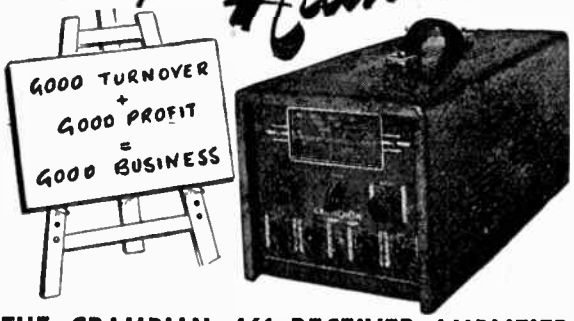
Simple Arithmetic



THE GRAMPIAN 461 RECEIVER AMPLIFIER

This new high-grade reproducer has been specially designed for use in Small Factories, Hotels, Clubs, Swimming Pools, Municipal Buildings, etc., where it is desired to broadcast Radio or Gramophone Records and provide amplification of speech by use of a microphone. Let us send you further details.

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All articles are new and guaranteed and are of well-known manufacture.

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Mains Transformers :
280-0-280 v. 6.3 v. 3 amp., 5.0 v. 2 amp. 20/–
60 m/a Chokes, 400 ohms. 5/6
465 Kc. I.F.'s, iron dust cored, permeability tuned, 1½in. × 1½in. can ... ... pr. 15/6
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7 m/cs I.F.'s ... ... pr. 5/–
GRAMOPHONE AMPLIFIER KITS, 4 watts output, including 2nd detector and A.V.C. components. All parts mounted. Complete with circuit. A.C. £3
Gramophone Amplifier Kits as above, AC/DC... ... ... £3

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.1 × .1 × .1 Condensers, 250 v. ... ... doz. 9/–
Octal Valveholders ... ... 4½d.
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32 mfd. 275 v. 3/9
5in. P.M. Speakers 12/6
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2¾in. Drums 1/–
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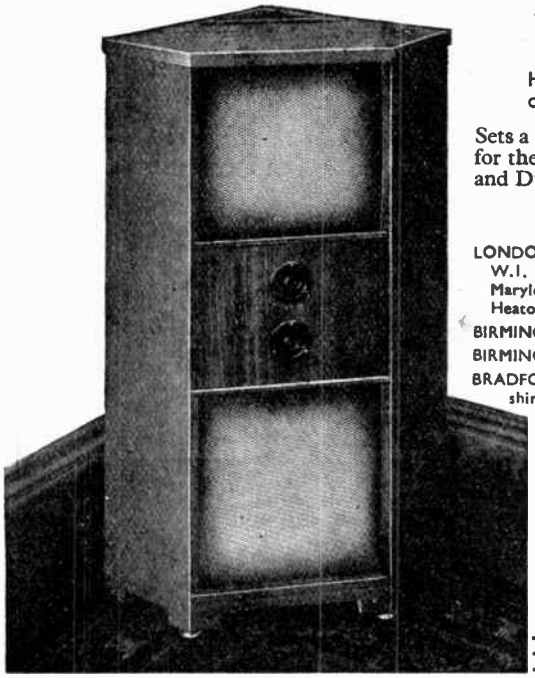
Wharfedale



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With Bass and Treble Reflex Chambers

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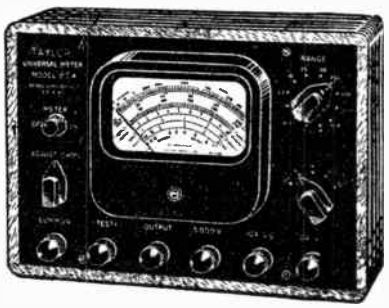

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Grams & Cables "TAYLINS" SLOUGH

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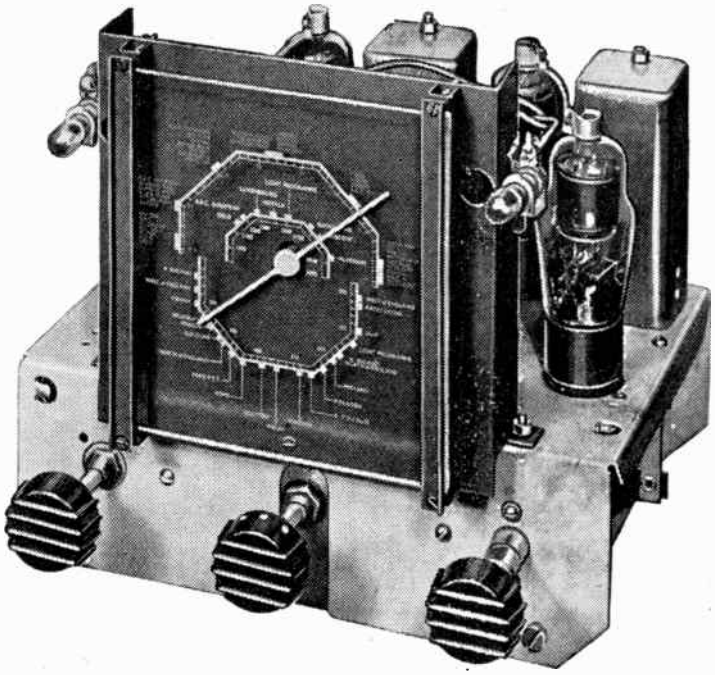
RM Radio Feeder 483



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Send for full particulars.

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Although priced to meet the more slender purse, the new U/48 Crystal Pick-up is an instrument designed to give high quality reproduction, since it embodies many features found in the more expensive models which include

- **Extremely light weight. No record wear.**
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- **Cartridge specially treated to withstand extreme humidity.**
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A twin unit loudspeaker of outstanding merit, incorporating a 12in. unit for bass reproduction and a moving coil pressure unit with Duralumin alloy diaphragm for higher frequencies. An electrical dividing network ensures correct distribution of the frequency spectrum between the two units. PRICE... £42 0 0

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Cabinet incorporates ingenious internal design giving equivalent of a five-foot folded pipe. Wide-response bass down to 35 c/s with good middle and top definition. PRICE £19 10 0

SOUND SALES "PHASE INVERTER SPEAKER."
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ACOUSTICAL AMPLIFIER "QA/12/P."
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All "Sound Sales" domestic reproducing equipment normally in stock.

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A standard of comparison for moving coil units. Excellent mechanical and electrical design. PRICE, with input transformer £7 13 4

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Incorporates ingenious semi-automatic insertion and rejection of special sapphire needles. PRICE £7 6 9

LEXINGTON "JUNIOR" MOVING COIL PICK-UP.
For standard miniature needles. PRICE £4 12 4
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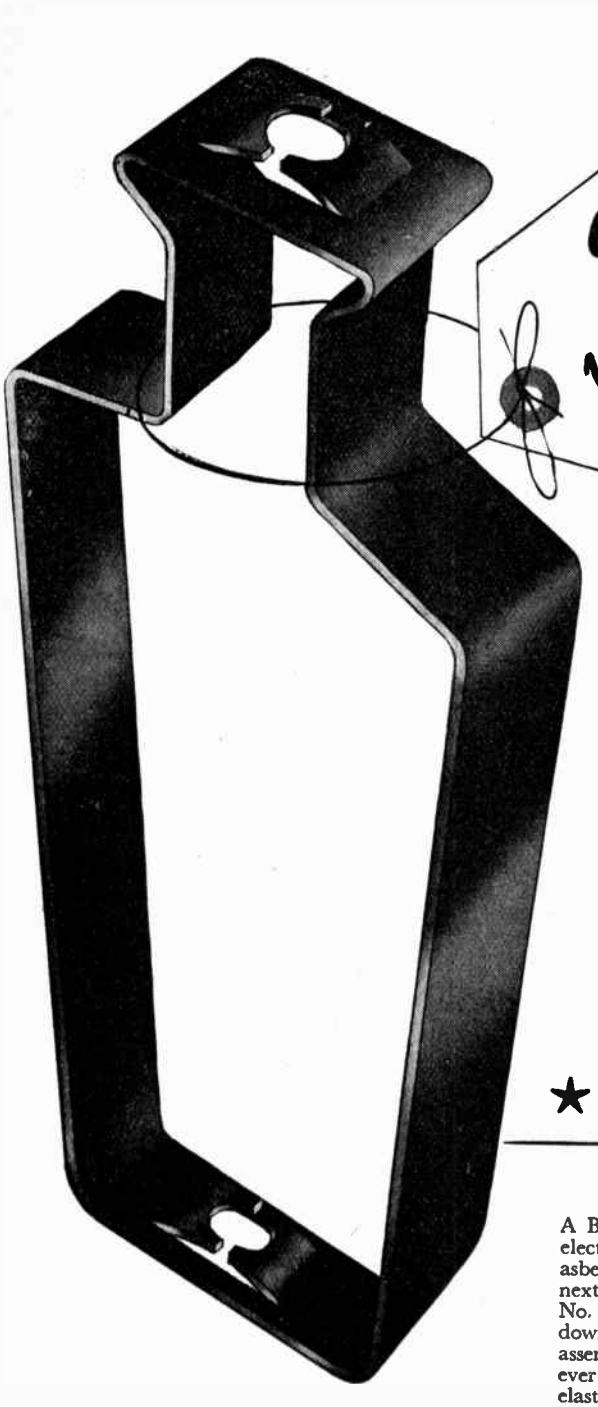

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RADIO AND ELECTRONICS

APRIL 1948

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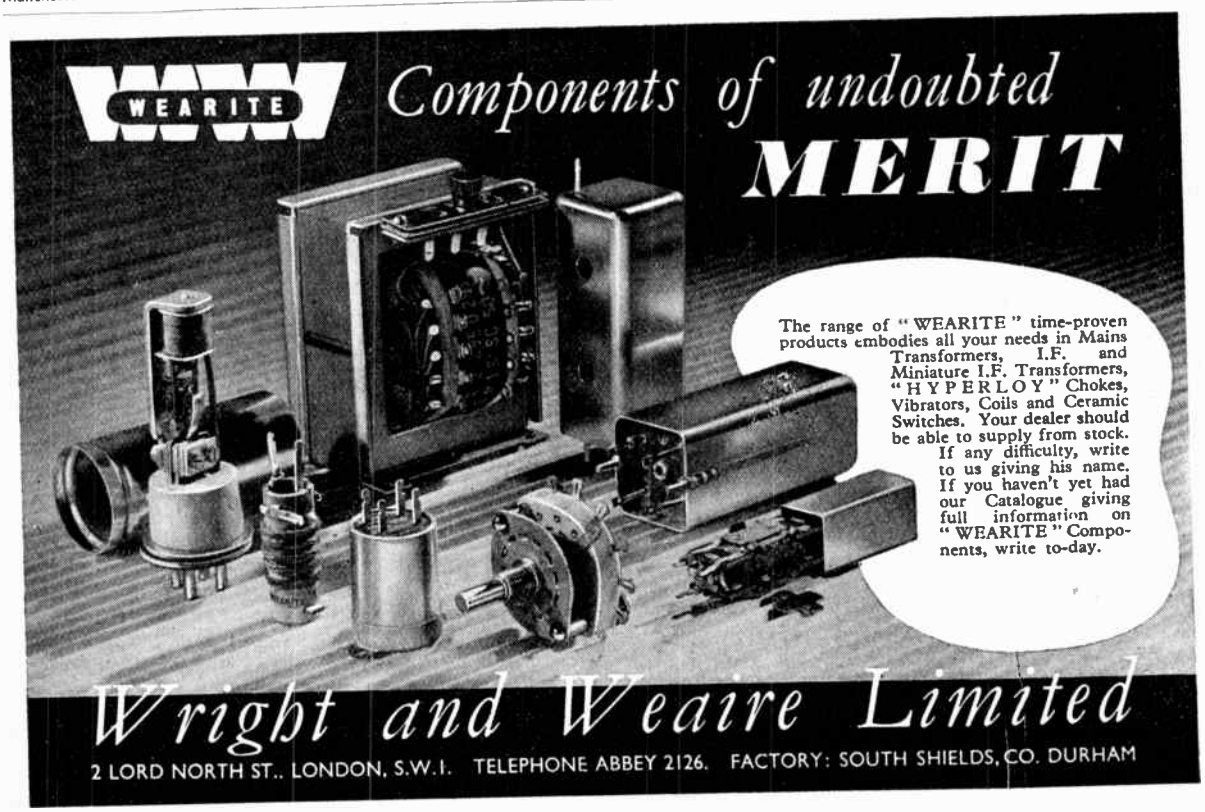
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VALVES AND THEIR APPLICATIONS

By M. G. SCROGGIE, B.Sc., M.I.E.E.

No. 16: Mullard System of Type Nomenclature for Transmitting Valves

THE system of Mullard valve nomenclature explained last month is designed for receiving valves. For transmitting valves, the information one wants to know first is not quite the same. For example, the type of base is rather a detail when the valve itself is a comparatively substantial item. Moreover, transmitter bases are not so distinctly classified as receiver bases; often they are just clamps to hold the valve in position. So they are not specified in the symbols. Nor are filament voltages and currents, for they too are more or less unstandardized. On the other hand, the general *type* of cathode is important; and the anode voltage and output power even more so.

The form in which the output power is best specified depends to some extent on the class of valve. ("Transmitting" valves, by the way, include rectifiers, and of course valves used for purposes other than transmitting, such as audio amplification and R.F. heating). The limiting factor for rectifiers is most suitably expressed as the maximum rectified *current*. Most power valves are limited primarily by the maximum wattage that can be dissipated by the anode. As this is not so with large water-cooled valves dissipating over 5kW, they form a separate class in which the power specified is the output power.

The form of nomenclature used for receiving valves (consisting of two—or possibly three—letters followed by two or more figures) is retained, with appropriately different meanings :

FIRST LETTER: General Class of Valve.

M	L.F. power amplifier or modulator triode.	*These are easy. If "Q" looks queer for "tetrode", remember that "triode" has first claim to "T", and "Quatre" is French for 4.*
P	R.F. power pentode.	
Q	R.F. power tetrode.	
R	Rectifier.	
T	R.F. power triode.	

SECOND LETTER: Type of Cathode.

- G Oxide-coated filament in mercury-vapour rectifier.
- V Indirectly-heated oxide-coated cathode.
- X Directly-heated pure tungsten filament.
- Y Directly-heated thoriated tungsten filament.
- Z Directly-heated oxide-coated filament (except in mercury-vapour rectifiers).

THIRD LETTER: "S" indicates Silica Envelope.

FIRST NUMBER: Anode Voltage in Kilovolts.

E.g.: 05 means 0.5 kV=500V.
1 means 1 kV=1,000 V.
5 means 5 kV.=5,000 V.
12 means 12 kV=12,000 V. and so on.

SECOND NUMBER: Output.

(*a*) For valves up to 5 kW anode dissipation, the figures indicate the maximum permissible anode dissipation in watts.

(*b*) For water-cooled valves over 5 kW dissipation, the figures indicate the maximum output in kilowatts.

(*c*) For rectifiers, the figures indicate the maximum permissible rectified current per valve in milliamps.

Note :—A further letter, A or W, may follow the valve type number, to indicate whether the valve is forced air cooled or water cooled.

Examples :—

QV04–7 R.F. power tetrode with indirectly-heated oxide-coated cathode. Anode rated to work at 400 V and dissipate 7 watts continuously.

TX12–20W R.F. power triode, water-cooled, with tungsten filament. Anode rated to work at 12,000 V, for an output of 20 kW.

RG3–250 Mercury-vapour rectifier with a rated anode voltage of 3,000, giving a maximum rectified output of 250 mA.

There are one or two exceptional valves for which the code has had to be modified, but normally it holds good.

Mullard

This is the sixteenth of a series written by M. G. Scroggie, B.Sc., M.I.E.E., the well-known Consulting Radio Engineer. Reprints for schools and technical colleges may be obtained free of charge from the address below. Technical Data Sheets on all types of valves are also available.

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(M.V.M. 59)

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Wireless World

RADIO AND ELECTRONICS

Vol. LIV. No. 4 — April 1948

Components for Export

THE vigour and flexibility of the components section of the British radio industry was well exemplified at the recent London exhibition organized by the Radio Component Manufacturers' Federation: the show is reported at some length elsewhere in this issue. By common consent, it was by far the best, both in diversity and interest of exhibits, as well as in detail organization, that has yet been staged. It must have convinced the foreign buyer—who appeared to be represented in large numbers—that our manufacturers cannot be ignored.

It is a fortunate circumstance that almost all the vast range of circuitry—which is, after all, the very essence of radio and electronics—can be set up with an extremely limited range of more or less standard components. With resistors and capacitors of a score or so of "preferred" values and two or three ratings, a few inductors and a small collection of more specialized parts, there is hardly any limit to what can be done. The fact that new arrangements can be put into effect so easily has undoubtedly been an important factor in the growth of our art. Standardization of components became established to a useful extent even before any conscious effort to achieve it was made. Since its real importance was realized constant efforts have been made to achieve greater uniformity; one of the good things that came out of the war was a notable advance in this direction. But we believe that still more standardization is necessary in order that production may reach higher levels combined with the greatest possible economy. This is a matter in which there must be co-operation between makers and users of components. The organization for ensuring this co-operation already exists, and we hope it will grow. Increasing standardization—of the right sort—will make for more efficiency in production for home use, and will give an advantage on the export market. In the latter market the contribution of component manufacturers is already considerable, and it is likely to become greater. A refreshing tendency, evident at the Exhibition, was to give the foreign buyer the kind of thing he wanted, rather than that judged to be good for him.

We are not suggesting that the maker of components should pander to the demand for cheap and nasty products. During the war, when cost did not matter, he learned to make things to a much higher standard than ever before; since the war he has learned in many cases that high quality and low production costs are not entirely irreconcilable. We observe with pleasure a distinct reluctance to depart from the high standards to which the industry has become accustomed. It would be a pity if the reputation that has been acquired should be lost.

A Virtually New Field

Makers of components are usually quick to react to the demand for products of new kinds, and a number of parts suitable for low-powered communication equipment were to be seen at the exhibition. But this is a side of radio that is making great advances at present, both at home and abroad, and we think that still more specialized components are needed; if a large measure of standardization of their design can be achieved, so much the better, as it will help to keep down costs, and so lead to still wider applications of what the G.P.O. calls "business radio."

At the opening of the R.C.M.F. exhibition the Minister of Supply stressed the need for increasing standardization, and promised in return that the Government would do its best to help the industry to sell its products in overseas markets. The industry has indicated that it would welcome Government help in securing its share of import quotas in countries which cannot at present accept its products; it would also benefit by a more rapid extension of our home television service. We think that the industry, by its own efforts, has shown itself to be worthy of Government support.

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Television E.H.T.

I.—Required Characteristics : Survey of

By A. H. B. WALKER, B.Sc. (Hons.), A.M.I.E.E.

(Research Laboratory, Westinghouse Brake and Signal Company)

MANY new problems have been introduced by the need for high D.C. voltages —in the order of 5kV—in television receivers. One of the most troublesome was, and still is, that of producing small, light and inexpensive transformers which will operate reliably at these voltages in the high temperatures and heavy dust deposits of the average domestic television receiver. The problem is becoming more acute at the present time owing to the continued trend towards ever-higher voltages in domestic equipment. While existing 9in and 12in tubes will give reasonably bright pictures at anode potentials of 4 kV and 5 kV, new developments on aluminium-backed phosphors will probably increase these voltages to the order of 7 or 8 kV, while special small high-brilliance tubes suitable for optical image projection, will probably require anode potentials of 25 or even 50 kV. Thus it is not surprising that there is much investigation in progress towards solving this E.H.T. supply problem, and it is the object of this article briefly to review some of the alternative methods, and in particular to draw attention to the way in which recent developments in high-voltage metal rectifiers have opened up possibilities hitherto impracticable on physical or economic grounds.

E.H.T. Supply Requirements.

Before comparing alternative methods, it is essential to set out the performance to be achieved; it is perhaps not generally realised how important is the performance of the E.H.T. supply, nor how "good" it should be for acceptable results.

Since the tube beam current is drawn from the E.H.T. supply, and (apart from safety discharging resistors) constitutes the total load on it, this load current is modulated over the whole band of video frequencies, and moreover, since the D.C. component of the video signal has been either preserved or restored at the grid of the cathode-ray tube, the band of frequencies extends right down to zero frequency or D.C. This, one might say, should cause no difficulty provided that the power pack can supply the maximum load. Unfortunately, two other important factors, namely, the beam focus and the beam "stiffness" or deflection sensitivity, are also affected by the electron velocity which is dependent on the E.H.T. voltage. To avoid upsetting the focus or the picture size it is therefore essential to maintain the E.H.T. voltage constant and independent of beam current variations (*a*) at both high and low video frequencies, and (*b*) (more difficult) at very low frequencies extending down to changes in mean D.C. load current. The first requirement can readily be met by terminating the E.H.T. supply with a reservoir capacitor sufficiently large to provide an adequate time constant with the equivalent resistance presented by the tube anode when carrying peak white beam current. This time constant must be long compared with the time of one frame scan period, and this is easily achieved. Consider, for example, a tube operating at 5 kV with a peak white beam current of 100 microamperes; then the equivalent tube resistance equals 50 MΩ, and if we aim at a time constant (RC) of five times the frame scan period, or 0.1 second, then

$$C = \frac{0.1}{50} = 0.002\ \mu F$$

In actual practice, except for high-frequency E.H.T. supplies, a larger capacitance than this is likely to be used in any case for smoothing purposes, so that (*a*) above does not usually cause any difficulty.

However, all forms of E.H.T. power supply have internal resistance, so that no increase in smoothing capacitance will deal with the problem of maintaining

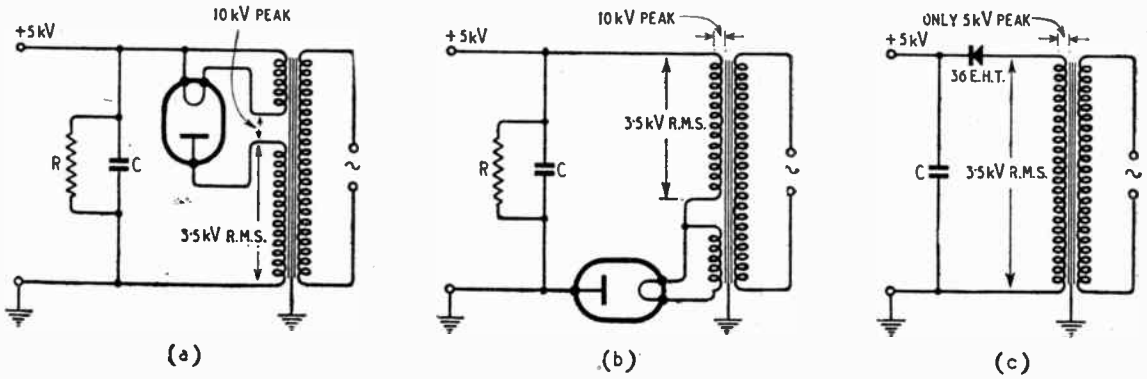

Fig. 1. Half-wave rectifier circuits all developing 5 kV. In (a) 10 kV peak appears between windings, in (b) 10 kV peak between windings and core, in (c) the peak is reduced to 5 kV by elimination of the heater winding

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Supply

Existing Methods

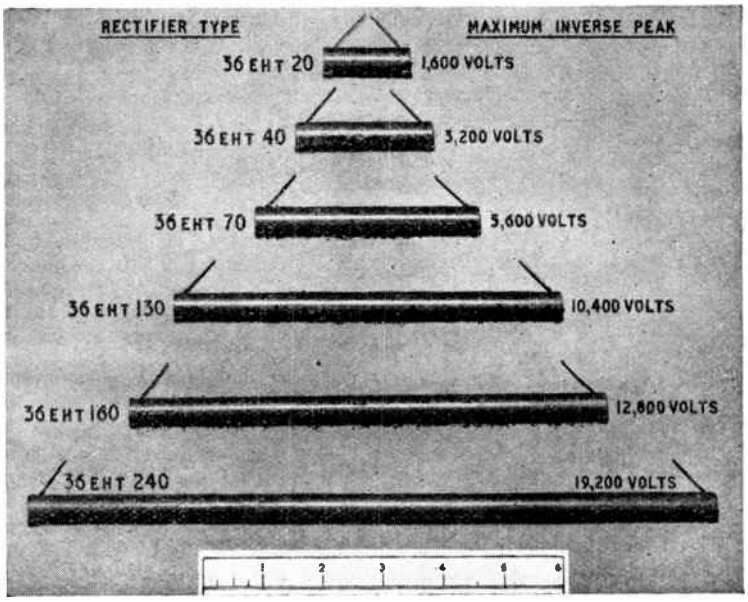
a constant E.H.T. voltage with changes in the mean D.C. load current. In order to define a tolerable limit to this D.C. " regulation " and to simplify the comparison between different forms of power supply, it is convenient to refer to the regulation as the percentage change in E.H.T. voltage for a mean load current change of 100 microamperes, as this represents typical operating conditions fairly well. A regulation of 10 per cent per 100μA change is a rough outside limit for a reasonable result on a directly viewed tube, while a figure of 1 per cent or 2 per cent will probably be necessary for projection equipment.

The remaining performance criterion is residual ripple on the E.H.T. supply. Where the transmitter frame scan frequency is locked to the mains supply, a certain amount of ripple can be tolerated, since stationary hum and defocus bands are not very noticeable. The B.B.C. is attempting to ensure frame frequency synchronisation to the electricity grid for all outside broadcasts, but as this may not always be possible, a low percentage ripple is desirable to avoid the confusion of moving hum bands on these occasions, and also to remove at least one easily avoidable cause of distortion from the normal studio picture. In practice, a figure of 2 per cent ripple gives acceptable results.

Effects of E.H.T. Shortcomings.

The screen effects produced by these faults are all easily recognizable. Apart from hum bands, too short a time constant in the E.H.T. supply will cause defocusing of parts of the picture, but this effect can easily be distinguished from bad focus, since the poorly focused parts will move with the picture ; and further, if the left- and right-hand edges of the picture are examined they will be found to be wavy instead of straight, moving " bulges " occurring on the same horizontal levels as white objects, since it is here that the peak beam current has reduced the E.H.T. voltage, and thus increased the deflection sensitivity. No confusion need arise with the effect which is produced by poor separation of the synchronising signals or " pulling on whites," since this causes a whole strip of the picture to move bodily to the right, thus causing a hollow instead of a bulge at the left-hand side.

If the time constant is adequate, but the regulation is poor, the picture will change in size and in overall focus when the mean D.C. component of the picture changes. This effect is usually seen at its worst on film transmissions where the rapid cutting from one type of shot to another (including titles) causes frequent changes in the mean D.C. level. If this defect is suspected, the picture should be reduced in size slightly so that the edges are just visible inside the mask. If the picture is then carefully watched, and the regulation is in fact poor, it will be seen to alter in size and change slightly in focus at the moment of cutting from shot to shot. The effect can also be produced by varying either the brilliance or the contrast controls, since both of these alter the mean beam current. A simple way of demonstrating the change in mean beam current during a transmission, particularly a film, is to turn one's back to the receiver, and observe the viewing room by the light from the screen alone. The total light in the room is proportional to the mean beam current, and the large light variation which will be observed should convince anyone of the need for a well-regulated E.H.T. supply.



Examples of new 36EHT high-voltage metal rectifiers.

New Metal Rectifiers.

In the following comparison between various possible forms of power supply, there is one important factor which affects nearly all of them. This is the recent introduction of a new range of metal rectifiers (type 36EHT) which operate at extremely high voltages per element. The increase which has been made in the operating voltage is so outstanding that it completely upsets the present balance of advantages between various methods of deriving E.H.T. Before reviewing these systems it is therefore essential to understand what these new rectifiers can do. The construction is tubular, as shown in the photograph ; diameter is $\frac{7}{16}$in, and connection is made by soldering directly to the end-tags. The smaller units (up to say 6000 volts peak inverse) can be mounted by soldering directly to tag boards or to other components, while

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Television E.H.T. Supply—
the larger units require some additional support by lightly clamping with insulating material at a suitable point. 36EHT rectifiers are rated at 0.5 mA mean output, which meets all the requirements of domestic television receivers, and in fact almost all other C.R. equipment. The self-capacitance of these rectifiers is also low, so that they will perform excellently in line fly-back pulse circuits, and will rectify efficiently up to frequencies of the order of 50 kc/s.

Various E.H.T. systems, both conventional and new, will now be examined, and it will be seen to what extent it is practicable or economic to achieve the performance requirements of a good E.H.T. power pack which have been set out above.

E.H.T. Systems Compared.

Having now defined the essential performance points of a good E.H.T. supply, various systems can be compared, and the additional factors of cost, reliability, weight and chassis space can also be taken into account. We will consider : (*a*) High voltage mains transformer and rectifier ; (*b*) High frequency oscillator and rectifier ; (*c*) Rectification of the line fly-back pulses appearing at the line output transformer. A new method of deriving E.H.T. from the normal H.T. transformer through the "Westeht" unit will be considered in a concluding article.

(*a*) *High-Voltage. mains transformer and half-wave rectifier.*— Although the circuit appears simple on paper (Fig. 1), it is not actually so from the designer's viewpoint, as a difficult compromise between cost and reliability has to be made. It has sometimes been overlooked that in the circuit of Fig. 1 (*a*), with a 3500-volt R.M.S. secondary winding, a peak voltage of 10 kV appears between the valve heater winding and the end of the E.H.T. winding, and moreover, that this voltage does not appear until the valve is plugged in. A case has recently been brought to the writer's notice in which a number of mains transformers, quite satisfactory on open-circuit test, all failed soon after being connected up with a valve in circuit.

If the circuit is re-arranged as in (*b*), with the heater winding joined directly to the lower end of the E.H.T. winding, the same 10-kV peak now appears between the windings and the transformer core, although the output is only 5 kV in each case. By the use of a metal rectifier as shown in (*c*), the difficulty is overcome with a very great increase in reliability ; in fact, a transformer which has actually broken down between windings when used in the circuit of (*a*) may often be used with complete satisfaction when connected as in (*c*). A further advantage of (*c*) is that the safety discharge resistor of about 100 MΩ connected across the capacitor is no longer required, since a discharge path of this order of resistance is provided through the metal rectifier and transformer.

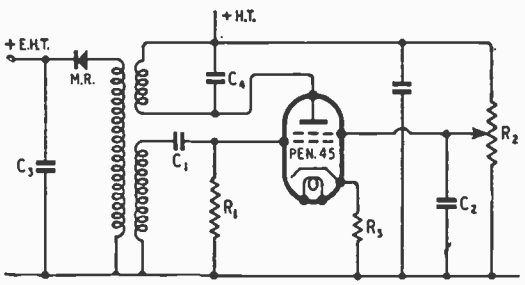

Fig. 2. Typical R.F. oscillator 5 kV E.H.T. unit using metal rectification. C_1, 0.001 μF ; C_2, 0.1μF ; C_3, 0.005 μF ; 6 kV (T.C.C. 'Cathodray') ; C_4 (see text). R_1, 1 MΩ ; R_2, 100 kΩ ; R_3, 50Ω ; MR = Westinghouse 36EHT145. Operating frequency approx. 50 kc/s.

Experience has shown that to obtain reliable service from small transformers wound for these voltages, particularly when using valve rectifiers, a change of technique is necessary. In order to prevent the intrusion of dirt and moisture which will eventually cause almost any small transformer to break down in circuits (*a*) or (*b*), it is now becoming accepted that the complete hermetic sealing of the transformer in a metal can filled with a good dielectric grease or wax is the only permanent answer This normally increases the weight and cost of a component already too heavy and expensive, and has tended to stimulate the search for alternative methods.

The regulation obtainable from all the circuits of Fig. 1 is, however excellent, and well within the limit of 10 per cent per 100 μA specified above, but it must be remembered that some degree of smoothing is usually necessary unless C is made very large. This is usually provided by a smoothing resistor in the positive line, followed by a second high-voltage capacitor, and the voltage drop in this resistor will cause some deterioration in the regulation. However, a value of 1 megohm will only increase the regulation by 2 per cent, and the total can be easily permitted on directly viewed tubes, as it still will not exceed 10 per cent.

(*b*) *High Frequency Oscillator and Rectifier.* One method of dispensing with the high voltage mains transformer is to use an R.F. power oscillator[1], and then, in effect, to use an E.H.T. transformer working at a much higher frequency. This reduces the number of turns necessary on the transformer, and the iron required may also be greatly reduced, or even eliminated.

However, the transformer does not become particularly simple to design since the distributed capacitance and losses must be kept low, while the tendency to corona and surface tracking is greater than at low frequencies. If a mains transformer is used in the receiver, a highly insulated heater winding may be included on it to supply the valve rectifier or alternatively, a suitable rectifier valve may be heated with R.F. current derived from a low-voltage winding coupled to the oscillator coils. In this case, this heater winding must be insulated to withstand a peak of twice the output voltage, exactly as in the low frequency circuit of Fig. 1 (*a*) or (*b*). However, the problem is somewhat eased compared with the 50-cycle case, since at R.F. the spacing can be much greater, and air can be used as part of the insulation. A power

[1] "R-F H-T Power Supplies for Cathode-Ray Tubes," by R. D. Boadle, *A.W.A. Technical Review*, 1946, Vol. 7, p. 53.

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valve is necessary for the oscillator since the R.F. output has to be adequate to supply the valve rectifier heater as well as the useful rectified output, and apart from the cost of this extra valve, the additional drain on the H.T. supply and the additional heater load form a most unwelcome additional burden on the already hard-pressed mains transformer and rectifier. A triode valve will often provide better regulation, but a tetrode is usually employed on account of the higher overall efficiency which can be obtained. The efficiency can, however, be further increased and the transformer design simplified by the use of a 36EHT rectifier, provided that the operating frequency is kept below about 50kc/s, and this requirement supports other design factors which also tend towards keeping the frequency down for a better performance. A possible circuit is shown in Fig. 2. A Pen45 is used as a power oscillator, and is biased by grid current rectification over R_1, added to cathode bias across R_3. The E.H.T. output can be conveniently adjusted by the screen feed resistor R_2, and the values given are suitable for a frequency of about 50kc/s. The E.H.T. winding should be carefully section-wound and well insulated, while the value of the tuning condenser C_4 will naturally depend on frequency and transformer characteristics.

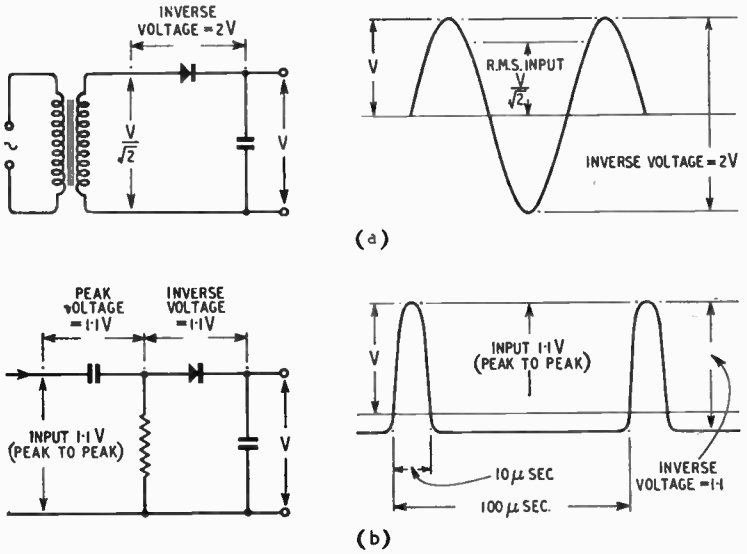

Fig. 3. Illustrating the reduction in rectifier inverse voltage brought about by a pulse waveform. Output voltage is V in both cases. (a) sine wave, rectifier inverse = 2V ; (b) pulse wave, rectifier inverse = 1.1V. Feed condenser peak = 1.1V.

(*c*) *E.H.T. from Line Fly-Back Pulses.*—During the time of the line scan (when the spot is moving from left to right across the picture) the current is increased linearly in the deflection coils and line output transformer, and energy is being gradually stored in the increasing magnetic fields associated with both these components. At the end of the line scan the output pentode is driven rapidly beyond cut-off, and the collapse of these fields produces a high positive voltage surge at the anode. The magnitude of this surge naturally depends on the maximum current value reached just before cut-off, the inductance, and the total losses in the whole circuit or, in other words upon the Q of the output circuit. If no provision is made to absorb this energy, undesirable oscillations will result which will last beyond the fly-back period and will destroy the linearity of the next scanning line, and it is therefore normal practice to connect a series RC circuit across the transformer secondary for this purpose, several watts being dissipated by the resistor. With a normal transformer, however a pulse of about 2,000V with a duration of about 8 or 10μsec still remains in spite of the additional damping, and this can be rectified and used to provide E.H.T. for the tube[2]

Apart from the agreeable fact that it is already available in the receiver, this pulse waveform is also desirable as it results in a great reduction in the rectifier inverse voltage as compared with a sinusoidal input waveform developing the same output voltage. The reason for this is demonstrated in Fig. 3, in which (*a*) represents a conventional half-wave rectifier operating on a sinusoidal input waveform. At the current loadings under consideration the D.C. voltage is very nearly equal to the peak of the input wave, but the peak inverse voltage which occurs on the following half-cycle is actually double the output voltage.

At (*b*) a half-wave rectifier is shown operating on a typical

TABLE 1

Details of some typical 36EHT rectifiers.

Rectifier Type	Overall Length	Peak Inverse Voltage	D.C. Output Voltage	
			In Half-Wave Pulse Circuit (Single-stage)	In 50-cycle Half-Wave Circuit
	in.			
36EHT20	1.41	1,600	1,300	700
36EHT40	2.23	3,200	2,620	1,400
36EHT70	3.67	5,600	4,580	2,330
36EHT130	6.33	10,400	8,500	4,330
36EHT160	7.78	12,800	10,400	5,230
36EHT240	11.26	19,200	15,700	8,400

[2] "Televison E.H.T. Supply," by W. T. Cocking, *Wireless World*, June 1947, Vol. 53, p. 207.

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Television E.H.T. Supply—

pulse waveform having a duration of about 10μsec in the total line scan time of 100μsec. Since there is no direct-current component in the input wave, the areas on either side of the zero line must be equal, and therefore with the time proportions shown, the zero line sinks nearly to the bottom of the waveform and the reverse voltage, although lasting for about 90 per cent of the time, becomes only about 10 per cent greater than the output voltage. The long duration of the inverse voltage makes it essential to ensure that the rectifier reverse leakage is negligible at this voltage, whereas in (*a*), although the peak inverse voltage is much greater, the duration is shorter, so that a somewhat higher instantaneous reverse rectifier current can be allowed. This is the reason for the different inverse voltage ratings recommended for the new type 36EHT rectifiers when used in different circuits. (See Table 1).

Half-Wave Valve Rectifier.—When a valve is used to rectify the pulse, the circuit is limited in practice to a straight half-wave arrangement, both on economic grounds, and also as a result of heater difficulties, and it is therefore necessary to design the line output transformer with very low losses in order to develop a peak voltage higher than the desired E.H.T. voltage across the primary winding. In this case a conventional series RC damping circuit would also reduce the desired peak voltage, so that damping is usually provided by short-circuiting the first unwanted half-cycle of the oscillation by a self-biased diode or metal rectifier. This arrangement is shown in Fig. 4, in which C_1 charges to a bias voltage which is adjustable by R_1 to vary the clipping level.

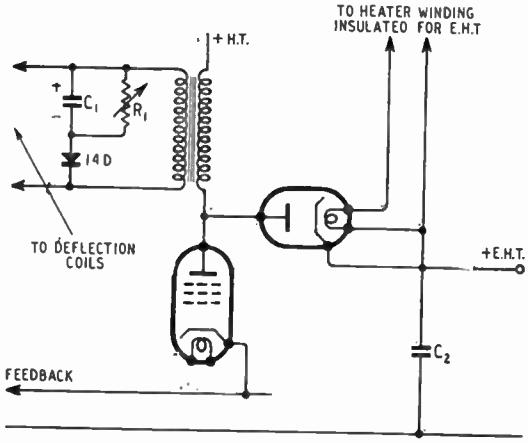

Fig. 4. Valve rectification of line flyback pulse. The circuit is usually limited to a single half-wave rectifier, and the transformer must be designed to give a very high peak voltage. Oscillation is damped by a self-biased rectifier type 14D across the deflection coils, as an RC circuit would damp the desired peak. C_1 25 μF, 25 V; C_2, 0.005 μF; R_1, 1000 Ω.

Pulse Voltage Multiplier.—By taking advantage of the new 36EHT series of metal rectifiers, a pulse-driven voltage multiplier may be used. There is no need to take any special steps to generate a very high-voltage pulse (itself a probable source of breakdown in the line output transformer) and the normal amplitude of pulse which is developed by a perfectly standard transformer, damped if required by the conventional RC circuit, may be used and multiplied up to the extent required. The pulse voltage multiplier circuit may comprise any desired number of stages; i.e., doubler, tripler, quadrupler, etc. As only small capacitors are required owing to the high frequency (10 kc/s), and since Series 36EHT rectifiers are also so small, a very compact and light source of E.H.T. can be built; it is, moreover, free from the cost and breakdown difficulties of highly insulated heater windings. Since the pulse voltage multiplier circuit has to operate from a "one-sided" wave, it differs from a conventional multiplier circuit, and a typical arrangement is shown in Fig. 5. The positive-going anode pulse in effect charges up the capacitors C_2 in parallel through the rectifiers and the feed capacitors C_1 and C_3. Capacitors C_2 then discharge in series through the load, and the cross-connected resistors R_1. It is worth noting that if three or more stages are used, C_3, and any following capacitors, may be fed directly from the valve anode instead of from the previous feed capacitor, as shown in Fig. 5. If this is done, the additional current and resultant voltage drop in C_1 is avoided, but C_3 must of course be increased in voltage rating to a figure of double the pulse voltage. This latter arrangement is known as "parallel feed," since all the rectifiers are fed from their own capacitors connected in parallel to the feed point (the valve anode in this case) while the arrangement of Fig. 5 is known as "series feed," as although the rectifiers are all fed in parallel, the feed capacitors are series connected. In general, series feed is preferable as all the capacitors may be of the same voltage rating which is usually convenient.

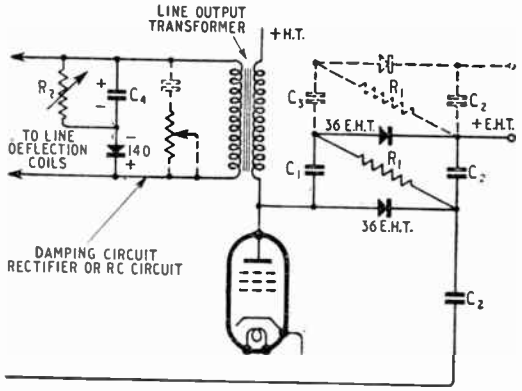

Fig. 5. Pulse-driven voltage multiplier circuit fed from a normal line output transformer. Heavy lines show a doubler, dotted lines show the additions to form a tripler. Normal RC damping across deflector coils may be used (dotted), or to increase the output voltage a self-biased metal rectifier may be substituted as shown. See Table 2 for component values for various output voltages.

The connecting leads should be kept as short as possible, to reduce the stray capacitance. As these

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leads are almost all carrying very high-voltage pulses at line frequency, they can, if unduly long, easily inject line frequency pulses into the frame scan generator circuits and thus impair the interlace.

Since the discharge path lies through the series resistors R_1, it is apparent that the regulation is bound to be impaired to some extent, but if R_1 is made too low, the output voltage will be reduced. The best compromise will depend on the mean beam current required, as well as other indeterminate variables, but a value of 1 megohm may be used for the first tests, as it will generally result in a voltage regulation of between 5 and 10 per cent per 100μA. In general, however, R_1 should be increased as much as possible without producing the effects of poor regulation which have already been described. Either RC damping or rectifier damping may be used, the latter producing a higher output voltage as already mentioned.

An approximate guide to the number of stages required, and the recommended components for various output voltages, is given in Table 2, but owing to variation in pulse shape and duration produced by different designs of transformer and different degrees of negative feed-back, etc., it should not be expected that the output voltages listed will be exactly obtained in all cases, but the circuit is very flexible, and it is hoped that the information given will be of help to those wishing to try the circuit.

TABLE 2

Typical operating conditions for the pulse multiplier circuit of Fig. 5. Capacitors all 0.005 μF. (May be reduced to 0.001 μF for parallel feed). $R_1 = 1$ MΩ, $R_2 = 1{,}000\ \Omega$ variable.

Peak Pulse Input Voltage	Approximate D.C. Output Voltage at 100 μA. Load			Rectifiers	
	Half-wave	Doubler	Tripler	E.H.T.	Damping (for 5 : 1 Transformer)
1,450	1,310	2,340	3,340	36EHT20	14D19
1,810	1,640	2,930	4,180	36EHT25	14D24
2,180	1,960	3,520	5,000	36EHT30	14D28
2,540	2,190	4,100	5,850	36EHT35	14D28
2,900	2,620	4,680	6,570	36EHT40	14D128
3,470	2,950	5,280	7,520	36EHT45	14D36

Short-wave Conditions

February in Retrospect : Forecast for April

By T. W. BENNINGTON and L. J. PRECHNER (Eng. Div., B.B.C.)

DURING February the average maximum usable frequencies for these latitudes increased somewhat both by day and night. The daytime increase—mentioned in this column for February—was due to normal seasonal trend after the "midwinter effect," and the night-time increase is the beginning of the increase towards the midsummer maximum.

The daytime increase was much less than expected, due possibly to decreasing sunspot activity. Although long-distance communication on the higher frequencies was good to most parts of the world, frequencies as high as 50 Mc/s were practically never usable, though they had been during November. Night-time working frequencies, though relatively low, were mostly above 9 Mc/s, except over a few high-latitude paths.

Conditions were not severely disturbed at any time during the month although ionosphere storms did occur during the periods 2nd, 11th and 15th-18th.

Forecast

In April, while the daytime M.U.F.s in the Northern Hemisphere should begin to decrease towards the midsummer minimum, the night-time M.U.F.s should continue their increase towards the midsummer maximum. However, since daylight will last longer, moderately high frequencies can remain in use for considerably longer periods. In April working frequencies for most transmission paths will be somewhat lower than in March during the full daylight period, somewhat higher during the morning and evening periods, and considerably higher during the full darkness period.

Daytime communication on high frequencies (like the 28-Mc/s band) though still possible should be rather less than in March. Over many circuits frequencies as high as 15 Mc/s —or even higher in some cases— should remain usable till well after midnight. Frequencies lower than 11 Mc/s will be seldom required at any time during the night.

For transmission distances between about 600 and 1,000 miles the E layer may often control transmission during the daytime, and higher working frequencies may be needed than would otherwise have been the case.

Sporadic E, though it should begin to increase, is not likely to be very prevalent during the month, the real increase usually occurring in May.

Below are given, in terms of the broadcast bands, the working frequencies which should be regularly usable during April for four long-distance circuits running in different directions from this country. All times mentioned here are in G.M.T. In addition, a figure in brackets is given for the use of those whose primary interest is the exploitation of certain frequency bands, and this indicates the highest frequency likely to be usable for about 25 per cent of the time during the month for communication by way of the regular layers:—

Montreal :	0000	15 Mc/s	(22 Mc/s)
	0100	11 ,,	(18 ,,)
	0900	15 ,,	(22 ,,)
	1000	17 ,,	(28 ,,)
	1200	21 ,,	(32 ,,)
	2100	17 ,,	(28 ,,)
	2300	15 ,,	(20 ,,)
Buenos Aires:	0000	17 Mc/s	(25 Mc/s)
	0200	15 ,,	(21 ,,)
	0900	21 ,,	(30 ,,)
	1000	26 ,,	(39 ,,)
	2100	21 ,,	(32 ,,)
	2300	17 ,,	(23 ,,)
Cape Town :	0000	17 Mc/s	(25 Mc/s)
	0600	21 ,,	(29 ,,)
	0700	26 ,,	(40 ,,)
	2000	21 ,,	(30 ,,)
	2300	17 ,,	(24 ,,)
Chungking :	0000	11 Mc/s	(16 Mc/s)
	0300	15 ,,	(21 ,,)
	0400	17 ,,	(25 ,,)
	0600	21 ,,	(30 ,,)
	1600	17 ,,	(24 ,,)
	2000	15 ,,	(22 ,,)
	2200	11 ,,	(17 ,,)

A moderate amount of ionosphere storminess is usual during April. At the time of writing it would appear that ionosphere storms are more likely to occur during the periods 1st, 8th, 10th-13th, 25th-26th and 28th, than on the other days of the month.

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Push-Pull Input Circuits

Part 4.—The Anode Follower

By W. T. COCKING, M.I.E.E.

AN important and widely used type of phase-reverser must now be considered. Originally known as the paraphase[1] amplifier, it was later termed the see-saw[2] circuit and in essentials it is identical with a radar circuit commonly called an anode follower.[3] Basically, it is a circuit, not unlike those described in Part 3, in which a phase-reversing amplifier is fed from a potential divider so that the overall amplification is unity. The amplifier, however, is provided with negative feedback of a form giving a low input impedance to the valve and the input impedance forms one arm of the input potential divider. As the input impedance depends on the amplification and the potential-divider ratio depends on the input impedance the circuit is largely self-compensating for changes of amplification. Discussion of the circuit is complicated by the fact that there are several minor variations of it, variations chiefly in the positions of blocking capacitors, but which do influence the performance at low frequencies. In their performance at medium and high frequencies the circuits are all substantially the same.

One arrangement of the amplifier part is shown in Fig. 18; no bias circuit is shown since it is assumed that the arrangements made for it have no effect on the operation. Considering matters at middle frequencies where both C_1 and any shunt capacitance can be ignored, the amplification is $A_0 = -E_{12}/E_{gc}$. The voltage E_{gc} drives a current i through R_f and as the grid of the valve is assumed to take no current, the input impedance is, by definition, $Z_{in} = E_{gc}/i$.

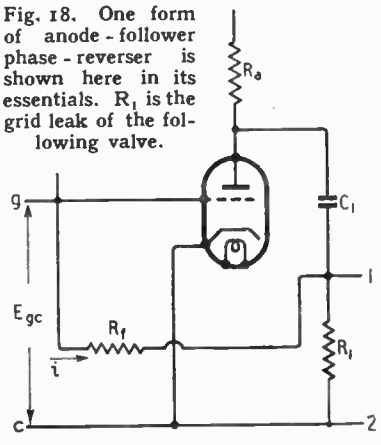

Fig. 18. One form of anode-follower phase-reverser is shown here in its essentials. R_1 is the grid leak of the following valve.

By inspection of Fig. 18 it is clear that $E_{gc} - E_{12} = iR_f$, consequently $Z_{in} = R_f/(1 + A_0)$. Now if this circuit is fed from a voltage E_{AB} through a series resistance R_i as in Fig. 19, $E_{gc} = E_{AB}/(1 + R_i/Z_{in})$ and hence the overall amplification $-E_{12}/E_{AB} = A =$

$$A_0\Big/\left[1 + \frac{R_i}{R_f}(1 + A_0)\right].$$

For push-pull operation it is required that $A = 1$, therefore, the balance condition is

$$\frac{R_i}{R_f} = \frac{A_0 - 1}{A_0 + 1}.$$

In some variations of the circuit a grid leak is connected across terminals g, c. Its effect can be taken into account by considering it as a resistance in shunt with Z_{in}.

From the above expression it is clear that if A_0 is large compared with unity R_i and R_f are nearly equal in value and then $A = A_0/(A_0 + 2)$. It is also plain to see that if A_0 is large compared with 2, A is very nearly 1 and is almost independent of the actual value of A_0. In other words, a circuit variation which acts to alter A_0 changes the input impedance Z_{in}, and so alters the input potential-divider ratio that it compensates for the change of A_0.

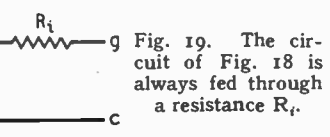

Fig. 19. The circuit of Fig. 18 is always fed through a resistance R_i.

The value of A_0 is easily calculable and is given by Eqn. (2) of Appendix IV. It is convenient to express the amplification and the balance condition in terms of g_mZ and Z/Z_f rather than A_0 and this is done in Eqns. (4) and (5). It then becomes clear that if it is desired to have R_i and R_f of equal value it is necessary to have g_mR very large compared with unity. With a triode valve R can rarely be much greater than

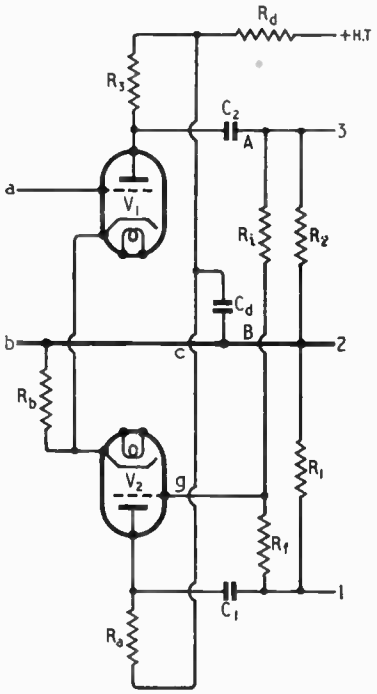

Fig. 20. The phase-reverser of Figs. 18 and 19 is drawn here combined in the usual manner with the preceding stage.

10 — 15 kΩ and g_m is usually about 2 mA/V so that g_mR is of the order of 20 — 30. While this is certainly a good deal larger than unity it is not very large compared with it, and with a triode it is usually necessary to adjust R_i or R_f for balance.

With a pentode R can often be

[1] "Science Museum Receiver," by R. F. G. Denman and A. S. Brereton. *Wireless World*, July 30th and August 6th, 1930. Vol. 27, pp. 96 and 116.

[2] "The See-Saw Circuit," by M. G. Scroggie. *Wireless World*, June 1945. Vol. 51, p. 194. See also p. 263, September 1945.

[3] "Introduction to Circuit Techniques for Radiolocation," by F. C. Williams. *Journ. Instn. Elect. Engrs.* Vol. 93, Part IIIA, No. 1, p. 289.

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20 — 50 kΩ and g_m can be 2 — 6 mA/V, so that g_mR may be 40 — 300. With values of over 200, say, R_i and R_f can be equal with only a very small error. From this point of view, therefore, the pentode is superior to the triode.

Technically, of course, there is no particular merit in having R_i and R_f equal. In practice, however, if they can be equal a balance adjustment is avoided, for it is not difficult to pick two resistors for equality of resistance when their precise actual values are unimportant.

We can now consider the performance at high frequencies. R_a is in effect shunted by a capacitance C comprising the anode-cathode capacitance of the valve, stray circuit capacitance and the input capacitance of the following stage. Also R_f is shunted by the grid-anode capacitance of the valve. This is appreciable with the triode, but negligible with the screened pentode.

The relevant equations are developed in Appendix IV and it is sufficient to use the approximate relations (12) and (13). It is easy to see that if the out-of-phase component of output is satisfactorily low the in-phase unbalance is negligible since $1 + g_mR$ will rarely be less than 20. We need only consider Eqn. (13) in practice, therefore.

In a typical case with a triode we might have $g_m = 2$ mA/V, R = 10 kΩ, R_f = 100 kΩ, C = 100 pF, f = 10 kc/s. Then $U_2 = 0.006$; the unbalance at 10,000 c/s is only 0.6 per cent, which is negligible. With a pentode g_mR tends to be higher and U_2 approximates $2\omega C/g_m$. It is clear, therefore, that the unbalance at high audio frequencies is sufficiently small for all ordinary requirements.

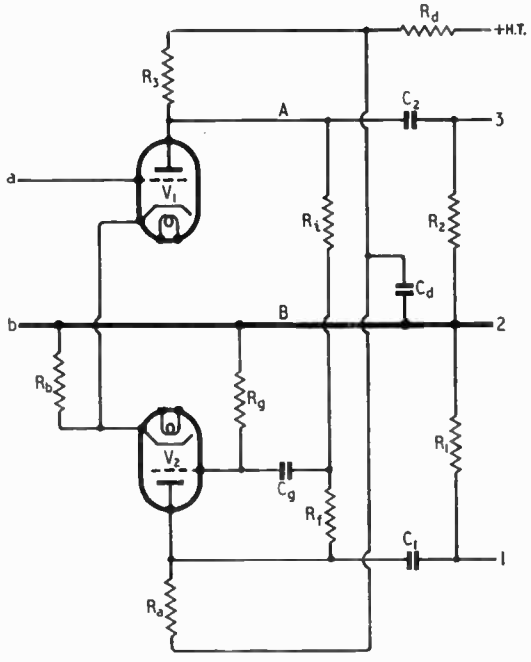

Fig. 21. A modified circuit is shown here in which R_i and R_f are transferred to the input side of C_1 and C_2.

It is to be noted that the equations have been developed on the assumption that $C_fR_f = C_iR_i$. As R_f and R_i are nearly equal this means that R_i should be shunted by a capacitance equal to the grid-anode capacitance of the valve. The low capacitance of a screened pentode is an advantage in making any such shunt to R_i unnecessary.

At low frequencies the coupling capacitor C_1 becomes important. The grid of one push-pull valve is connected to 1 of Fig. 18 and the grid of the other to A of Fig. 19. The necessary equations are developed in the Appendix and Eqn. (17) gives the out-of-phase unbalance approximately, the in-phase unbalance being negligible.

With a triode we might well have $g_m = 2$ mA/V, $r_a = 15$ kΩ, $R_a = 45$ kΩ, $R_1 = 250$ kΩ, R_f = 250 kΩ, $C_1 = 0.1$ μF. These give $R'' = 11.25$ kΩ, R = 10.8 kΩ, $R' = 261.25$ kΩ, and so at 50 c/s, $U_2 = 0.01$. As under the conditions given the value of R_f does not affect the high-frequency response, the change of value between the two examples is unimportant. At low frequencies a high value of R_f is advantageous; thus, if in the last example R_f is reduced to 100 kΩ, U_2 is increased to 0.018.

This is, of course, as one would expect, for R_1 and R_f are almost in parallel as regards the feed through C_1. As regards the high-frequency response it must not be forgotten that it is independent of R_f only if R_i and R_f are shunted by equal capacitances. If they are not, then the high-frequency unbalance will increase with high values of R_f.

It is to be noted that the low-frequency unbalance arises because there is one more coupling on one side of the chain than on the other. In Fig. 19 one push-pull valve is fed directly from A, B, but the other is fed from 1, 2 of Fig. 18 and this voltage is derived from A, B, through the whole network including C_1R_1.

The time constant effective is not that of C_1R_1 alone, however,

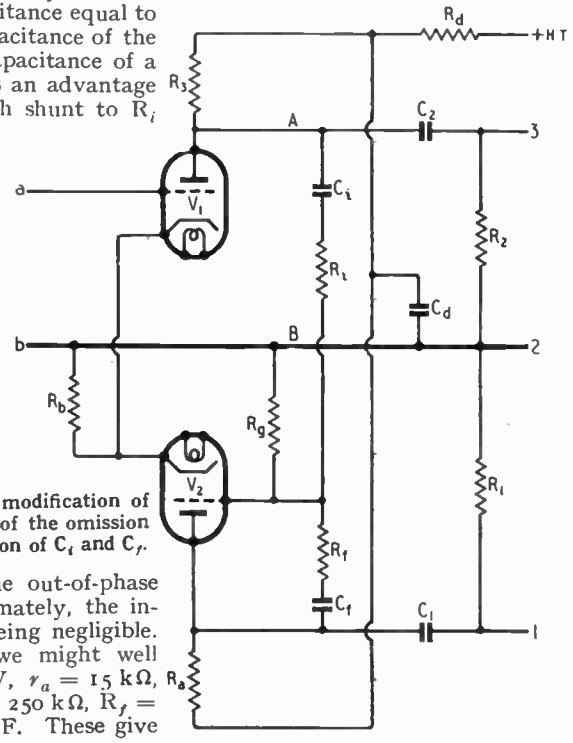

Fig. 22. A further modification of the circuit consists of the omission of C_g and the inclusion of C_i and C_f.

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Push-pull Input Circuits—

as in the case of the non-feedback circuits of Part III, for the effective value is greatly increased by the feedback. This is clearly shown by the approximate relation of Eqn. (17a) which holds when $g_m R$ is very large. The time constant is $C_1 R'$ ($\approx C_1 R_1$) multiplied by $g_m R'_1/(1 + R_1/R_f)$.

The complete circuit of the phase-reverser with the preceding amplifier is drawn in its usual form in Fig. 20 and the parts belonging to the phase-reverser are lettered in the same way as in Figs. 18 and 19. If V_1 and V_2 are similar valves and if $R_3 = R_a$, $R_2 = R_1$, and $C_2 = C_1$ the alternating anode currents of the two valves will be nearly equal and opposite. The bias resistor R_b and the decoupling components R_d and C_d will then have a negligible effect on the performance. This is actually the only reason for using similar valves and circuit values, for there is no push-pull action as regards distortion.

Because of the negative feedback provided on V_2 by R_f this stage is much more linear than V_1, so that if the two stages are otherwise similar it is necessary to design V_1 for the requisite undistorted output and one can be assured that V_2 will be rather better.

Suitable values for the circuit of Fig. 20 using EF37 valves as triodes are :—$R_a = R_3 = 47$ kΩ, $R_1 = R_2 = 220$ kΩ, $R_b = 750$ Ω, $R_f = 250$ kΩ, $R_i = 226$ kΩ, $C_1 = C_2 = 0.1$ μF. The output obtainable is at each pair of output terminals 3, 2 and 1, 2, and is the output of which V_1 alone is capable with the H.T. supply available and the value of the decoupling resistor R_d.

A variation of the circuit of Fig. 20 is produced by omitting R_1 and R_2 and connecting a resistor to earth from the junction of R_i and R_f; that is, from the grid of V_2. This change in itself affects the performance very little and it gives a saving of one resistor. However, it is desirable for this added resistor to be large compared with Z_{in}, which means that it cannot be much different from R_f. It is common to the grid circuits of three valves and so should not be very large. As V_2 is not a large valve it is not

APPENDIX IV.

Referring to Fig. 18, let $A_0 = E_{21}/E_{gc}$ and $Z_{in} = E_{gc}/i$.
Now $iZ_f = E_{gc} + E_{21}$, therefore,

$$Z_{in} = \frac{Z_f}{1 + A_0} \quad \ldots \quad (1)$$

Also, at frequencies for which the reactance of C_1 can be ignored,

$$i_a = g_m E_{gc}$$
$$E_{21} = (i_a - i) Z$$

Therefore, $$A_0 = \frac{g_m Z - Z/Z_f}{1 + Z/Z_f} \quad \ldots \quad (2)$$

When the stage is fed through an impedance Z_i, Fig. 19,

$$\frac{E_{21}}{E_{AB}} = A = \frac{A_0}{1 + Z_i/Z_{in}} \quad \ldots \quad (3)$$

$$= \frac{A_0}{1 + \frac{Z_i}{Z_f}(1 + A_0)} = \frac{g_m Z - Z/Z_f}{1 + Z/Z_f + (1 + g_m Z)\, Z_i/Z_f} \quad \ldots \quad (4)$$

At middle frequencies all reactances are negligible and all the Z terms become R terms. The condition for balance in push-pull operation is $A = 1$, hence

$$\frac{R_i}{R_f} = 1 - 2\,\frac{1 + R/R_f}{1 + g_m R} \quad \ldots \quad (5)$$

At high frequencies $Z = R/(1 + j\omega CR)$, $Z_f = R_f/(1 + j\omega C_f R_f)$, $Z_i = R_i/(1 + j\omega C_i R_i)$ and then

$$A = \frac{g_m R - R/R_f - j\omega C_f R}{\left\{1 + \frac{R}{R_f} + \frac{R_i}{R_f}(1 + g_m R)\frac{1 + j\omega C_f R_f}{1 + j\omega C_i R_i}\right\} + j\omega CR\left\{1 + \frac{C_f}{C} + \frac{R_i}{R_f}\cdot\frac{1 + j\omega C_f R_f}{1 + j\omega C_i R_i}\right\}} \quad (6)$$

When $C_f R_f = C_i R_i$ this reduces to

$$A = \frac{g_m R - R/R_f - j\omega C_f R}{1 + \frac{R}{R_f} + \frac{R_i}{R_f}(1 + g_m R) + j\omega CR\left\{1 + \frac{C_f}{C} + \frac{R_i}{R_f}\right\}} \quad \ldots \quad (7)$$

Inserting the value of R_i/R_f given by Eqn. (5) gives

$$A = \frac{g_m R - R/R_f - j\omega C_f R}{g_m R - R/R_f + j\omega CR\left\{1 + \frac{C_f}{C} + \frac{g_m R - 1 - 2\,R/R_f}{g_m R + 1}\right\}} \quad (8)$$

The unbalance is

$$U = 1 - A$$

$$= \frac{j\omega CR\left\{1 + \frac{g_m R - 1 - 2\,R/R_f}{g_m R + 1}\right\}}{g_m R - \frac{R}{R_f} + j\omega CR\left\{1 + \frac{C_f}{C} + \frac{g_m R - 1 - 2R/R_f}{g_m R + 1}\right\}} \quad \ldots \quad (9)$$

$$= U_1 + jU_2$$

$$U_1 = \frac{\omega CR\left\{\frac{C_f}{C} + 2\,\frac{g_m R - R/R_f}{g_m R + 1}\right\}}{\left(g_m R - \frac{R}{R_f}\right)^2 + \omega^2 C^2 R^2\left(\frac{C_f}{C} + 2\,\frac{g_m R - R/R_f}{g_m R + 1}\right)^2} \quad \ldots \quad (10)$$

$$U_2 = \frac{2\omega CR\,\frac{\left(g_m R - \frac{R}{R_f}\right)^2}{g_m R + 1}}{\left(g_m R - \frac{R}{R_f}\right)^2 + \omega^2 C^2 R^2\left(\frac{C_f}{C} + 2\,\frac{g_m R - R/R_f}{g_m R + 1}\right)^2} \quad \ldots \quad (11)$$

When U_1 and U_2 are small and $C_f \ll C$

$$U_1 \approx U_2/(g_m R - R/R_f) \quad \ldots \quad (12)$$

$$U_2 \approx \frac{2\omega CR}{g_m R + 1} \quad \ldots \quad (13)$$

where $$\frac{1}{R} = \frac{1}{r_a} + \frac{1}{R_a} + \frac{1}{R_1}$$

At low frequencies the effect of the shunt capacitances is negligible, but C_1 is important. Equations (1) and (3) are still valid but the expression for A_0 is changed. If

$$R'' = \frac{r_a R_a}{r_a + R_a}; \quad R' = R_1 + R''$$

$$A_0 = \frac{E_{21}}{E_{gc}} = -\frac{\frac{R}{R_f} - g_m R + \frac{R/R_f}{j\omega C_1 R''}}{1 + \frac{R}{R_f} + \left(1 + \frac{R\,R'}{R_f R''}\right)\Big/ j\omega C_1 R'} \quad \ldots \quad (14)$$

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and so

$$A = \frac{E_{21}}{E_{AB}} = \frac{1 - \frac{1}{j\omega C_1 R''} \cdot \frac{R/R_f}{g_m R - R/R_f}}{1 + \frac{1}{j\omega C_1 R'}\left\{\frac{2}{g_m R + 1} + \frac{R\,R'/R_f\,R''}{g_m R - R/R_f}\right\}} \quad \ldots \quad (15)$$

when R_i/R_f has the value of Eqn. (5).

Therefore,

$$U = \frac{\frac{2}{j\omega C_1 R'}\left[\frac{1}{g_m R + 1} + \frac{R\,R'/R_f\,R''}{g_m R - R/R_f}\right]}{1 + \frac{1}{j\omega C_1 R'}\left[\frac{2}{g_m R + 1} + \frac{R\,R'/R_f R''}{g_m R - R/R_f}\right]} \quad \ldots \quad \ldots \quad \ldots \quad (16)$$

and when U is small

$$U_2 \approx \frac{2}{\omega C_1 R'} \cdot \frac{\frac{g_m R - R/R_f}{g_m R + 1} + \frac{R_1}{R_f}}{g_m R - R/R_f} \quad \ldots \quad \ldots \quad \ldots \quad \ldots \quad (17)$$

When $g_m R \gg 1$ and $g_m R \gg R/R_f$

$$= U_2 \approx \frac{2}{\omega C_1 R'} \cdot \frac{1 + R_1/R_f}{g_m R} \quad \ldots \quad \ldots \quad \ldots \quad \ldots \quad \ldots \quad (17a)$$

Referring to Fig. 21.

$$Z_{in} = \frac{R_f + Z}{1 + g_m Z x_1} \quad \ldots \quad \ldots \quad \ldots \quad \ldots \quad (18)$$

$$A = \frac{E_{21}}{E_{AB}} = \frac{x_2 Z (g_m R_f x_1 - 1)}{R_f + Z + R_i (1 + g_m Z x_1)} \quad \ldots \quad \ldots \quad \ldots \quad (19)$$

The balance condition is still given by Eqn. (5) and so

$$U = 1 - \frac{g_m Z x_1 - Z/R_f}{1 + \frac{Z}{R_f} + \left(1 + g_m Z x_1\right)\left(1 - 2\frac{1 + R/R_f}{1 + g_m R}\right)} \frac{x_2}{x_3} \quad \ldots \quad (20)$$

where

$$Z = R\frac{1 + 1/j\omega C_1 R_1}{1 + 1/j\omega C_1 R'}; \; x_1 = \frac{1}{1 + 1/j\omega C_g R_g}$$

$$x_2 = \frac{1}{1 + 1/j\omega C_1 R_1}; \; x_3 = \frac{1}{1 + 1/j\omega C_2 R_2}$$

When $R_1 \approx R'$, $g_m R \gg 1$ and $x_2 = x_3$ Eqn. (20) reduces to the approximate relation for the phase unbalance

$$U_2 \approx \frac{1}{\omega C_g R_g} \cdot \frac{1 + R/R_f}{g_m R} \quad \ldots \quad \ldots \quad (20a)$$

Referring to Fig. 22

$$Z_i = R_i + 1/j\omega C_i; \; Z_f = R_f + 1/j\omega C_f$$

and other symbols have their previous meanings

$$Z_{in} = \frac{Z + Z_f}{1 + g_m Z} \quad \ldots \quad \ldots \quad \ldots \quad (21)$$

$$U = 1 - \frac{1 + 1/j\omega C_2 R_2}{1 + 1/j\omega C_1 R_1} \cdot \frac{g_m Z - Z/Z_f}{1 + Z/Z_f} \cdot \frac{1}{1 + Z_f\left[\frac{1}{R_g} + \frac{1 + g_m Z}{Z + Z_f}\right]} \quad (22)$$

It is usual to make $C_i R_i = C_f R_f$ and $C_1 R_1 = C_2 R_2$. Then the balance condition is

$$\frac{R_i}{R_f} = \frac{g_m R - (1 + 2R/R_f)}{g_m R + 1 + \frac{R + R_f}{R_g}} \quad \ldots \quad \ldots \quad (23)$$

and

$$U = 1 - \frac{g_m Z - Z/R_f}{1 + \frac{Z}{Z_f} + \frac{R_i}{R_f}\left[1 + g_m Z + \frac{Z + Z_f}{R_g}\right]} \quad \ldots \quad \ldots \quad \ldots \quad (24)$$

If $R_g \to \infty$ and $Z = R$, then $U = 0$.

When $g_m Z \gg (Z + Z_f)/R_g$ and $g_m Z \gg 2$.

$$U_2 \approx g_m/\omega C_f \quad \ldots \quad \ldots \quad \ldots \quad \ldots \quad (24a)$$

At middle frequencies the unbalance is

$$U = \frac{\Delta x}{\Delta x + \frac{g_m R - R/R_f}{g_m R + 1}} \quad \ldots \quad \ldots \quad (25)$$

$$\approx \frac{\Delta x}{\Delta x + 1} \text{ When } \frac{R}{R_f} \ll g_m R \gg 1$$

$$\approx \Delta x \text{ when } \Delta x \ll 1$$

where $\Delta x = \Delta R_i/R_f =$ the change of $\frac{R_i}{R_f}$ from its correct value for $U = 0$.

unreasonable to ignore it in comparison with output valves, in which case the added resistor can be chosen as if it were common to two valves only. If it is equal to R_f, then R_f should not be more than one third of the maximum permissible grid leak. This is often only 250 kΩ for output valves and then R_f cannot be much more than 90 kΩ. To obtain an equivalent degree of low-frequency unbalance C_1 and C_2 must be considerably larger than with the circuit of Fig. 20. Because of this, this modification is rarely desirable and it need not be further considered.

One very commonly used arrangement is shown in Fig. 21. The change consists of the transference of R_i and R_f to the input side of the coupling capacitors. This necessitates the inclusion of an extra capacitor C_g and grid leak R_g to isolate the grid of V_2 from the H.T. supply.

At medium and high frequencies the performance is unchanged save for the presence of R_g in shunt with Z_{in}. As Z_{in} is often around 5 kΩ or less and R_g can be 2 MΩ the error involved by neglecting it is of no importance.

At low frequencies conditions are different. Unfortunately, the mathematical expressions become much more complex with the result that the labour of determining the unbalance is greatly increased. The expression is given by Eqn. (20). As the expansion in terms of the full resistive and reactive components of the impedances becomes very complicated, it is simpler in this case to use numerical values only and so to work directly from Eqn. (20). A simplified approximate expression is given in (20a), but it is reasonably accurate only when $g_m R$ is very large.

Taking similar values to before (i.e., $g_m = 2$ mA/V, $r_a = 15$ kΩ, $R_a = 45$kΩ, $C_1 = C_2 = 0.1$ μF, $R_1 = R_2 = 250$ kΩ, $R_f = 100$ kΩ, $C_g = 0.01$ μF, $R_g = 2$ MΩ, $f = 50$ c/s), the phase unbalance comes out at 1.5 per cent using Eqn. (20).

Still another form of the circuit is shown in Fig. 22. The change from Fig. 21 lies in the omission of C_g and the insertion of capacitors C_i and C_f in series with R_i and R_f. Eqns. (21) to (24) give the performance and again they are complex when expanded. In

World Radio History

Push-pull Input Circuits—

this circuit if $C_iR_i = C_fR_f$ then in the absence of the grid leak R_g and if C_1 had no influence on Z, the balance could be perfect down to the lowest frequency. In practice there is unbalance at low frequencies and it amounts to 0.9 per cent phase unbalance with $g_m = 2$ mA/V, $r_a = 15$ kΩ, $R_a = 45$ kΩ, $R_1 = R_2 = 250$ kΩ $C_1 = C_2 = C_i = C_f = 0.1$ μF, $R_g = 2$ MΩ, $R_f = 100$ kΩ.

Note that here C_i and C_f are being used as symbols to represent capacitance in series with R_i and R_f instead of capacitance in shunt as in the case of the high-frequency response.

With the sort of values that are practicable in typical cases the phase unbalances at 50 c/s for the circuits of Figs. 20, 21 and 22 are respectively 1 per cent, 1.5 per cent and 0.9 per cent. The differences are very small and, practically speaking, there is little to choose between the circuits.

The unbalance at middle frequencies as a function of circuit values is important and Eqn. (25) shows that the percentage unbalance is approximately proportional to the percentage changes of R_i and R_f from their correct values. Much more latitude in other circuit values is permissible and it can be seen from Eqn. (4) that if g_mZ is high enough such changes are negligible.

The value of R_i/R_f is always slightly less than unity and Z/Z_f is usually around 0.1, but may sometimes be as high as 1. Taking these values Eqn. (4) reduces to $\frac{g_mR - 1}{g_mR + 3}$ and it is clear that when g_mR is large compared with 3 the amplification is nearly unity and almost independent of either g_m or of R. Therefore, neither the valve nor the resistors of the output circuit is critical in value.

The anode-follower phase reverser, or paraphase circuit, is obviously such a great improvement on the other phase reversers, treated in Part 3, that one would always choose it in preference. A comparison with the phase-splitter (Part 2) is less easy.

As far as balance over the A.F. range is concerned there is little to choose between them. The phase splitter requires two equal resistors for balance, whereas the anode follower needs, in the general case, two unequal resistors of precise ratio of values and is, therefore, slightly more difficult in practice.

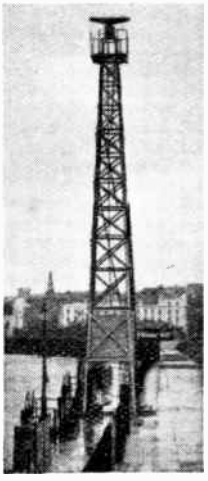
The anode follower has the considerable advantage that the difference of potential between heater and cathode is negligible, whereas it is large in the cathode-follower phase splitter. Also the valve has to supply one output voltage only instead of two so that the undistorted output is doubled. The phase-reverser has a high degree of negative feedback and is consequently very linear.

Where the circuits are used immediately before an output stage which requires a large input the anode-follower circuit is likely to be better than the cathode-follower phase splitter because of the larger output and negligible heater-cathode voltage. When an intermediate push-pull stage is used, or when the output valves need only a small input, there is much less to choose between the circuits and the cathode-follower type is often the more convenient.

Douglas Harbour Radar

BAD-WEATHER AID TO SHIPPING

A RADAR system designed for the complete control of a port was opened on 28th February. The system, designed by Cossor Radar, has been installed at Douglas, Isle of Man. During the summer months, when there is heavy holiday traffic, the port is subject to sudden fog and the radar system will enable shipping to be worked safely in and out of the port in the thickest weather.



The scanner of the Douglas Harbour radar installation on its 60-ft tower.

A rotating cheese aerial is mounted on a 60-ft tower situated at the harbour mouth, and is waveguide-fed through a rotating joint. The transmitter and receiver are housed in a cabin mounted within the base of the mast and are normally unattended, the video output being fed by a 220-ft cable to a P.P.I. display unit in the harbourmaster's control room.

The radar system is basically the standard Cossor Marine Radar set and operates at a wavelength of 3 cm. The pulse width is 0.2 μsec with a peak power of 22-30 kW; the recurrence frequency is 2,000 c/s. A magnetron is used in the transmitter, but the receiver local oscillator is a klystron provided with A.F.C. which operates by controlling its electrode voltages.

The display is on a 9-in cathode-ray tube, two fixed pairs of deflecting coils being used to provide electromagnetic deflection. Three ranges are provided, the maximum being about 3 miles, and the others 1.2 and 0.8 miles. This enables a ship to be located at an adequate distance off-shore and it can be brought in by wireless control to something less than a mile. The shorter ranges can then be brought into action and the ship worked right into harbour.

Navigational information derived from the radar system is conveyed to the ship by V.H.F. telephony and gives the master of the ship precise information about his position and that of other shipping. No radar equipment is needed on the ship and all that is necessary aboard is the transmitter and receiver of the communication channel.

Since not all vessels are equipped with wireless, the port is provided with a high-power loudspeaker, so that warnings and instructions can be conveyed at short range by audible signals.

Index and Binding Case

COPIES of the index to Volume LIII, January-December, 1947, of *Wireless World* are now available from our Publisher, price 1s 1½d, including postage. Binding Cases are also available which, together with the Index, cost 4s 10d by post.

World Radio History

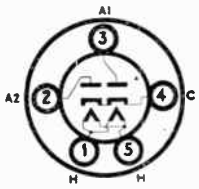
Valve replacements - hard to get

*BRIMARIZE! - a working set

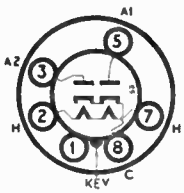
TYPE 84/6Z4 is a full wave rectifier, very popular in pre-war car radios. Type 6X5G will make a satisfactory replacement and in 6 volt receivers, only a change of socket is required.

In 12 volt receivers, the heaters of the 84/6Z4 and one of the other valves are usually connected in series across the 12 volt supply, a resistance being fitted across one of the heaters to equalise the currents in the two valves. When a 6X5G is used the value of this resistor must be reduced.

PUNCH HOLES HERE



84/6Z4



6X5G

CHARACTERISTICS

	84/6Z4	6X5G
Heater Voltage	6.3	6.3 volts
Heater Current	0.5	0.6 amp.
R.M.S. Input	325	325 volts
Rectified Current	60	70 mA.

TYPE	CHANGE SOCKET		CHANGE CONNECTIONS		OTHER WORK NECESSARY	PERFORMANCE CHANGE
	FROM	TO	FROM OLD SOCKET	TO NEW SOCKET		
6X5G	U.X. 5 PIN	INT. OCTAL	PIN 1 " 2 " 3 " 4 " 5	PIN 2 " 3 " 5 " 8 " 7	6 volt sets—None. 12 volt sets — Change value of balancing resistor if fitted (see Note)	NONE

Note.—The value of this resistance in ohms is found by dividing 6.3 by the difference in heater current (expressed in amps.) of the two valves which are in series. e.g.—A type 41 (heater current 0.4 amp.) will require a parallel resistance of value $\frac{6.3}{0.2} = 32$ ohms when connected in series with a 6X5G across a 12 volt supply.

84/6Z4

INSTRUCTIONS: Punch holes where indicated, cut away this portion and file for reference guide.

13

BRIMARIZING . . . A scheme devised by BRIMAR for keeping repair lines on the move, a means whereby radio sets may be kept working happily in the home and not waiting on the shelf.

BRIMAR
RADIO VALVES

STANDARD TELEPHONES AND CABLES LIMITED, FOOTSCRAY, SIDCUP, KENT.

A SERVICE PLAN FOR PLANNED SERVICE

World Radio History

WE'D LIKE YOU TO KNOW —

simplicity WITH *efficiency*

IN FERRANTI TELEVISION

A major problem in the designing of television receivers has been to make satisfactory provision of scan generators — and more particularly, the horizontal scan generator.

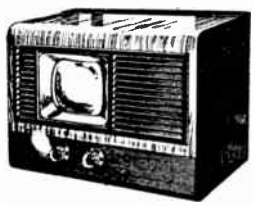
By making use of a number of valves the problem had been simplified somewhat, but it still has been the aim of designers to evolve the single valve generator. For a solution on these lines would not only lead to economy in design, but should result in really efficient operation. Ferranti television engineers have found a solution to the problem, and the single valve line time base is now an accomplished part of a Ferranti television circuit.

In practice it has proved that the single valve generator has a number of advantages over the conventional two valve generator. For instance, the grid behaves as an " efficiency diode " and gives 25% more power than the class "A" operated amplifier.

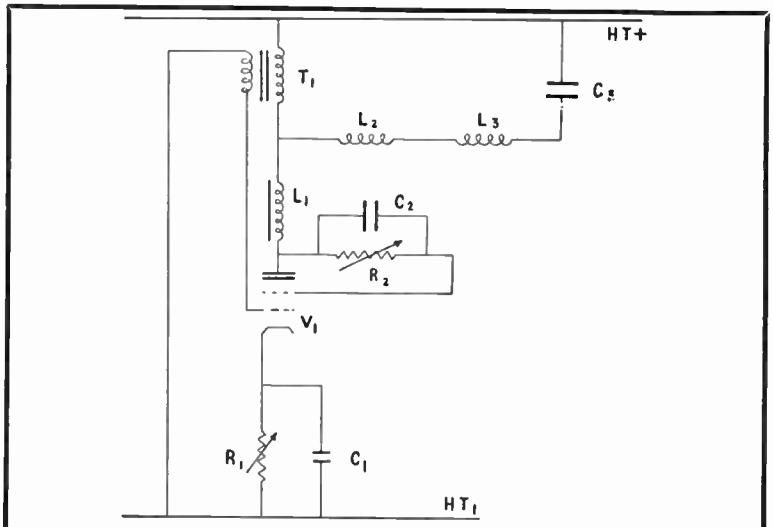
Again, owing to its highly inductive anode load the generator possesses inertia which can be likened to a flywheel in that it makes for stability, enabling synchronism to be held throughout the worst interference.

The biggest disadvantage resulting from the use of the single valve generator is the interdependence of controls, for it is difficult to control the amplitude without affecting the frequency. This difficulty, however, has been successfully overcome in the Ferranti circuit by a unique design. In this, the screen grid in a triode operated tetrode valve has been used to control the amplitude quite independently of frequency.

Thus, the single valve line time base generator is simplicity itself. And, as the number of components used is at a minimum, so set reliability is enhanced.



MODEL 1146 in bleached walnut and ebonised cabinet, with 7½" x 6" screen. High quality sound and vision performance. Vibrationless chassis mounting. Two-knob control. A.C. Mains only. Price £95.11.9 (inc. £24.1.9 tax).



TECHNICAL EXPLANATION

The scanning coils L2 and L3 provide an inductive load in the anode circuit of the valve V1. With the valve A.C. resistance, the circuit becomes an inductance and resistance in series. At the instant of switching on the H.T., current flows through this circuit increasing in value at a rate determined by the time constant of the circuit. To obtain a linear current change through the coils, the time constant must be much longer than the single stroke time. This is achieved by using scanning coils with a high inductance and a valve with a low A.C. resistance.

The oscillatory action is obtained by coupling the grid into the anode circuit, the frequency being controlled by R1 which determines the bias applied to the grid circuit. During part of the cycle, grid current flows, its direction being such that energy is restored to the scanning circuit, thereby improving the efficiency.

To linearise the trace, the choke L1 is included in the anode circuit. This choke saturates during the scanning stroke, modifying the rate of change of current through the scanning coils from an exponential to a linear trace.

The amplitude of the current change is controlled by the potentiometer R2 shunted by the condenser C2.

FERRANTI TELEVISION

Ferranti Ltd MOSTON MANCHESTER 10; & 36 KINGSWAY LONDON WC2

World Radio History

Progress in Components

Review of the R.C.M.F. Exhibition

THE annual private exhibition organized by the Radio Component Manufacturers' Federation was held this year from March 2-4. In the following pages we give a broad survey of the industry's productions in the main categories, together with a list of makers. A general list of exhibitors, with addresses, appears at the end of the review.

CAPACITORS

Fixed Capacitors.—One interesting feature of the capacitor display is the greater interest shown by manufacturers in the silvered mica and silvered ceramic forms of construction.

Further headway has been made in the development of ceramic capacitors for television and V.H.F. equipment. Physical size is generally vitally important in order to keep lead lengths short and this is being greatly helped by the more general use of ceramics with very high dielectric constants. It gives about a tenfold increase in capacitance for a given size of component.

Standard Telephones had an entirely new range of silvered mica types for working voltages of 350 and 750 D.C. and in capacitances of from 10 to 3,000 pF.

The introduction of two new sizes of moulding for both their silvered and stacked mica series by Dubilier will, it is claimed, simplify the choice of a capacitor and lead to a marked reduction in the different varieties hitherto produced.

The smallest of the new range is the type S635 and is quite a miniature. It is made in capacitances of from 5 pF to 1,500 pF in preferred values. The other model, the S672, is a larger moulding and is used for capacitances of from about 1,800 pF to 10,000 pF.

T.C.C. make this type of capacitor in moulded cases as well as wax protected and among other firms adopting this form of construction are British N.S.F., Hunt, Stability Radio and United Insulators. The last mentioned had a twin silver mica capacitor made in the form of an I.F. end plate with four eyeletted holes in the corners for soldering lead-through wires. A large and a miniature size is available from 40 to 250 pF.

Erie make use of a ceramic material called "Hi K" for some of their latest "Feed Thru" capacitors and so obtain capacitances up to 1,500 pF without increase in bulk.

Erie also had a new model described as the Post Ceramicon its main feature being that one connection is an internally screwed fixing bush and the other a lateral lead wire from the "live" element. It is intended to be mounted close to the valve-holders and provides a very short lead for cathode and screen by-passing. Two sizes are made, one up to 2,500 pF and the other up to 5,000 pF.

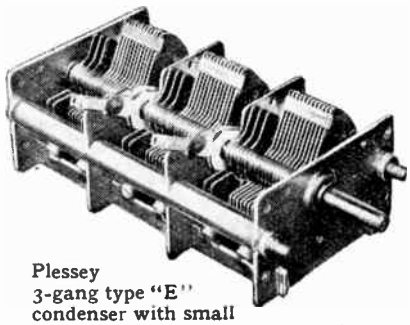
United Insulators had a new pattern lead-through insulator made also in normal and in high "K" ceramic. By the use of the latter its maximum capacitance is raised from 300 pF to 2,000 pF.

Other types of V.H.F. ceramic capacitors were a new button silvered mica model made by Erie for soldering to the chassis and the T.C.C. range of Micadisc capacitors for both receiving and transmitting apparatus. Dubilier had a lead-through bushing type among their long range of ceramic capacitors.

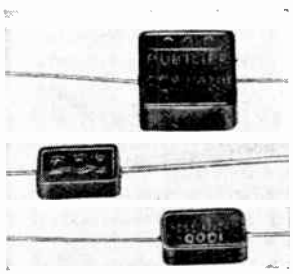
Electrolytics were shown in a profusion of capacitances, sizes and shapes and for every conceivable application. Special transmitting capacitors for which the ceramic "pot" form of construction is now largely favoured were seen among the exhibits of Dubilier, T.C.C., United Insulators, and Wego.

Variable Capacitors.—A new design gang condenser was shown by Plessey in which a tiny bandspread unit is embodied in each section. The rotor vanes are carried by the main shaft but stators are separately insulated. There are two- and three-gang types with either 10 pF or 60 pF bandspread sections and giving capacitance swings of 483 and 438 respectively.

Another Plessey innovation is the fitting of transparent dust covers

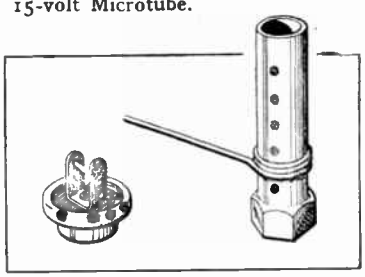


Plessey 3-gang type "E" condenser with small bandspread units in each section



Examples of the new moulded cases now used by Dubilier for their silvered mica and stacked mica capacitors.

Three of the latest T.C.C. electrolytic capacitors; a 32 μF plug-in model, an 8 μF Micropack and the 30 μF 15-volt Microtube.



Two examples of the latest V.H.F. by-pass capacitors made by Erie.

World Radio History

Progress in Components—
to their miniature "R" type.

Gang condensers with bandspread section of from 10 to 55pF were shown by Wingrove and Rogers (Polar), which firm also had some two-gang models with double spacing for the oscillator section as a means of combating condenser microphony.

Jackson Bros. have evolved a novel bandspread drive mechanism for ordinary gang condensers. It has dual pointers, coarse and fine slow-motion drives and separate but concentric spindles. The two ratios are 6 to 1 and 48 to 1 respectively. This provides a mechanical means of bandspread using standard variable capacitors. Short-wave capacitors, air and mica dielectric trimmers were also shown.

Precision type variable capacitors and many special types for high- and low-power transmitting and industrial heating apparatus were seen among the Cyldon exhibits. Square law, logarithmic law, linear frequency and capacitance are now available in most ranges. Rigid aluminium or brass frames are used with aluminium vanes and ceramic insulation.

A range of split stator transmitting capacitors for amateurs was shown by Labgear, a particularly well-made postage stamp type mica trimmer by Walter Instruments and air dielectric concentric trimmers by Mullard in sizes of 2 to 8 pF and 3 to 30 pF.

Makers*: Bird (FA, T, TX, V), British Electrolytic (E), B.I. Callenders (E, P), British N.S.F. (P, M), Bulgin (FA, T), Daly (E), Dubilier (C, E, M, P, T, TX), Erie (C, T), Ferranti (E, P), Fulham (C), Hunt (C, E, M, P, TX), Jackson (T, TX, V) Labgear (TX), London Electrical Manufacturing (C, M), Mullard (T), Plessey (T, V), Stability Radio (M), Standard Telephones (M, P); Static Condenser (P, TX), Telegraph Condenser Co. (C, E, M, P, T, TX), Telephone Manufacturing Co. (M, P), United Insulation (C, M, TX), Walter Instruments (T), Wego (C, M, TX), Welwyn (T), Wingrove & Rogers (V, T).

**Abbreviations*: C, ceramic; E, electrolytic; FA, fixed air dielectric; M, mica; P, paper; T, trimmers and preset; TX, transmitting types; V air dielectric variables.

RESISTORS

Fixed Resistors.—A considerable amount of research appears to have been devoted to the vitreous enamelled type of resistor mainly with the view to increasing the permissible loading with the sizes now in common use.

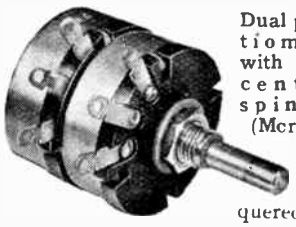
Painton has a new range which makes use of a ceramic tube of very high thermal conductivity and which is designed to allow for forced draft or even liquid cooling to be used. It is said that the surface of the enamel remains perfectly homogenous under the most exacting tropical conditions and does not develop fine hair-line cracks known as "crasing" which give a foothold for corrosion and fungoid growths.

Resistance values are normally available up to 100kΩ in sizes ranging from 2in to 9½in long. A 4-in size is claimed to dissipate 1¼kw without damage.

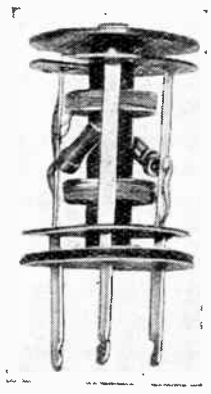
This pattern is also available with a low inductive winding and one use of this type is as the R.F. load for a transmitter. The limiting frequency is above 20Mc/s.

A new style resistor shown by British Electric Resistance (Berco) consisted of a crimped strip wound edgewise on a porcelain tube and secured by vitreous enamel. So far only low values are available but the method almost doubles the power rating for a given size.

Many examples of power-type wire-wound resistors, some lacquered and some vitreous enamelled, were shown by Bulgin, Erg, Goldsman and Welwyn. This style is used to a large extent as dropping resistors in A.C./D.C. sets, and they are fitted with suitably positioned tappings.



Dual potentiometer with concentric spindles (Morgan).



Interior of the Wright & Weaire miniature "round-can" I.F. transformer.

There are a number of circuit positions in quite ordinary apparatus where a resistor of nigh stability is very desirable. Hitherto this pattern has been regarded as rather specialized, but recent developments have placed it on a more general-purpose footing. High stability qualities are imparted by the method of manufacture, which basically consists of depositing a film of the finest possible carbon particles on an insulated rod, usually ceramic, although quartz fibre has been used by Welwyn for some special types.

This firm makes the high stability resistor in sizes ranging from ⅛ watt to 2 watts and up to 100MΩ. The standard finish is tropical-grade.

Dubilier recently added a ⅛ watt size to their high stability range which are available with either a varnish finish or insulated. They are made in preferred values up to 5.1MΩ.

There are four sizes in the Mullard series, ¼, ½, 1 and 2 watts respectively and resistance values up to 10MΩ are available.

A comprehensive range of carbon type resistors was shown by both Erie and Morgan. The smallest now made by Erie is a 1/10 watt. Resistors of quite low value are now readily obtainable in this style.

Variable Resistors.—Whilst minor improvements have been made in the design of volume control potentiometers there are no major changes to be seen in this year's display. Linear, logarithmic and semi-logarithmic types were shown in the standard size, approximately 1½in in diameter, and in miniature patterns.

The latter varied considerably in size, one of the smallest being the Morganite type BJ measuring just under ¾in yet dissipating 0.1 watt. This pattern has the contacts place on the back plate, which feature is embodied in several other Morganite models.

Bulgin make a range of wire-wound potentiometers with resistance values from 10Ω to 68kΩ in preferred values and of 3 watts rating. Among the other firms showing this type of component may be mentioned Dubilier, Erie, Goldsman and Plessey.

Colvern were showing a selection of wire-wound types in small sizes with and without switches and up to 100kΩ in value. These include single and two ganged models with separate concentric spindles or a common one. This firm also make a range of cam-corrected potentiometers for precision apparatus.

Ganged volume controls were shown also by Morgan Crucible, and

World Radio History

other examples of ganged units were included among the exhibits of Berco and Painton.

Berco variable potentiometers are all wire-wound and range in value from a single-turn slide wire of a fraction of an ohm to one of 300 watts rating. This firm now applies the vitreous technique to the construction of potentiometers thereby doubling the wattage rating.

Painton variable resistors are essentially of a precision character and consist largely of faders and attenuator controls for use in broadcast monitoring and high-grade public address equipment. An R.F. attenuator was shown also by Advance Components.

Makers*: Advance (A), Belling & Lee (S), British Electrical Resistance (P, R, V, W), British N.S.F. (P), Bulgin (P, W), Colvern (R, P), Dubilier (HS, S, V, W), Erg (V, W), Erie (C, P, S), Goldsman (P, S, W), Morgan (C, P, S), Mullard (HS), Oliver Pell (R, W), Painton (A, P, V, W), Plessey (P), Welwyn (HS, V, W).

**Abbreviations*: A, attenuators; C, composition; HS, high stability; P, potentiometer; R, rheostats; S, suppressors; V, vitreous enamelled; W, wire-wound.

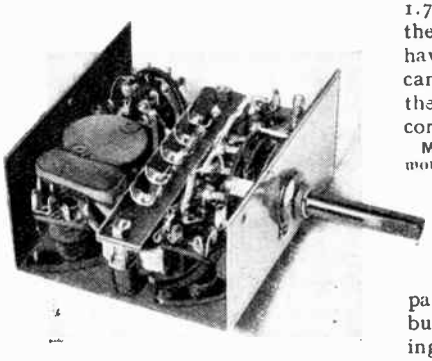
COILS AND TRANSFORMERS

R.F. Coils.—Signal- and oscillator-frequency coils fall into two categories—air-core and dust-iron core—which are about equal in numbers. The air-core types are usually wound on formers of about ½-in diameter and 1½-in length and are available with inductance values suitable for frequencies ranging from 30 Mc/s to 150 kc/s with the usual values of tuning capacitance. The iron-core types are smaller and in many cases the adjustable cores permit the exact matching of coils during the trimming of the set and so allow more accurate ganging to be achieved. Not all cores are adjustable, however, for in some types the cores are used as a factory adjustment for matching coils and are then sealed in position.

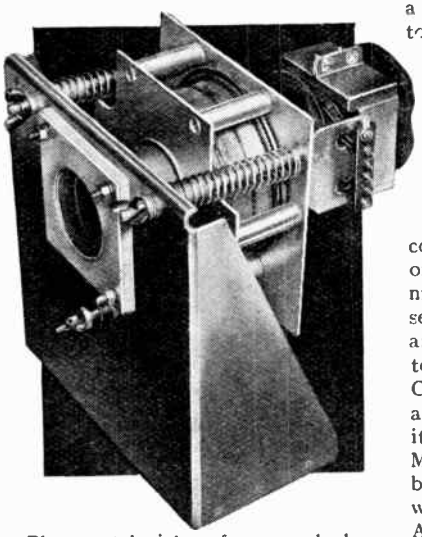
In addition to separate coils, quite a number of tuning units are made. These usually include the aerial and oscillator coils for three wavebands with switch and trimmers, and both Weymouth and Wearite have examples. Weymouth also showed a permeability tuner in which four dust-iron cores are attached to a plate and move together under the control of a cam.

Makers: Advance Components, Automatic Coil Winder, Labgear, Plessey, Radio Instruments, Weymouth, Wright & Weaire.

I.F. Transformers. — The intermediate frequency of broadcast receivers is now virtually standardized at 465 kc/s, or very close thereto. A typical transformer consists of a pair of wave-wound coils tuned by fixed ceramic capacitors and with adjustable dust-iron cores for trimming. The spacing between the coils is fixed and arranged in manufacture so that the coupling, which is mainly by mutual inductance, is at about the optimum value. Overcoupling is rarely adopted in view of the trimming difficulties which arise. In some designs there are two types, one for use between amplifier stages and one for coupling an amplifier to a diode detector. The latter has rather tighter coupling because of the damping imposed by the detector.



Weymouth type B.6 midget coil pack covering three wavebands.



Plessey television focus and deflector coils.

In addition to the so-called standard-size components (about 1½-in square by 2½-in high) there are many miniature types which have remarkably good characteristics. The Plessey M1, for instance, has a rectangular can measuring ⅛ in by 1.79-in high. It is for 465 kc/s and the coils have a Q of 80. Wearite have a model with a 1-in circular can which is 1½-in high and again the Q is 80. In both cases dust-iron cores are used for trimming.

Makers: Bulgin, Labgear, Plessey Weymouth, Wright & Weaire.

Mains and A.F. Transformers.—Most of the small mains and speaker transformers, typical of broadcast receiver practice are of the paper-interleaved type, and in all but the cheapest models the windings are impregnated The standard primaries of the mains type are tapped for 200-250 V and sometimes a voltage-adjustment panel is fitted to the transformer. In the Plessey types, for instance, both the solder tags and the snap-type connectors of the voltage adjustor are carried by a thin strip of insulation wrapped around the winding.

Some models, especially those for tropical use, are completely sealed. One example of this technique is the Parmeko "Mercury" model; it is sealed in a cylindrical copper can and designed to work in ambient temperatures from −40° to +100° C; it will also operate at an altitude up to 50,000 ft, so that it is suitable for aircraft use. Miniature sealed types were shown by Ferranti, who also had their well-known "A.F." series on view. Auto-transformers in sizes from 60 W to 250 kVA are made by Woden and, among a wide range of mains and A.F. transformers made by Partridge there is a modulation transformer rated at 45 W. It is tropicalized and has tapped primary (3/10 kΩ) and secondary (6/12 kΩ). This firm also showed a supersonic power transformer (300 W 50 kc/s).

Makers: Acoustic Products, Advance, Associated Electronic Engr., Automatic Coil Winder, Bulgin, British Communications, British Electric Resistance, Electro Acoustic, Ferranti, Labgear, Oliver Pell, Parmeko, Partridge Transformers, Plessey, Radio Instruments, Tannoy Products, Teledictor, Weymouth, Woden, Wright & Weaire, and most loudspeaker manufacturers.

Television Coils.—Deflector coils, focus coils, line and frame scan transformers and blocking oscillator coils appeared on the Plessey stand. The line-scan transformer is impregnated and contained in a cylindrical can packed with sponge rubber to reduce mechanical noise.

World Radio History

Progress in Components—

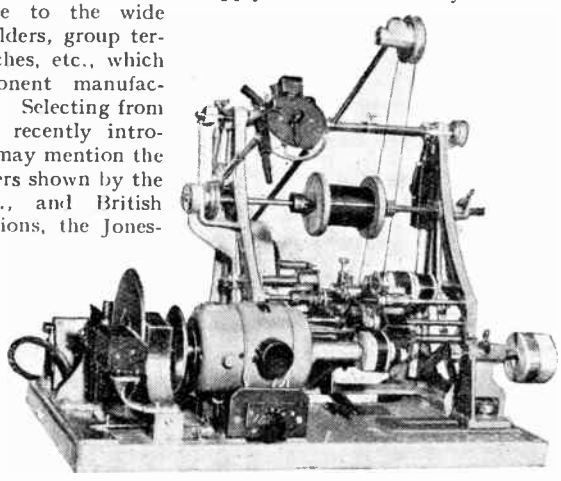
Coil Winders.—Machines for coil winding were shown by several firms and range from small hand-operated types to power-driven models for factory production. Among the latter, the Automatic Coil Winder "Macadie" is interesting for it is equipped with an automatic paper inserter.

Labgear were showing a hand-operated wave-winding machine of simple construction and capable of dealing with coils of up to 2½-in outside diameter. The traverse is operated by an adjustable friction-driven cam. Another wave-winder of the hand-operated type is the Neville's Winnipeg model.

Makers: Automatic Coil Winder, Labgear, Neville's.

CHASSIS FITTINGS

It is difficult in the space available to do justice to the wide variety of valve holders, group terminal boards, switches, etc., which the British component manufacturers have to offer. Selecting from some of the more recently introduced products we may mention the B8A and B8G holders shown by the Carr Fastener Co., and British Mechanical Productions, the Jones-type inter-chassis connectors made by Belling and Lee, a new push-button unit by A.B. Metal Products, the universal dial drive unit shown by Plessey and a range of Bulgin's jack switches suitable for bias checking, etc.



"Macadie" automatic coil winder made by Automatic Coil Winder and Electrical Equipment.

A range of heavy-duty telescopic chassis mountings similar to those used in Admiralty equipment were shown by Hallam, Sleigh and Cheston and are capable of carrying evenly distributed loads up to 250 lb for extensions up to 2ft.

Makers*: A.B. Metal Products (S), Antiference (PS), Associated Electronic Engineers (TB), Belling & Lee (C, CRH, FU, PS, T, VH, VT), B.I. Callenders (C), British Electrical Resistance (K, S), British Mechanical Productions (C, CRH, MS, P, PS, ST, T, VB, VH, VP), British N.S.F. (S), Bulgin (C, FU, G, J, K, L, MS, PS, S, T, VH, VT), Carr Fastener (C, CRH, E, F, FU, L, MS, PS, ST, VH, VP, VT), Colvern (TB), Electrothermal (S, VR), Imhof (CH, P), Jackson (D), Labgear (CH, MS, P, S, VH), Long & Hambly (PS, RM, TM, VR), McMurdo (K, VH), Oliver Pell (S), Painton (K, PS, S, SP, T), Plessey (C, D, L, PS, S, SP, VH), Radio Instruments (VH), Reliance Electrical Wire (C, RM), Ripaults (T), Salford (D), Standard Telephones (C, S), Taylor Instruments (T), Telegraph Construction & Maintenance (C), Telephone Manufacturing Co. (J, PS), Truvox (S), J & H. Walter (CH, P), Walter Instruments (S, SP), Wingrove & Rogers (D), Wright & Weaire (S).

**Abbreviations:* C, connectors, CH, chassis; CRH, cathode-ray tube holders; D, drives; E, eyelets; F, fasteners; FU, fuseholders; G, group boards; J, jacks; K, knobs; L, lampholders; MS, mounting strips; P, panels; PS, plugs and sockets; RM, rubber mouldings; S, switches; SP, scale pointers; ST, solder tags; T, terminals; TB, terminal blocks; TM, television masks; VB, valve bases; VH, valve holders, VP, valve pins; VR, valve retainers; VT, valve top connectors.

CONTACT RECTIFIERS

The usefulness of the well-known metal rectifier has been extended by the introduction of types of higher voltage rating and of smaller physical dimensions. The Westinghouse Type 36E11T is intended for the supply to a cathode-ray tube or apparatus of similar power requirements. It will supply an output of up to 0.5 mA and is available in sizes ranging from 1.47-in long (1,600 V peak inverse) to 11.6-in (19,200 V peak inverse). All types are of $\frac{7}{16}$-in diameter and are suitable for use with sine wave or pulse inputs of up to 50 kc/s. For really high voltages they lend themselves to the use of voltage-multiplying circuits. Heavier current types for lower voltages are suitable for receiver H.T. supply systems.

Standard Telephones & Cables showed selenium types. The E.H.T. models are of tubular construction and are rated up to 2 kV for single units for currents of 1 mA to 10 mA. There are also Uniplate rectifiers intended for the low voltages of telecommunication circuits.

Metal rectifiers also find application in instruments, and four different patterns were shown by Salford, ranging from 200 μA to 50 mA.

Makers: Salford, Standard Telephones, Westinghouse.

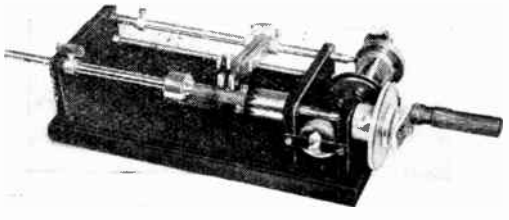
VIBRATORS

Synchronous and non-synchronous vibrators for receiver H.T. supplies were shown on several stands, as well as complete vibrator power-supply units. The Plessey model is unusual in being designed for a 2-V input, and an overall efficiency greater than 50 per cent is claimed. The elimination of rubber from the vibrator has made it possible to adopt silver contacts and, to reduce losses. The output is 10 mA at 90 V, and 6 V for grid bias is available.

Makers: Bulgin, Plessey, Wimbledon, Wright & Weaire.

AERIAL EQUIPMENT

Detail improvements have been made in the mechanical design of television and anti-interference aerials and their fittings, and some firms are catering for the requirements of amateur transmitting enthusiasts. For example, Antiference, Ltd., have introduced a 300-ohm dipole with parallel wire elements embedded in polythene. The span is marked for cutting to the required length for the 10, 20 and 40 metre amateur bands and the 11, 13, 16, 19, 25 and 31 metre broadcast bands. A matching transformer is available if the aerial is to be connected to a broadcast receiver with an unbalanced input. The aerial is rated for power loadings of 1.9 kW at 7 Mc/s and 0.9 kW at 30 Mc/s.



Labgear hand-operated wave-winding machine.

Makers: Antiference, Belling & Lee, B.I. Callenders Cables, Labgear, Reliance Electrical Wire, Ripaults, Standard Telephones, Telegraph Construction & Maintenance.

World Radio History

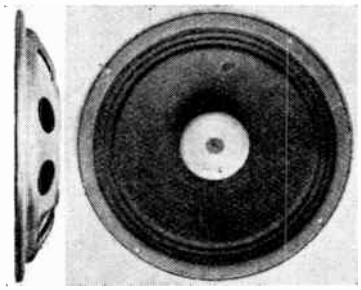
SOUND REPRODUCTION

Loudspeakers. — In the highly competitive field of loudspeaker units for broadcast and television receivers the centre-pole type of magnet continues to hold its own for flux densities up to 10,000 gauss. With the active material concentrated in a compact lump and surrounded by a return path of "soft" steel, this design is not only economical, but has a very small external field and does not cause deflection in adjacent C.R. tubes. For high-powered P.A. and quality loudspeakers requiring fluxes above 10,000 gauss, ring-type magnets using anisotropic materials are favoured. More manufacturers are introducing shallow designs with the moving coil reversed and the magnet contained inside the angle of the cone diaphragm.

In the R. & A. "700" series the leads from the voice coil consist of beryllium-copper strips sandwiched between corrugated fabric centring diaphragms.

A new 12-inch speaker by Acoustic Products makes use of two independent diaphragms with separate voice coils.

Notable examples of heavy-duty loudspeaker were shown by Goodmans and Truvox. Goodmans were also showing a matched pair of loudspeakers consisting of a 12in unit for bass and 8in for treble.

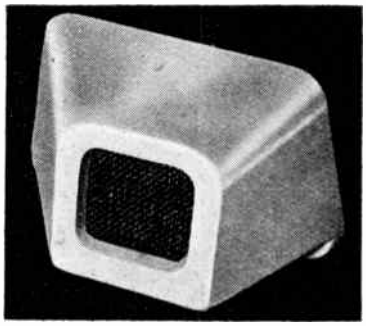


B.C.C. "Disc" loudspeaker.

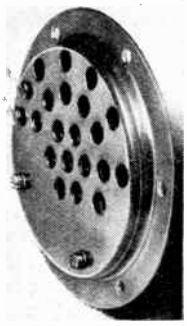
The Truvox 12in heavy-duty loudspeaker is available with either copper or aluminium speech coil, the former giving balanced reproduction up to 8,000 c/s and the latter up to 11,000 c/s.

At the other end of the scale several interesting miniature loudspeakers were noted. The B.C.C. 2½in "Disc" speaker Model M21 weighs 2oz and is only ⅝in thick. Even shallower is the Cosmocord (Acos) RE5, which is driven by a bi-morph crystal and is suitable for incorporation in miniature "personal" portables. A neatly designed midget cabinet speaker (Model CT117) was seen on the Celestion stand. The dimensions are 6¼in × 4¼in × 2¾in, and the Bakelite case is available in a variety of colours.

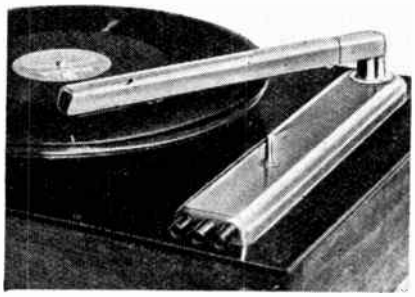
To meet the demand of Continental radio-gramophone manufacturers for a 12in loudspeaker at a low price, Celestion have also introduced the Model 44 which is successfully meeting foreign competition. The Model 44 has a 1½in voice coil and will handle 10 watts.



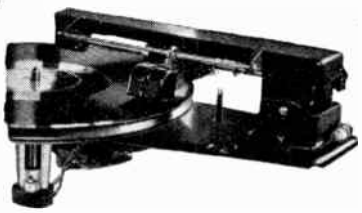
Celestion Midget loudspeaker.



Cosmocord Model R.E.5. piezo-electric loudspeaker.



Ferranti ribbon pickup.



Garrard Model S.A.1 record player with radial tracking mechanism.

Makers: Acoustic Products, Brit. Communications Corp., Brit. Rola, Celestion, Electro Acoustic Industries, Goodmans, Plessey, Reproducers & Amplifiers, Reslosound, Tannoy, Teledictor, Truvox, Vitavox.

Gramophone Equipment. — The trend of design of pickups continues to move in the direction of even lighter moving parts and the use of permanent sapphire styli. Pick-up manufacturers are keeping ahead of the requirements of wide frequency range recordings by designing ribbon movements capable of reproducing up to 18 or 20 kc/s.

A notable newcomer in this field is the Ferranti ribbon pickup which requires a vertical weight of only 5 gm (0.18 oz). The moment of inertia referred to the stylus tip is equivalent to a mass of 2.5 milligrams, and it is claimed that the pickup will track under accelerations of 1,000g. The stylus tip is elliptical and it is calculated that it will trace with low distortion wavelengths as short as 0.0012in, corresponding to a frequency of 17 kc/s at 78 r.p.m. and 5in diameter. An output of 3 mV per cm/sec is obtained in 0.1 MΩ. Naturally a pickup of this nature requires careful handling and an ingenious push-button mechanism has been devel-

World Radio History

Progress in Components—

oped for placing the pickup on 10in or 12in records.

Garrard have introduced an automatic single-record player (Model SA1) with a radial tracking mechanism. A switch mechanism in the motor spindle and another operated by the lid ensures that the motor does not start unless there is a record on the turntable and the lid is closed. The starting position of the pickup is automatically selected by the size of the record.

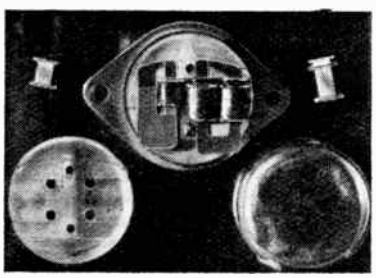
Makers*: Cosmocord (PU, RH), Garrard (M, PU, GU, RC), Plessey (PU, GU, RC), Radio Instruments (PU), Erwin Scharf (PU), Truvox (PU).

**Abbreviations*: M, motors; PU, pickups; RH, recording heads; GU, gramophone units; RC, record changers.

Microphones. — Moving coil and ribbon microphones predominate for P.A. work and among new designs noted were the Tannoy MR/421 ribbon and the range of moving coil types shown by Reslosound. Piezo-crystal microphones for use in hearing aid formed an important section of the Cosmocord exhibit.

Makers: Cosmocord, Reslosound, Tannoy, Vitavox.

Wire Recording. — A recording head designed for 0.004in diameter wire was shown by Associated Electronic Engineers. This consists of 0.020in Mumetal laminations with



Magnetic wire recorder head (Assoc. Electronic Engineers).

two gaps and coils for recording, playback and erasure. The wire runs in a slot cut longitudinally in the edge of the lamination and is designed to pass knots and joints without jamming.

MATERIALS

Ceramics. — Precision moulded ceramic parts were displayed in the customary profusion and included minute, almost microscopic, spacers for use in the construction of miniature valves.

Magnetic Materials.—The technique of powder metallurgy as applied to magnets was exemplified by exhibits of moulded "Ticonal" magnets by Mullard and "Alnico" by Murex. The process is economically justified for magnets weighing less than one ounce, and intricate designs can be made with greater facility than by casting.

Although no great changes were

Tannoy MR/421 microphone.

noted in the varieties of high-permeability laminated materials available, there seems to be a tendency for suppliers to undertake more fabrication in the way of complete laminated assemblies, screening, boxes, etc.

Insulating Materials and Sleeving. —The standard insulating materials were well represented and some *conducting* tape for internal screening in transformers was noted on the stand of H. D. Symons. The same firm was showing varnish-impregnated woven glass fabric sleeving with a dielectric strength of 25 kV/mm.

Cables.—Most of the R.F. cables used for television and developed from war-time experience were again shown, and several firms were providing special cables for use in car radio installations.

Solder. — Activated rosin-cored solders in a wide variety of alloys were shown. Enthoven provided a large diagram illustrating the relationship between melting point and the lead/tin ratio. A useful range of indicator wires for testing soldering bit temperatures has been introduced by Multicore, who were also showing their method of testing fluxed joints for corrosion under conditions of 100 per cent humidity and with A.C. or D.C. traversing the joint.

Makers*: Associated Technical Manufacturers (C, CO, IM, IS, PVC, W), B.I. Callenders (C, CO, PVC, S, W), Bray (CE), British Rola (L), Bullers (CE), De la Rue (IM, IS, W), Du Bois (S), Duratube & Wire (B, C, IM, IS, PVC, W), Enthoven (S), Hellermann (IM, IS), Long & Hambly (IM), Magnetic & Electrical Alloys (DC, L, M), Micanite & Insulators (IM, IS, V), Mullard (M), Multicore (S), Murex (M, MO, T), Plessey (DC), Reliance Electrical Wire (B, C, CO, PVC, W), Ripaults (C, CO, PVC, W), Salford (DC), Scott (L), Spicers (IM, IS), Standard Telephones (C, CO, PCV, W), Steatite & Porcelain (CE), Suflex (IS, W), H. D. Symons (IM, IS, V), Telegraph Construction & Maintenance (C, IM, IS, L, M, W), Telephone Manufacturing Co. (DC), Taylor Tunnicliff (CE), United Insulator (CE).

**Abbreviations*: B, braiding; C, cables; CE, ceramics; CO, cords; DC, dust cores; IM, insulating materials; IS, insulating sleeving; L, laminations; M, magnetic alloys; MO, molybdenum; PVC, polyvinyl chloride tapes, wires, etc.; S, solder; T, tungsten; V, varnished materials; W, covered wires.

List of Exhibitors

A.B. Metal Products, Ltd., Hatton Works, Feltham, Mddx.
Acoustic Products, Ltd., 50-58, Britannia Walk, City Road, London, N.1.
Advance Components, Ltd., Back Road, Shernhall Street, London, E.17.
Antiference, Ltd., 67, Bryanston Street, London, W.1.
Associated Electronic Engineers, Ltd., Dalston Gardens, Stanmore, Mddx.
Associated Technical Mfrs., Ltd., Vincent Works, New Islington, Manchester, 4, Lancs.
Automatic Coil Winder & Electrical Equipment Co., Ltd., Winder House, Douglas Street, London, S.W.1.
Belling & Lee, Ltd., Cambridge Arterial Road, Enfield, Mddx.
Bird, Sidney S., & Sons, Ltd., Cambridge Arterial Road, Enfield, Mddx.
Bray, Geo., & Co., Ltd., Leicester Place, Blackmans Lane, Leeds, 2, Yorks.
British Communications Corp., Ltd., Gordon Avenue, Stanmore, Mddx.
British Electrical Resistance Co., Ltd., Queensway, Ponders End, Mddx.
British Electrolytic Condenser Co., Ltd., 52, Vicarage Lane, Ilford, Essex.
British Insulated Callender's Cables, Ltd., Surrey House, Temple Place, Embankment, London, W.C.2.
British Mechanical Productions, Ltd., 21, Bruton Street, London, W.1.
British Moulded Plastics, Ltd., Avenue Works, Walthamstow Avenue, London, E.4.
British N.S.F. Co., Ltd., Ingrow Bridge Works, Dalton Lane, Keighley, Yorks.
British Rola, Ltd., Ferry Works, Summer Road, Thames Ditton, Surrey.
Bulgin, A. F., & Co., Ltd., Bypass Road, Barking, Essex.
Bullers, Ltd., 6, Laurence Pountney Hill, Cannon Street, London, E.C.4.
Carr Fastener Co., Ltd., Brantwood Works, Tariff Road, London, N.17.
Celestion, Ltd., London Road, Kingston, Surrey.
Colvern, Ltd., Mawneys Road, Romford, Essex.
Cosmocord, Ltd., 700, Great Cambridge Road, Enfield, Mddx.
Daly (Condensers), Ltd., West Lodge Works, The Green, Ealing, London, W.5.
Dawe Instruments, Ltd., Harlequin Avenue, Great West Road, Brentford, Mddx.
De la Rue Insulation, Ltd., Imperial House, 84, Regent Street, London, W.1.
Dubilier Condenser Co. (1925), Ltd., Ducon Works, Victoria Road, North Acton, London, W.3.
Du Bois Co., Ltd., 15, Britannia Street, King's Cross, London, W.C.1.
Duratube & Wire, Ltd., Faggs Road, Feltham, Mddx.
Electro Acoustic Industries, Ltd., Stamford Works, Broad Lane, Tottenham, London, N.15.
Electrothermal Engineering Co., Ltd., 270, Neville Road, London, E.7.
Enthoven, H. J., & Sons, Ltd., Croydon Works, 230, Thornton Road, West Croydon, Surrey.
Erg Industrial Corp., Ltd., 1021a, Finchley Road, London, N.W.11.

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Erie Resistor, Ltd., Carlisle Road, The Hyde, London, N.W.9.
Ferranti, Ltd., Hollinwood, Lancs.
Fulham Electrical Components, Ltd., 459, Fulham Road, London, S.W.10.
Garrard Engineering & Mfg. Co., Ltd., Newcastle Street, Swindon, Wilts.
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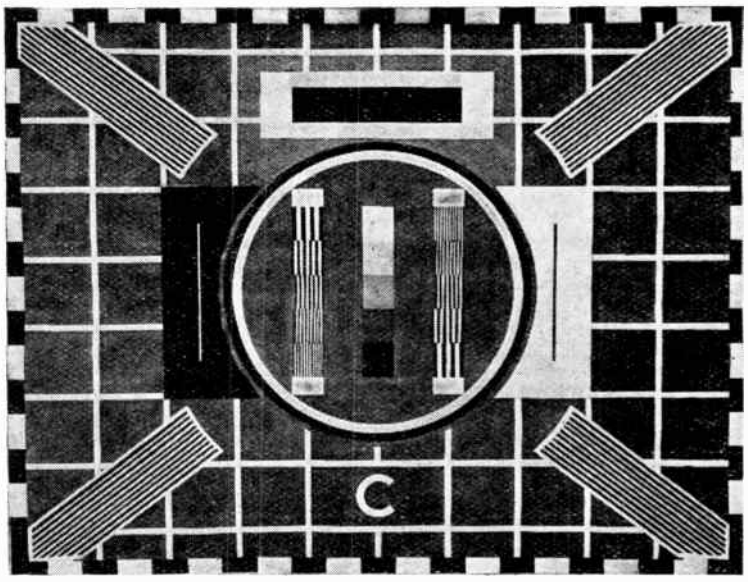
Television Test Pattern



The New "Card C"—Features and Notes on its Uses

These notes on the new test pattern being used by the B.B.C. in the morning transmissions from Alexandra Palace are based on data prepared by the British Radio Equipment Manufacturers' Association. The pattern is radiated each weekday for one hour from 10-11 *a.m.*

THE pattern is designed to approximate an average picture in mean signal level. The general background of the whole pattern is made mean grey to enable both positive and negative high-frequency overswing and similar effects to be observed at the correct setting of the brightness level and in the form in which they are usually most noticeable on picture transmissions.

Areas of mean grey background are left between all sections of the test pattern to enable following effects to be observed and in order to avoid, as far as possible, interference between different tests.

The main frequency- and contrast-range tests are confined to the area of the pattern within the centre circle where the focus quality should be a maximum. Subsidiary focus tests are provided in the corners of the pattern.

An outer border of black and white sections similar to that used

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Television Test Pattern—
in Test Card "A" has been retained.

High - Frequency Response.—The two frequency test patterns within the centre circle consist of five frequency gratings corresponding to fundamental frequencies of 1.0, 1.5, 2.0, 2.5, and 3.0 Mc/s. They are arranged vertically for ease of intercomparison and are provided with white reference areas at the top and bottom to aid in assessing the reproduced level of modulation in the grating. The two patterns are reversed vertically relative to each other to reduce effects of non-uniformity of cathode-ray tube focus and effects arising from other parts of the whole test pattern.

In use for receiver checking, referring to the left-hand pattern, the top three frequencies, 1.0, 1.5, 2.0 Mc/s, should certainly be resolved, and, in the later designs of receiver, the 2.5-Mc/s pattern also, although with reduced intensity of modulation. It is unlikely that significant resolution of the last pattern will normally be obtained since the frequency is outside the range for which most receivers are designed.

Focus Uniformity.—Additional diagonal frequency gratings are provided in the corners of the pattern and extend over that part of the picture area where focus variation is most significant. The equivalent horizontal definition of these gratings corresponds to a fundamental frequency of about 1 Mc/s and should, therefore, be well within the response of the amplifier circuits. The variation of cathode-ray tube focus, or optical focus in projection systems, over the picture area can, however, still be judged by observation of the sharpness of the lines of the gratings.

Linearity of Scan.—The majority of the pattern is covered by a white square grid on the grey background. This provides a means of judging scan linearity over the major part of the picture area for both directions of scan. In addition a more critical test of linearity over the central area is provided by a centre circle of slightly larger diameter than that on Test Card "A": the grid is, therefore, omitted from the area inside the circle.

For perfect linearity of scan the circle would be accurately circular and all the grid meshes square and equal in size. A close approximation to this can usually be obtained with present receivers.

Picture Aspect Ratio. — The pattern is surrounded by a border of alternate black and white sections, the length of each section being half that of the mesh of the linearity grid.

The outer edges of this border represent the boundaries of the transmitted picture and therefore have an aspect ratio of 5:4. Under correct scan amplitude adjustment these outer edges should just fill the receiver mask. In practice it may be found that it is not possible to fulfil this condition exactly with optimum linearity in the centre of the picture, as judged by the circle. In this case it is probably preferable slightly to overscan in either the horizontal or the vertical direction in order to maintain central linearity.

Synchronizing - Signal Separation.—The black and white border sections on the right-hand side of the picture, immediately preceding the line-synchronizing pulses, also afford a critical test of separation of synchronizing pulses from picture signal.

Incorrect adjustment of the synchronizing separator or limitation of frequency response in the vision channel will tend to cause horizontal displacement of parts of the picture information (e.g., the contour of the circle), corresponding to the positions of the black and white sections down the height of the pattern.

Contrast Range.—The central contrast wedge provides five tone values, varying between full white at the top to black at the bottom. It is not at present possible to specify the brightness of the intermediate tones exactly, but with satisfactory receiver operation they should all be reproduced as definite steps in brightness. It is expected that the characteristics of this wedge will be more exactly specified in the course of time.

For satisfactory receiver operation the Brightness and Contrast Controls should be adjusted so that the scan is just not visible on the black square and the white square represents the maximum brightness available from the tube at satisfactory focus quality. If one of the intermediate tones is missing, or the grading appears unequal, it will in general be necessary to reduce the contrast, and reset the brightness to give the correct black level.

Pulse Response and Spurious Echo Signals.—Two vertical bars, one white and the other black, of about 0.25-μsec width, are provided on either side of the centre circle. These provide in effect a pulse test of the whole system and enable the response to isolated detail approaching the maximum resolution of the system to be judged.

In addition these bars provide a means of checking the presence of spurious reflection signals, such as those arriving at the aerial by multipath transmission.

Low - Frequency Response.—Amplitude and phase distortion at the low-frequency end of the video spectrum give rise to background shading over the picture area in the form of horizontal streaking effects. Such effects, however, are infrequent as a form of receiver distortion and could only occur where one or more stages of video amplification, with unsuitable L.F. time constants, are employed, or through faulty D.C. restoration. It is, however, more likely to occur at the transmitter due to the difficulty of maintaining accurately a perfect L.F. response of the transmission system.

An adequate test for practical purposes is provided by the black bar on a white ground positioned above the centre circle and the black and white areas on either side of the centre circle.

Miscellaneous. — The grid pattern has been made to correspond to full white signal in order to provide an additional check on the variation of focus quality over the picture area at maximum cathode-ray tube modulation.

For this purpose, the lines of the grid have been made as narrow as permissible without appreciable introduction of the interference effects on horizontal lines, inherent in the line scan process.

The centre circle has been divided radially into black and white sections in order to provide all possible boundary conditions between white, mean grey and black.

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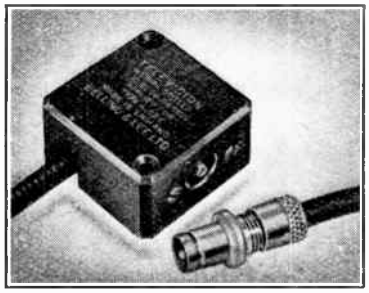
THE "BELLING-LEE PAGE"

Providing technical information, service and advice in relation to our products and the suppression of electrical interference



*1. Television outlet box *L624*.

TELEVISION OUTLET BOX

The Belling-Lee television coaxial outlet box **L624***1 (illustrated above) is for skirting board termination of ⅛in. to ¼in. diameter coaxial feeders (Uniradio 32 or "Belling-Lee" **L600***6) and the outlet socket will take any of our new range of coaxial plugs.

The metal braiding of the incoming feeder is connected between the cable clamp and casing, while the inner conductor is taken to a screw terminal on the central stem of the output socket.

BURNT-OUT "ELIMINOISE" TRANSFORMERS

As we have had a few more cases of these transformers being returned to us "burnt-out" we feel no apology is required for repeating question and answer No. 36 which appeared in "Wireless World," March, 1947.

When a transformer does "burn-out" in this way, we can accept no responsibility, as any aerial would become alive in the same circumstances and therefore the receiver is in a very dangerous condition and should not be used until the isolating capacitor has been replaced by a dealer.

Question 36: *Can an "**Eliminoise**" receiver transformer be "burnt-out"?*

Answer 36: It is surprising how many people in the trade—and out of it—do not realise that this can happen until the possibility is pointed out to them—then the reason seems obvious. It invariably happens with AC-DC sets, in which the design allows the chassis to be alive at mains voltage, with respect to earth If an earth terminal is fitted, it should be connected to chassis via a capacitor, thereby isolating the chassis. Unfortunately, some manufacturers omit the earth connection altogether; in other cases the earth capacitor breaks down.

When an "**Eliminoise**"*4 aerial is used in these circumstances, the receiver "**Eliminoise**" transformer is earthed. If there is no capacitor (or one that has broken down) between earth and chassis, or between aerial and chassis, current from the chassis flows through the "**Eliminoise**" coil and may burn it out.

Unfortunately, there are AC-DC sets where the aerial becomes alive through the same cause, and should the aerial fall down on a garden or metal clothes line, the results might be disastrous.

AIRCRAFT AND TELEVISION

It is now generally known that a television signal can be reflected from an aircraft flying in the vicinity of a domestic viewer, and that the resulting "echo" appears on the television tube as an interference in the form of a flutter.

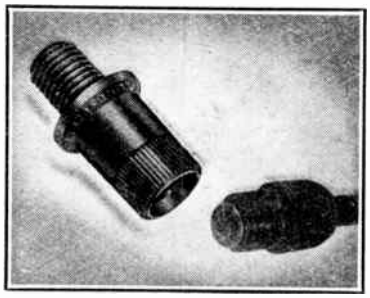
We have learnt that the "Belling-Lee" Inverted "V" television aerial **L606***2 is particularly sensitive to this form of interference and therefore is not recommended for use in districts close to busy airfields where aircraft are continually making circuits. In such locations a simple dipole such as **L501***5 or preferably dipole and reflector **L502** is to be recommended.

IGNITION INTERFERENCE SUPPRESSORS

The "Belling-Lee" suppressor **L630***3 (shown above) is designed to obviate car ignition interference with television and to fit in the H.T. lead from coil to distributor.

The use of this suppressor eliminates the cutting of the lead, by screwing into most makes of distributor caps or coil cans after the H.T. Lead terminal has been removed. The latter is then screwed into the top of the suppressor.

With distributors or coils where the screw-in connections are not employed a different suppressor is required, type **L1274.** With this type the H.T. lead has to be cut, preferably near the distributor, and the cut ends then screwed into the ends of the cylindrical suppressor. No tools are required other than that to cut the lead.



*3. A new version in ignition interference suppressors *L630* manufactured by Belling & Lee Ltd., designed to fit in "distributor caps" or "coil cans." List Price *1/6* each.

Wholesalers, retailers and manufacturers can do a lot towards helping the campaign to suppress car interference, by making provision for their own employees and customers to fit suppressors to their cars. All "Belling-Lee" vehicles and those owned by our employees have been dealt with, and we understand that the B.B.C., R.I.C., and many publishers of motor and radio trade journals have done likewise.

The success of television may be seriously affected if potential television viewers encounter car ignition interference at the time of demonstration, and it should be made known to those that object (not being owners of television sets) to fitting a **1/6** suppressor to their cars, that any improvement in television reception will increase its popularity, create a greater demand for sets and bring down the prices, making everybody a potential buyer.

It is the task of the Industry to do everything possible to aid the campaign.

*1. Television outlet box **L624.**

*2. Inverted "V" aerial **L606, £4 10s.** For attic or loft **L605, £2 12s. 6d.**

*3. A new version in ignition interference suppressors **L630** manufactured by Belling & Lee Ltd., designed to fit in "distributor caps" or "coil cans." List Price **1/6** each.

*4. "**ELIMINOISE**" Regd. Trade Mark, **L308/K, £6 6s.**

*5. "**VIEWROD**" Regd. Trade Mark.

*6. **L600, 1/6** per yard.

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The type JCF/200 unit illustrated above is representative of the wide range of vacuum type units available for low and medium frequencies.

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A. C. Bridges

Their Principle of Operation in Terms of Vectors

By "CATHODE RAY"

FOR some reason unknown to me, books that discuss or explain A.C. bridges seldom make much use of vectors for

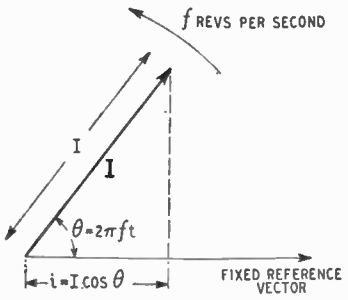


Fig. 1. I is a rotating vector representing a current of I amps at a frequency f c/s. The instantaneous value, i, at any time, t secs, after the start from the fixed reference, is given by I cos $2\pi ft$. Although this is the basic principle of vectors as applied to A.C., fixed vectors showing either peak or R.M.S. values are almost invariably used.

the purpose. If vectors are used at all, they are brought in rather half-heartedly. This seems strange, because it is only with the help of vector diagrams that I can follow A.C. bridges at all clearly. My remarks on j, the month before last, may have helped to get the thin end of the vector home among any who had hitherto shied at it. So now (mixing the metaphor still more) it may be a good opportunity to kill two birds with one stone —to help readers who are hazy about bridges, and to give an unhackneyed example of the use of vectors.

Just a few words of recapitulation. For the full story, consult the appropriate books.

An alternating current can be represented by a vector rotating at the frequency of the current. The length of the vector represents the peak value of the current, and its angle with some fixed vector (generally one pointing at 3 o'clock) represents the instantaneous phase angle (θ) of the current (Fig. 1). The instantaneous strength of the current is represented by the projection of the rotating vector on the fixed reference vector. In other words, if I is the peak current and f its frequency, the length of the current vector should be I units to some convenient scale, and it should be imagined as rotating anticlockwise at f revs per sec. The instantaneous phase angle, t secs after the start, is then $2\pi ft$ radians. And the instantaneous current, i, is I$\cos\theta$. The vector itself is denoted by **I**, as distinct from I which is the numerical strength of the current irrespective of phase. (One may not always trouble the printer to bring out special type when the vectorial nature of the quantity

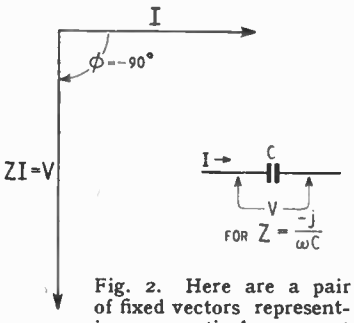


Fig. 2. Here are a pair of fixed vectors representing respectively current and voltage in and across an impedance consisting solely of capacitance. Current leads (i.e., is more anticlockwise than) voltage by 90°.

is obvious—as in Fig. 4 onwards—or unimportant.)

Generally we are not very much interested in the instantaneous values or phases, but we are interested in the peak value (or R.M.S. value, which is 70.7 per cent as large) and the phase of the current relative to other currents or voltages. So instead of making ourselves dizzy by trying to visualize the vectors

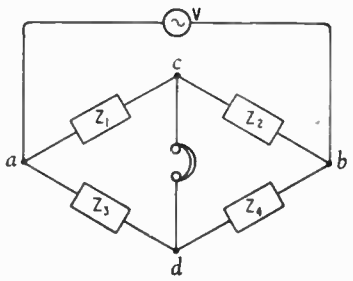


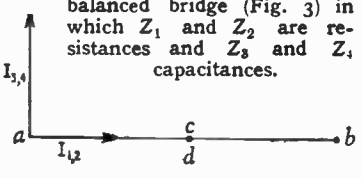
Fig. 3. Basic form of A.C. bridge.

all rotating at high speed, we freeze their motion and can then observe their relative phases. This is only possible, of course, if they are all rotating at the same speed; i.e., represent currents and voltages of the same frequency.

Given the current, the voltage across it is obtained (according to the extended Ohm's Law) by multiplying by the impedance. On the vector diagram the voltage vector is derived from the current vector by operating on it with the vector operator **Z**, which, as was explained in the February issue, is R + jX. Take the case of a purely capacitive circuit, in which **Z** = $-j/2\pi f$C or $-j/\omega$C. The voltage vector is obtained by multiplying the current vector by $1/\omega$C and rotating it $-j$, which is one right-angle backwards (i.e., clockwise), as in Fig. 2. As can be seen, this illustrates the well-known statement that a capacitive current leads the voltage by 90°.

In a purely inductive circuit the V vector would, of course, have to be turned in the opposite

Fig. 4. Vector diagram for balanced bridge (Fig. 3) in which Z_1 and Z_2 are resistances and Z_3 and Z_4 capacitances.



direction (+j), making it point vertically upwards, and it would

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be ωL times as long as the I vector.

The effect of resistance is to make the relative phase angle, ϕ, less than 90° or $\pi/2$.

Just as Ohm's Law can be extended to include A.C. circuits, by substituting **Z** for R, so the principle of the original Wheatstone Bridge, intended for D.C., can be extended to include the great variety of A.C. bridges having the same general circuit (Fig. 3). The condition for balance is $\mathbf{Z_1Z_4 = Z_2Z_3}$. When that happens there is no current through the detector, which means that the points *c* and *d* are at the same potential. Incidentally, so far as this condition for balance is concerned it makes no difference if the signal source and the detector (represented in Fig. 3 by a pair of phones) are interchanged. That is not to say it makes no practical difference which goes where; there are at least two things that may decide a choice. One of them has to do with stray capacitances, and the other with impedance matching; but at present we are considering only the main principle, not these side lines.

The interesting thing about A.C. bridges is that not only can resistance be measured in terms of resistance (as in the D.C. prototype), or capacitance against capacitance, or inductance against inductance; it is possible, and often very convenient, to measure any of these elements in terms of one of the others. Or one may wish to measure impedance in

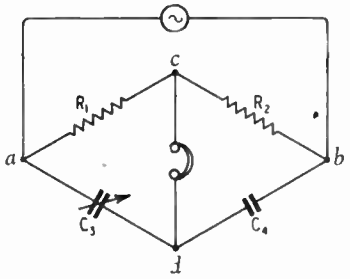

Fig. 5. Circuit diagram of bridge corresponding to Fig. 4.

general, in the $R + jX$ form. When measuring L and C, we generally want to know the resistance too, either directly or as a power factor or "Q." In fact, that is often more interesting than L or C itself.

To cover all sorts of measurement, dozens of variations on the main bridge theme (Fig. 3) have been devised. The question at the moment is to find the guiding principle which explains the whole lot, so that there will be no need to learn each one separately from scratch. For example, if it is desired to measure inductance in terms of a known fixed capacitance and resistances (fixed and variable), in which arms should they go?

Our starting point, or rather pair of points, is the applied voltage, which acts between *a* and *b*. So we can make the distance *ab* in Fig. 4 represent this voltage. It is applied to two paths in parallel—$Z_1 + Z_2$ and $Z_3 + Z_4$. Since we are assuming a balanced bridge, *c* and *d* are at the same potential, and the cross path through the detector can be left out of account. So there are two currents; one through Z_1 and Z_2 and equal to $\frac{\mathbf{V}}{\mathbf{Z_1 + Z_2}}$, and the other through Z_3 and Z_4 and equal to $\frac{\mathbf{V}}{\mathbf{Z_3 + Z_4}}$.

Our too-brief recapitulation said nothing about *dividing* by an impedance operator. But it is quite easy. The process is just the reverse of multiplying. To derive the current vector from the voltage vector, divide by the magnitude of the impedance, and rotate it in the direction opposite to multiplying. (The latter part is obvious vectorially; but in

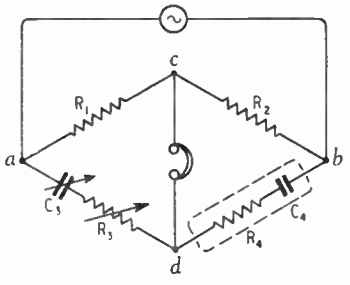

Fig. 6. Capacitance bridge with provision (R_3) for measuring capacitor loss (R_4).

case it doesn't seem quite what one would expect algebraically, note that $1/j = j/j^2 = j/-1 = -j$).

For some of the simpler types of bridge one need not even bother about currents. There is no need to, if the two impedances in series in each path have the same phase angle; that is to say, if both Z_1 and Z_2 are pure resistance or reactance or have the same proportion of both. Similarly for Z_3 and Z_4. The reason is clear from the diagram, Fig. 4. If the voltages across Z_1 and Z_2 (or Z_3 and Z_4) are in the same phase, their vectors must both be in the same direction, so the potential of the point *c* must lie on the straight line *ab*, dividing it into two parts proportional to Z_1 and Z_2 (or Z_3 and Z_4).

Take Z_1 and Z_2, and suppose they are equal. Then (as the same current flows through both) the voltages across them must be equal, so the potential across them must be represented by the midpoint, *c*, in Fig. 4. The current vector may be anywhere from − 90° to + 90° from *ab*, depending on whether Z_1 and Z_2 are pure

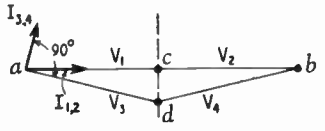

Fig. 7. Vector diagram for bridge which is unbalanced, although $Z_3 = Z_4$, because Z_4 includes resistance (represented by V_4 not being at right angles to $I_{3,4}$), while Z_3 does not.

resistance, or pure reactance (of either kind), or a mixture. If pure resistance, the current is in phase and lies along *ab*, as for example $I_{1,2}$. Now for balance *d* must coincide with *c*, so obviously Z_3 must be equal to Z_4. And both must have the same phase angle. But there is no need for it to be the same phase angle as in Z_1 and Z_2. It might be 90° leading, as shown by $I_{3,4}$. Notice, too, that there is no need for $I_{3,4}$ to be equal in strength to $I_{1,2}$.

The completed diagram, Fig. 4, corresponds to the common and quite useful De Sauty capacitance bridge, Fig. 5. If $R_1 = R_2$, then for balance the reactance of C_3 must equal the reactance of C_4, so $C_3 = C_4$. And so for other ratios than 1 : 1 (but remember that $\frac{C_3}{C_4} = \frac{R_2}{R_1}$, not $\frac{R_1}{R_2}$, because X_C is proportional to $\frac{1}{C}$!). C_3 may be a standard against which C_4, the

World Radio History

unknown, is compared. If C_4 has appreciable loss, its effect is the same as if there were a resistance in series (R_4 in Fig. 6). So it is necessary to put equal (assuming $R_1 = R_2$) resistance in series with

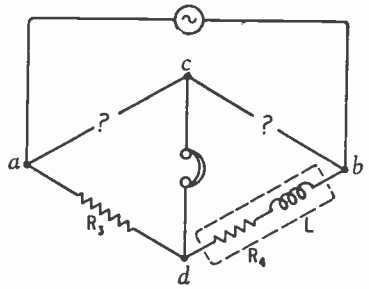

Fig. 8. If inductance is to be measured in terms of resistance and/or capacitance, how should they be arranged in arms 1 and 2?

arm 3. It is not enough just to make the impedance of arm 3 numerically equal to that of arm 4. For suppose that while Z_3 was (quite correctly) equal to Z_4, Z_3 was a pure capacitance but Z_4 included some resistance. The path $Z_3 + Z_4$ as a whole would therefore have some resistance; i.e., in the vector operator equation $\mathbf{Z}_3 + \mathbf{Z}_4 = R + jX$, R would *not* be zero, and therefore there would be a component in phase with the voltage as well as one at right angles. So when the voltage vector was divided by $\mathbf{Z}_3 + \mathbf{Z}_4$ to give the current vector, its angle with *cb* would be less than 90°, as perhaps in Fig. 7. Considering now the separate voltages across R_3 and R_4; as Z_3 is a pure capacitive reactance, V_3 must be at right angles to the current through it; $I_{3,4}$, as represented by *ad*. So *d*, although midway between *a* and *b*, no longer coincides with *c*, and the bridge is out of balance. The effect of inserting some resistance into arm 3 is to reduce the angle between $I_{3,4}$ and V_3; when V_3 is in line with V_4, then $R_3 = R_4$. The effect of varying C_3 is to shift point *d* horizontally along *ab*, and the effect of varying R_4 is to shift *d* vertically. An out-of-balance due to C_3 being wrong cannot be compensated by any possible adjustment of R_3. Just as the label "*j*" keeps X in a separate compartment from R in all calculations, so they work separately in actual measurements. Which means that a bridge of this kind enables **Z** (i.e., $R + jX$) to be measured; not merely Z.

As a matter of fact, the value of C_3 (and therefore C_4) is usually known as a capacitance, not as a reactance, though of course the reactance X_C can easily be derived for any particular frequency, because it is $1/2\pi fC$. That raises another interesting point. Suppose the generator produces a signal with more than one frequency. It might be an oscillator with strong harmonics. The C_3 and C_4 have more than one reactance at the same time. That is all right if there is no resistance, because the various pairs of reactances are all in the same ratio. So one can use a buzzer or other A.C. source with a poor waveform. (There is a possible slight qualification if either C_3 or C_4 varies appreciably with frequency). It is all right even if there *is* resistance, provided that the ratio of resistances is the same at all the frequencies. Since the standards will generally be designed to have the same C and R at all frequencies, any variability of the unknown with frequency will make the bridge unbalanceable unless either the source has a

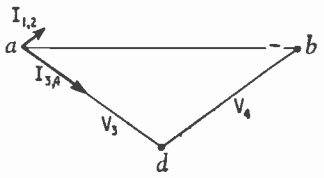

Fig. 9. Diagram for Fig. 8, showing a possible current vector which would enable arms 1 and 2 to balance 3 and 4.

pure waveform or the detector can be made to ignore all but one frequency.

So much for C and R. How about L? The same argument holds good for L as for C; but in practice it is generally difficult and inconvenient to provide a standard inductor. Whereas a standard capacitor can be made to have negligible R for most purposes, an inductor inevitably has a substantial amount of R in itself, so if the coil to be measured happens to have less R it is impossible to balance the bridge. That is why various types of bridge have been devised to measure L in terms of the more convenient standards of C and R. And that is also where vector diagrams are particularly helpful.

It is quite clearly impossible to balance an inductive arm 4 by a capacitive arm 3, because the voltages across L and C in series are

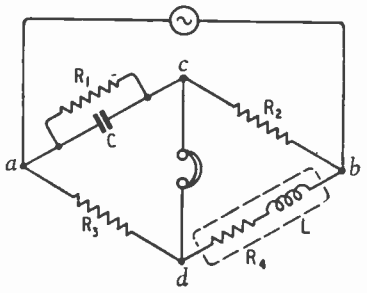

Fig. 10. Derivation of a bridge (Maxwell) from Fig. 9.

in opposition and certainly can never be brought into line along *ab*. The solution is to make *c* and *d* coincide off *ab*. Suppose the inductive unknown in arm 4 is balanced by a resistance in arm 3, as in Fig. 8. The path *adb* as a whole is inductive, so *j* is positive; dividing by $+j$ is the same as multiplying by $-j$, so the current vector $I_{3,4}$ lags the voltage across *ab*, as shown in Fig. 9. The voltage V_3 across R_3 must be in phase with the current; which gives the direction of V_3; and assuming for simplicity that $Z_3 = Z_4$, the position of *d* is fixed equidistant from *a* and *b*.

How now do we make point *c* coincide with *d*? It can be done of course, by making arms 1 and 2 identical with 3 and 4; but we are trying to avoid another inductive arm. If the Z_1Z_2 path is capacitive, $I_{1,2}$ must be leading, as in Fig. 9. And if arm 1 is all resistance it is in phase with $I_{1,2}$, which is no good. The arm in phase with $I_{1,2}$ must coincide with V_4; it must be arm 2. If then arm 1 is capacitive, so that $I_{1,2}$ leads the voltage across it (V_1), there should be no difficulty in making V_1 coincide with V_3. Inductance in one arm, therefore, can be balanced by capacitance in the diagonally opposite arm.

The result is the Maxwell bridge (Fig. 10) for balancing C against L. It should be quite an easy extension of the above reasoning to show that the resistance in arm 4 can be balanced by resistance in arm 1. This R_1 is usually connected in parallel with C as shown.

World Radio History

A.C. Bridges—

If L = o and C = o, it simplifies down to an ordinary Wheatstone bridge, in which $R_1R_4 = R_2R_3$, and *c* and *d* lie on *ab*. The effect of C and L is to move points *c* and *d* respectively off *ab*. Because C is in parallel with R_1 it is not very easy to work out the balance relationship between L and C from the vector diagram, even although the relationship itself is about as simple as it could be ($L = CR_2R_3$) and the $R_1R_4 = R_2R_3$ relationship is unchanged. To prove this by algebra will give you some practice in the use of *j*. You start with $\mathbf{Z_1Z_4} = \mathbf{Z_2Z_3}$ and substitute the appropriate $R + jX$ throughout, remembering that, in arm 1, R and X are in parallel, and that the *j* terms and the *j*-less terms can be separately equated.

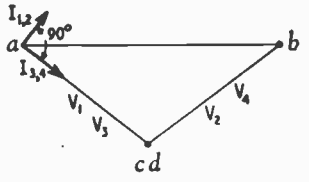

Fig. 11. Alternative current vector $I_{1,2}$ for balancing arms 3 and 4 in Fig. 8.

An advantage of the Maxwell bridge is that frequency does not come into the balance condition, so one need not be very particular about the waveform of the signal source. But a disadvantage is that if you adjust R_2R_3 you affect the balance for both R_4 and L; so if you are in balance for one and not for the other, any further adjustment will throw the bridge out of balance for whichever was right. This little peculiarity makes it a rather exasperating bridge to use.

So let us examine just one more bridge by the vector method. We have seen that what is wanted in the *acb* path to balance inductance in arm 4 is a turn to the left in the vector diagram on passing from arm 1 to arm 2. The obvious but unpractical way is to make arm 2 inductive to match arm 4. The Maxwell way is to make arm 1 *less* inductive, i.e., capacitive. Still another way is to start off with arms 3 and 4 (inductance in 4) and assume that arms 1 and 2 balance it. If the two currents are in phase we get the inductive arm 2, already rejected. But try shifting $I_{1,2}$ 90° clockwise (Fig. 11). As the current now leads the

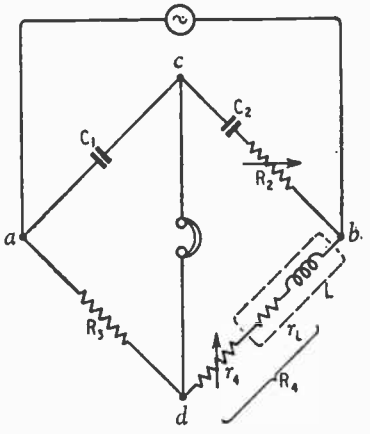

Fig. 12. Derivation of a bridge (Owen) from Fig. 11.

voltage by 90° in arm 1, Z_1 must be purely capacitive. And with no L in arm 4, Z_2 would have to be capacitive too, i.e., Fig. 5 upside down. With Z_4 purely inductive, Z_2 would have to be all R. So C_2 balances R_4 and R_2 balances L_4—a very convenient arrangement known as the Owen bridge (Fig. 12). Generally L is balanced by a variable R_2 and its resistance r_L by a reduction in r_4.

The condition for balance in the Owen bridge can be worked out by the *j* method (very easy this time because everything is in series), or from the vector diagram by analysing V_2 and V_4 into their in-phase and 90° components. This is done by producing *ac* to *e* where *aeb* is a right angle (Fig. 13). Then *ce* represents the part of V_2 that is at right angles to the current, $I_{1,2}$, and therefore reactive, $(I_{1,2}X_2)$. It also represents the part of V_4 that is in phase with $I_{3,4}$, and therefore resistive $(I_{3,4}R_4)$. Similarly for *eb*. So we get the proportion

$$\frac{R_3}{X_1} = \frac{R_4}{X_2} = \frac{X_4}{R_2}$$

or $$R_3\omega C_1 = R_4\omega C_2 = \frac{\omega L}{R_2}$$

The ω's cancel out, leaving

$$L = R_2R_3C_1$$

$$R_4 = R_3\frac{C_1}{C_2}$$

So $$r_L = R_4 - r_4 = R_3\frac{C_1}{C_2} - r_4.$$

As with the Maxwell bridge, frequency does not come into the matter; but unlike the Maxwell bridge the adjustments for balancing L and r_L (by R_2 and r_4 respectively) are quite independent, and it is an easy bridge to adjust. Moreover, variable resistances are the easiest accurate standards to provide for a wide range of values. And C_1 and C_2, being fixed, can be made much larger than C in the Maxwell, so that their reactances match the other impedances of the bridge better and are less affected by

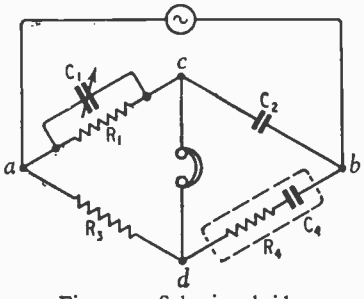

Fig. 14. Schering bridge.

stray capacitances. Only one of them need be an accurate standard. So altogether it is a very satisfactory type of bridge.

When once the idea of the vector diagram has been grasped, one need never be in doubt about what arrangements of bridge arms are capable of balance, and which element in one arm balances any other in any other. It also gives one a helpful picture of the *j* algebra processes. If you are interested, try the Schering bridge next (Fig. 14). It is a valuable one for measuring the losses in capacitors, especially at high voltage.

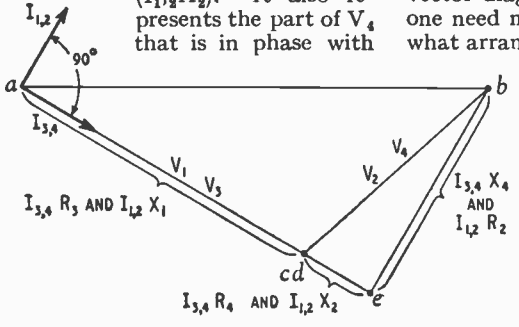

Fig. 13. Completed Fig. 11, showing geometrical construction for discovering conditions of balance in Owen bridge.

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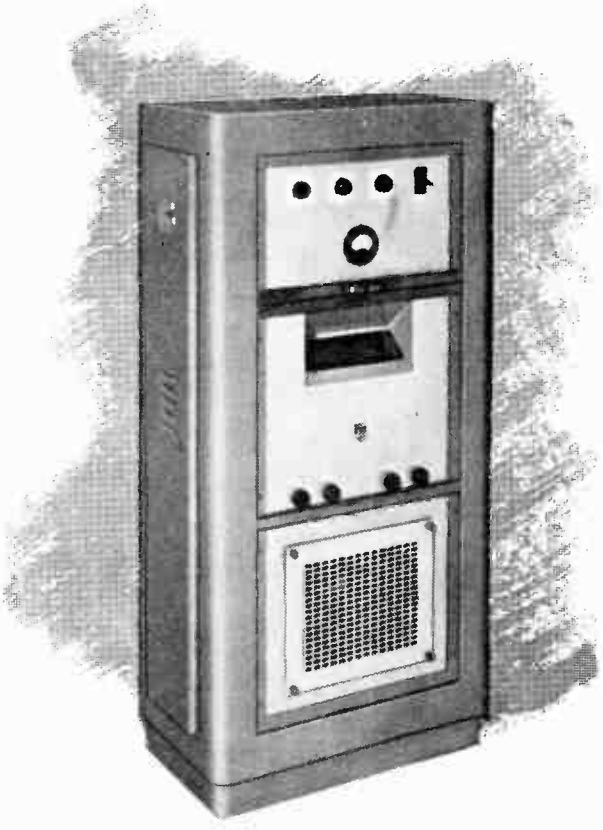

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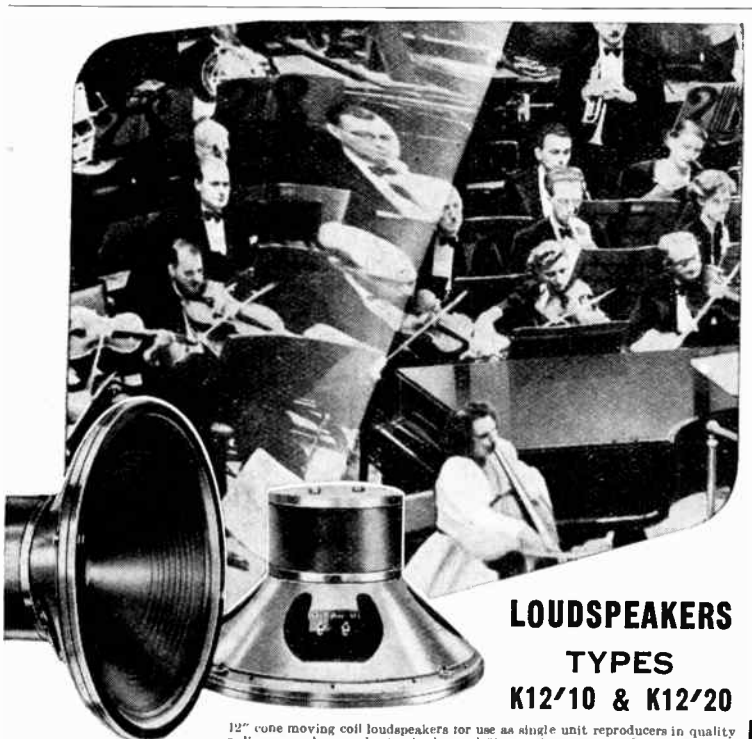

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WORLD OF WIRELESS

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" BUSINESS RADIO "

IT is learned on enquiry from the Post Office that fifty "Business Radio Licences" have so far been issued by the P.M.G. and that about half of them are for taxi services in various parts of the country—four are in London.

As previously stated, these licences are issued in very limited numbers for such concerns as towage companies, railways, public utility vehicle services, newspapers and taxi hire services, and also to professional men, such as doctors. The initial cost is £5, plus another £5 for each transmitter-receiver.

Fifteen frequencies between 67 and 87 Mc/s have now been allocated for the use of the Press. These frequencies are for mobile equipment, which must operate within ±25 kc/s of the allotted frequency. In addition, one channel (76.9-77.0 Mc/s) has been allocated for low-power walkie-talkie type equipment.

Applications for "Press" frequencies had to be made to the Joint Telecommunications Committee of the Newspaper Society and the Newspaper Proprietors' Association by March 7th, who will advise the G.P.O. on the allocation of licences. It is understood that 22 applications from representatives of 83 newspapers and two news agencies have been received.

Applications for "Business Radio Licences" should be made to the Director, Overseas Telecommunications Department, Broadcasting Branch, G.P.O. Headquarters, London, E.C.1, who has the supervision of all radio frequency allocations.

B.B.C. REPORT

THE annual Report of the Governors of the B.B.C. for the year ended March, 1947, was recently issued as a White Paper (Cmd. 7319). It states that, in addition to the erection of the F.M. station at Wrotham and the Birmingham television station, which are in hand, the Corporation has a number of substantial development schemes, which, because of present conditions, cannot be started. "The major schemes involved are the erection of a series of television and F.M. stations, Broadcasting House extension, new regional headquarters and a new centre in London to provide for the development of television and for the grouping of other broadcasting activities at present scattered throughout London."

The story of progress in the technical field during twenty-five years of broadcasting is told briefly by H. Bishop, B.B.C. chief engineer, in the *B.B.C. Yearbook*, 1948, which has just been published.

In another chapter reviewing the year's work of the engineering division reference is made to F.M. test transmissions in the 45- and 90-Mc/s bands in various parts of the country which are continuously recorded on automatic field-strength recorders at distances up to several hundred miles. F.M. transmissions from Alexandra Palace continue on a mean carrier frequency of 90.3 Mc/s.

AMATEUR BAND PROPOSALS

A PLAN has been submitted to the International Amateur Radio Union and all I.A.R.U. societies in Europe by the R.S.G.B. outlining proposals for the sub-division between telephony and telegraphy of the five amateur bands between 3.5 and 28 Mc/s.

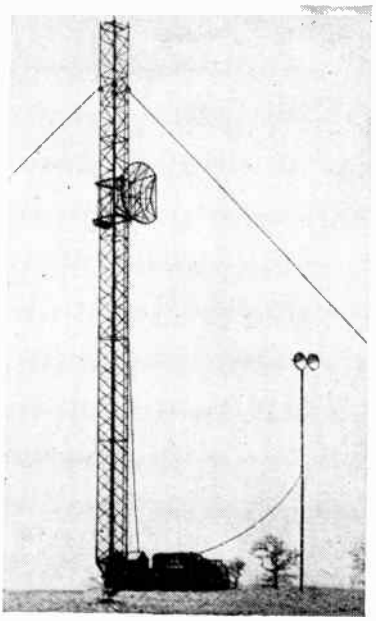
The Society states that it recognizes that any form of band planning will fail unless it is introduced into the licence and enforced by the respective licensing authorities. For this reason the European societies have been asked, when commenting on the plan, to indicate whether they consider that their licensing authority will agree to make the plan mandatory if it is finally adopted.

LONDON-BIRMINGHAM RADIO LINK

PROPAGATION tests are being conducted by the G.E.C. over the route of the London-Birmingham television radio-relay link to investigate signal strength stability and the interference level at the various sites.

Two mobile laboratories with temporary masts are being used for the tests. Each mast is fitted with a cradle to carry the 14-ft diameter paraboloid aerial system. This cradle can be raised and lowered to investigate variations in the received signal strength at various heights.

Communication is maintained between the two units on decimeter wavelengths, for which the small portable mast shown in the photograph is used.



TEMPORARY MAST with elevated paraboloid aerial used during the G.E.C. television field trials.

The results of these trials will also provide useful data for multi-channel radio-telephony systems.

½-MILE TELEVISION TOWER

ONE of the most ambitious projects yet suggested for extending the range of television has been launched in the U.S.A. It is proposed to erect a tower 2,650 feet—over half-a-mile—high in the vicinity of New York, and to install at the top a number of transmitters. William van Alen, architect, with W. Ralph Squier, civil engineer, are responsible for the design. Associated with them are: Ralph Batcher, executive editor of *Electronic Industries*, and Louis G. Pacent, radio consulting engineer.

It is planned to use the tower for other radio services, including F.M. Estimated coverage would extend over the whole of Long Island, most of New Jersey, and parts of Connecticut and Pennsylvania.

PHYSICAL SOCIETY'S SHOW

TICKETS for admission to the Physical Society's 32nd annual exhibition of scientific instruments and apparatus, which opens at the Imperial College, South Kensington, London, S.W.7, on April 6th, are available from Fellows of the Society, exhibiting firms and most of the learned societies. The tickets are valid for the sessions indicated

World Radio History

World of Wireless—

—10.0 to 1.0 or 2.0 to 8.0. On the first day the exhibition will be open from 2.0 to 9.0. The exhibition closes on the 9th.

YOUNG TECHNICIANS' PAY

AS a result of an agreement between the Association of Scientific Workers and the Engineering and Allied Employers' National Federation, young technical workers in the engineering industry now receive a minimum wage at the age of 21. The agreement provides for the following minima, plus a 29s 6d cost of living bonus: London, £3 19s 6d; the Provinces, £3 14s 6d.

The Federation is to recommend its members to make additional payments in recognition of suitable qualifications.

EXPORT TARGET HIT

FOR the first time during last year the industry's export target of "a million a month" was hit in December. The total value of all kinds of radio equipment exported during the month was £1,013,162 which brought the year's total to £10,271,716. The approximate figures for 1946 and 1938 were eight million and two million respectively.

Broadcast receivers and radiogramophones accounted for nearly half the year's exports.

The component manufacturers exceeded their monthly export target of £190,000 by some £46,000 in December making the year's total £2,095,008.

TELEPHONE RECORDING

THE final order of the U.S. Federal Communications Commission prescribing the conditions under which it is now permissible to use telephone recording devices in the U.S.A. has recently been issued.

The main features can be summarized as follows:

(1) An "approved" type of recording device must be used; i.e., it must be a device capable of warning all parties to the telephone conversation that the conversation is being recorded; adequate notice that the conversation is being recorded must be provided by an automatic tone signal, of higher frequency than the ordinary "busy" signal (1,400 c/s).

(2) Unapproved types of recorders are illegal and telephone companies may refuse to serve subscribers known to be using these.

(3) The order relates to telephone recording devices on interstate telephone communications, but it is generally accepted that it will become the basis of regulations concerning recording devices on all telephone circuits.

INSTITUTE OF RECORDED SOUND

A MEETING, arranged by the Association of Special Libraries and Information Bureaux (ASLIB), was held in London on March 3rd interested to discuss the formation of an Institute of Recorded Sound. The formation of such an institute, providing a permanent storehouse for all forms of recorded sound was agreed in principle.

Among the nine members of the committee appointed to investigate the plan in detail and make a report are: H. L. Fletcher (Association of Professional Recording Studios), Dr. L. E. C. Hughes (British Sound Recording Association), and A. C. Cameron (Educational Department, Electric and Musical Industries).

CONSOL ERROR

THE Ministry of Civil Aviation advises that observations of the transmissions from the Bushmills, N. Ireland, consol beacon taken at sea confirm that there is a possibility of large errors if a loop receiving aerial is used near the null position for direction finding. In conditions where a horizontally polarized component is present the use of a loop near the null position may lead to errors in count of twenty or more characters. Automatic gain control must be switched off when receiving Consol signals.

U.S. ELECTRONICS CAPITAL

THE vast manufacturing and research centre for General Electric of America, some six miles from Syracuse, N.Y., on which work was started two years ago, is now complete. The G.E. Electronics Park, as it is called, covers 155 acres, of which 30 acres are occupied by the main buildings.

As will be seen from the annotated photograph of a model of the centre the receiver and transmitter buildings are the largest. When in full production the peak output from the ten assembly lines in the receiver building will be 800 table models, 200 consoles or 100 television receivers a day.

Valves and heavy industrial electronic equipment continues to be manufactured in Schenectady.

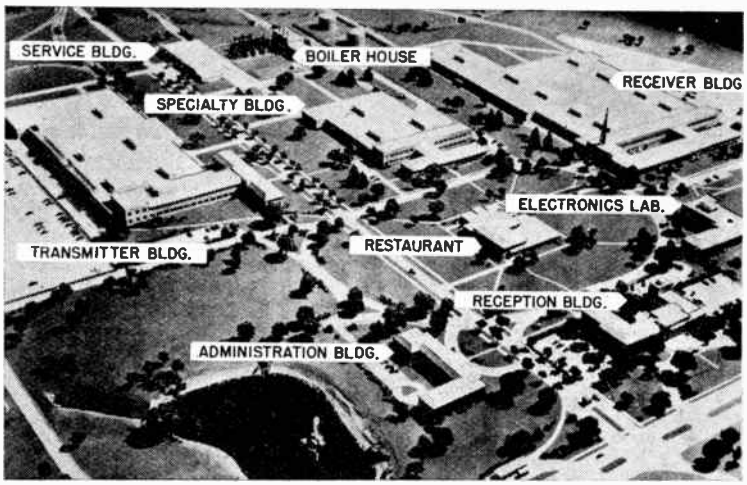
PERSONALITIES

T. A. Davies has been appointed G.P.O. inspector of wireless telegraphy in succession to Col. A. H. Read (see note below). He was deputy inspector from 1940 to 1944, when he was appointed a principal in the G.P.O. overseas telecommunications department.

A. J. A. Gracie, who as assistant secretary of the G.P.O. overseas telecommunications department was a delegate to last year's Atlantic City conferences, has been appointed as U.K. representative on the International Frequency Registration Board, and recently left for Switzerland, where the Board has its headquarters.

Walter G. Powitzer, chief studio engineer of the Palestine Broadcasting Service, Jerusalem, since its formation in 1935, has relinquished his post as assistant engineer, Posts and Telegraphs, and is returning to this country. During the war he was working for the Psychological Warfare Branch of the U.S. Army in its "Freedom" stations.

Col. A. H. Read, O.B.E., who has been G.P.O. inspector of wireless telegraphy since January, 1945, has been appointed deputy regional director of the G.P.O. London telecommunications region. He was deputy inspector



ELECTRONICS PARK, the twenty-five million dollar manufacturing and research centre of General Electric at Syracuse, N.Y.

World Radio History

for fifteen years. As recorded elsewhere in this issue, he was among the delegates to the Atlantic City conferences.

Morris Reed, Ph.D., M.Sc., M.I.E.E., has been appointed chief radio engineer at Philips' Mitcham works, where he will be in charge of all engineering activities relating to radio and television apparatus. From 1929 to 1946 Dr. Reed was with Siemens Brothers, where he held successively

DR. MORRIS REED.

the positions of head of the wireless laboratory, chief radio engineer and assistant to the chief engineer, telecommunications department. For a short time after leaving Siemens he was general manager of R.F. Equipment, Ltd.

R. Salmon, formerly managing director of R.S. Amplifiers, Ltd., is leaving for Australia on March 31st and will open offices in Sydney, New South Wales. He will be glad to assist British manufacturers wishing to increase their Australasian interests. Enquiries should be addressed c/o Phillips Advertising, Ltd., Thanet House, Craven Road, London, W.2.

Len Schultz, chief engineer of the Macquarie Broadcasting Network of Australia, which comprises some forty-five radio stations, is on a visit to this country to study F.M. and television.

W. C. Stevens has been elected general secretary of the Electrical Trades Union. He was for some years sound maintenance engineer in a film production and renting company.

Dr. M. J. Strutt, D.Techn.Sc., electronics consultant to the N. V. Philips Co., Eindhoven, has been appointed professor in the Faculty of Electricity at the Federal Swiss Institute of Technology at Zurich. Dr. Strutt has contributed many articles to our sister journal *Wireless Engineer*.

OBITUARY

It is with regret we record the death of **Cyril H. Hunt,** chairman and managing director of A. H. Hunt, Ltd., the well-known manufacturers of capacitors. He was aged 50 and the only son of the founder of the company. He died suddenly whilst travelling to his office with his wife and father.

IN BRIEF

Receiving Licences.—January's total of £2 television-and-sound receiving licences was approximately 39,000, which is an increase of 6,300 over the previous month—a record month's increase. The number of broadcast licences in force in Great Britain and Northern Ireland, including the above, was approximately 11,195,800.

Price Freezing.—Broadcast receivers, television sets, radiogramophones, components and accessories for each of these, and gramophone records are included in the list of goods in the Miscellaneous Goods (Maximum Prices) Order, 1948, which, together with thirteen other Orders, fixed the prices of the vast majority of consumer goods in this country from March 15th.

U.K.-N.Z. Facsimile.—The world's longest phototelegraph circuit, between London and Wellington, was opened by Cable and Wireless on March 1st. Pictures are automatically relayed via Colombo.

B.I.F.—A model of the radar-equipped harbour at Douglas, I.o.M., which was recently opened, will be on view in the radio section of the British Industries Fair at Olympia. The Music and Radio section will this year occupy 3,000 sq ft more than last year. The fair opens on May 3rd.

A.F.N.—The wavelengths of the Frankfurt and Bayreuth transmitters of the American Forces Network in Germany were changed at the end of February. Frankfurt is now on 499.2 metres (601 kc/s) instead of 212.6 metres, and Bayreuth on 212.6 metres (1,411 kc/s) instead of 249.2 metres.

Professional Association.—At a meeting of the Engineers' Guild on March 10th, which was attended by some 400 chartered electrical, civil and mechanical engineers, a resolution, proposed by Sir Stanley Angwin, to the effect that the Guild is capable of fulfilling all the non-technical requirements of professional engineers and should have the active support of the entire corporate membership of the three senior institutions, was agreed. It is stressed that the Guild, which was founded in 1938, is non-political and is not a trade union. The offices of the Engineers' Guild are in 28, Victoria Street, London, S.W.1.

Vacation Courses, lasting three weeks and consisting almost entirely of laboratory and workshop work, are held by E.M.I. Institutes, 44, Grove Park Road, London, W.4, during the Easter and Summer vacations. They are designed primarily as a follow-up to the postal courses in Basic Radio and Basic Television. Separate courses are held for radio and television receivers and they include work on a wide range of modern receivers of various makes. The fee for the next course, which begins on March 30th, is £6 16s 6d.

"The Trader" Jubilee.—It is with pleasure we record the silver jubilee of our associated journal *The Wireless and Electrical Trader*, which was first published monthly in March, 1923.

Mechanical Handling.—As mentioned last month, our associate journal *Mechanical Handling* is organizing the first National Mechanical Handling Exhibition, which will be held at Olympia

RE-ENTRANT HORN

TYPE 42 REH

The new 42REH has advantages of complete weather-proofness, smaller overall length, better weight distribution and consequently greater ease in handling, which make this one of the most popular of the new F.I. loudspeakers. The horn is designed for use with the standard F.I. L.S.7 Unit and allows for this unit to be driven to 12 watts input. A spun aluminium cover over the unit has room for housing a suitable matching transformer.

The construction has been designed so that the whole unit is assembled and held together with ONE LARGE NUT only. This construction enables a number of units to be packed for export in a space which is a fraction of that normally required; assembly is a matter of a few minutes unskilled labour.
This unique feature will recommend itself to all export buyers particularly.

The 42REH is not of the "loud-hailer" type of speaker, but is designed to cover a range of frequencies considerably greater than those needed for purely "announcing" purposes: i.e., it is suitable for all normal requirements of high power reproduction of music as well as speech.

Dimensions assembled	...	22in. dia. x 24in.	
Bell diameter	... ...	22in.	
Cut-off frequency	... ...	175	
Effective Air Column	... ...	42in.	
Weight Horn only	... ...	8 lbs.	
Shipping space	...	One—23in. x 23in. x 18in	
		12—33in. x 33in. x 27in.	

F.I. for P.A.

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60, PADDINGTON ST., W.1
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W.W.14

World Radio History

World of Wireless—

from July 12th to 21st. Seventeen papers covering various aspects of mechanical handling will be presented at the convention, which will be held concurrently with the exhibition.

A Weakness.—A notice to airmen from the Ministry of Civil Aviation states that whip aerials have a tendency to fracture at the point where the type number or other trade mark has been stamped or "indented" in the metal during manufacture. Whip aerials so marked are not to be fitted to British Civil Registered aircraft.

World Broadcasting.—A useful book has been produced by the Editor of our Danish contemporary, *Populaer Radio*, giving information on the organization and activities of the broadcasting systems of the world. "World Radio Handbook for Listeners," as it is called, gives, in its 96 pages, details of each country's broadcasting stations, times of transmission, address of operating concern and the difference between local time and G.M.T. A list giving the world's stations in order of frequency is also included. The book, which will be published in May and November, costs 5s.

Navigation.—The Institute of Navigation, which was formed a year ago to "promote the interest of science and practical navigation by uniting together in a scientific body those who are concerned with, or are interested in, the art of navigation," has issued a *Journal*. It will be published quarterly and contains papers read at meetings of the Institute, together with the ensuing discussions. It is obtainable from John Murray, 50, Albemarle Street, London, W.1, price 6s 3d, including postage.

Television Française.—We were misled regarding the manufacturer of the equipment used in the Eiffel Tower television station. It was manufactured and installed by Le Matériel Téléphonique. During the war this equipment was partly dismantled by the Germans, but was repaired soon after the liberation of France.

INDUSTRIAL NEWS

"Clix."—Sales of Clix radio and television components will, from April 1st, be handled by General Accessories Co., 21, Bruton Street, London, W.1. The new company is a subsidiary of British Mechanical Productions, Ltd., the manufacturers.

G.E.C. has been given a £20,000 contract to provide a F.M. mobile radiotelephone system for the Netherlands police. The equipment, which is similar to that used by our own Police Forces, will comprise ten 100-watt fixed transmitter-receivers, five 10-watt fixed stations and fifty-two mobile units. The system will operate on a frequency around 80 Mc/s.

H.M.V.—Three new receivers for the home market were exhibited on the H.M.V. stand at the *Daily Mail* Ideal Home Exhibition, Olympia. They were Models 1407, a 4-valve transportable battery superhet; 1608, a 4-valve (+rectifier) push-button auto-radiogram with twin speakers; and 1117, a table version of 1608.

Marconi Instruments.—A display of new communication test equipment will be staged by Marconi Instruments, Ltd., at their London showrooms, 109, Eaton Square, S.W.1, from April 6th to 16th. The instruments shown will be additional to those presented at the Physical Society Exhibition (April 6th-9th). It will be open on weekdays between 10 a.m. and 5 p.m. A demonstration of test equipment will also be staged at the Mechanics' Institute, Bradford, on March 31st and April 1st between 2.15 and 6.30. "Measurtest" instruments, including the new portable receiver tester, will be demonstrated.

Plessey International, Ltd., has been formed by the Plessey Co., of Ilford, with a view to establishing factories in other countries, with the exception of Eire where a new company, to be known as **Communication Components, Ltd.,** is being established in Dublin.

R.C.E.E.A.—The Council of the Radio Communication and Electronic Engineering Association, which is one of the four constitutory bodies of the Radio Industry Council, has elected L. T Hinton, B.Sc., (S.T.C.), and M. M. Macqueen (G.E.C.) chairman and vice-chairman, respectively, for the current year.

Wire Recorders.—A company has been formed to combine the activities of Boosey and Hawkes and Associated Electronic Engineers in the field of magnetic wire recording. The new company—Wirek (Electronics), Ltd., 9/10, Dalston Gardens, Stanmore, Middlesex—has in production eleven different types of recording equipment ranging from medium-fidelity speech recorders for lectures, conferences, etc., to high-fidelity machines, with overall characteristics level to ±3 db from 50 to 9,000 c/s. The company is also in a position to supply the following components for experimenters: recording heads, wire, spools, screened bias oscillator coils and input transformers. Circuit diagrams will also be available.

MEETINGS

Institution of Electrical Engineers

Radio Section. — Discussion on "Future Trends in the Design of Receiving Aerials," on April 13th, at Savoy Place, London, W.C.2, at 5.30. Opener E. M. Lee, B.Sc.

Cambridge Radio Group.—"Television Camera Tubes," by F. H. Townsend, on April 6th, at the Cambridgeshire Technical College, at 6.

North-Eastern Radio and Measurements Group.—Annual general meeting followed by discussion and demonstration on "The Influence of Frequency Response Bandwidth on the Appreciation of Electrically Reproduced Speech and Music," on April 12th, at King's College, Newcastle-on-Tyne, at 6.15. Opener, G. A. Hickling.

North - Western Radio Group.—"Pulse Communication," by D. Cooke, B.A., Z. Jelonek, A. J. Oxford, B.Sc., and E. Fitch, B.Sc., on April 7th, at the Engineers' Club, Albert Square, Manchester, at 6.30.

Scottish Centre.—"The Cavity Magnetron," by H. A. H. Boot, Ph.D., and J. T. Randall, D.Sc., F.R.S., on April 14th, at the Heriot-Watt College, Edinburgh, at 6.

South Midland Radio Group.—"Investigation and Forecasting of Ionospheric Conditions," by Sir Edward Appleton, G.B.E., K.C.B., M.A., D.Sc., F.R.S., on April 27th, at the James Watt Memorial Institute, Great Charles Street, Birmingham, at 7.

Southern Centre.—Faraday Lecture on "Electricity and Everyman," by P. Dunsheath, C.B.E., M.A., D.Sc. (Eng.), on April 8th, at the Guildhall, Southampton, at 7.30.

British Institution of Radio Engineers

London Section.—"High Fidelity Recording and Reproduction," by W. S. Barrell and G. F. Dutton, Ph.D., D.I.C., on April 8th, at the E.M.I. Studios, 3, Abbey Road, St. John's Wood, London, N.W.8, at 6.

Merseyside Section.—"The Physical Applications of Micro-Waves," by J. B. Birks, B.A., on March 31st, at 6.45.

"Some Aspects of Moderate Precision Temperature Control in Communication Engineering," by M. P. Johnson, B.A.Sc., E.E., on April 14th, at 6.45.

Both these meetings will be held in the Lecture Room, Liverpool Engineering Society, 9, The Temple, 24, Dale Street, Liverpool, 2.

North - Western Section.—"Link-Coupled I.F. Circuits Applied to Car Radio Receivers," by R. D. Trigg, on April 8th, at the College of Technology (Reynolds Hall), Sackville Street, Manchester, at 6.45.

Scottish Section. — "The Physical Applications of Micro-Waves," by J. B. Birks, B.A., on April 21st, at the Institution of Engineers and Shipbuilders in Scotland, Elmbank Crescent, Glasgow, C.2, at 6.45.

North-Eastern Section.—"The Pulse Signal," by Professor M. G. Say, Ph.D., M.Sc., on April 14th, at Neville Hall, Westgate Road, Newcastle-on-Tyne, at 6.

British Sound Recording Association

London Meetings.—The meeting on March 25th, at which W. S. Barrell, B.Sc., will read a paper on "High Quality Disc Recording," will be held at E.M.I. Studios, 3, Abbey Road, St. John's Wood, London, N.W.8, at 7.15, and not at the Royal Society of Arts as stated last month.

"Quality Factors in Film Recording," by B. C. Sewell, on April 23rd, at the Royal Society of Arts, John Adam Street, Adelphi, Strand, London, W.C.2, at 7.

Electrical Trades Union

London Meeting.—Open discussion on "Tone Control Circuits," on April 22nd, in the Oak Room, Kingsway Hall, Kingsway, London, W.C.1, at 7.

Junior Institution of Engineers

"The Manufacture of Gramophone Records," by H. W. Bowen, O.B.E., on April 16th at the Institution, 39, Victoria Street, London, S.W.1, at 6.30.

Radio Society of Great Britain

"Radio Signals from the Sun," by M. A. Ryle, M.A., on April 9th at the I.E.E., Savoy Place, London, W.C.2, at 6.30.

Society of Relay Engineers

"Negative Feedback and Direct Coupling as applied to A.B.2 Amplifiers," by L. F. Odell, on April 27th, at the Royal Society of Arts, John Adam Street, Adelphi, Strand, London, W.C.2, at 2.15.

World Radio History

Unbiased

By FREE GRID

Retrogress in Receiver Design

THE Moguls of the wireless industry who are responsible for the receivers offered to us members of the listening public—who indirectly pay the rent of the marble halls in which they dwell—seem, in certain respects, to be altogether out of touch with the common man and his radio needs. They seem to imagine that we all dwell in baronial halls, like themselves, each member of the family occupying a separate wing to which he can retire and listen to the programme of his choice without interfering with that of the others. It never seems to occur to them that—perish the thought—some of us on occasion have such perverted tastes as to like certain items in the third programme and are debarred this enjoyment because we cannot very well start up a set in opposition to the one churning out the melancholy cadences of some cacophonous crooner in the light programme. The resulting noise would be more horrible than that of the crooner.

The only solution is for third-programme addicts to listen with high-quality headphones, but how many receivers are there with provision for connecting headphones? None so far as I am aware and this, in spite of all the talk about the necessity of a second receiver in the home. The reason, as I have already mentioned, is the baronial hall complex of the set manufacturers who imagine that we can

Leg-entangling paraphernalia.

retire with our second set and listen to the third programme in the chilly and ghost-ridden East Wing of the castle.

Reluctant as I am to praise manufacturers, I must do so in the case of those turning out radio-gramophones with a flush top panel and a deeply recessed lid. This enables us to sweep all the dust on to the floor and is a great improvement on the old dust-trap type. It was impossible to clean the latter except by fitting together the hose and other leg-entangling paraphernalia of a vacuum cleaner. But why not go a step further and make the lid domed so that a woman cannot stand an aspidistra on the top of it, which has to be hurled to the ground every time you want to play a record. Radio manufacturers ought to realize that the broad lid of the conventionally designed radio-gramophone is an open invitation to women to stick things on it; probably, however, most of them keep their wives in a separate wing of the baronial hall and so cannot be expected to be acquainted with the conditions of family life which have to be endured by the common man.

"I Done It"

IT is never wise to meddle in matters which you don't properly understand, as an old countryman once told me when I poked my umbrella, with disastrous results, into a wasps' nest which he was pointing out to me. By my blundering reference in the February issue to an American claim to locate paranormal entities (ghosts to you) by means of radar I certainly got more than I bargained for in the way of helpers willing and anxious to accompany me to the site of Borley Rectory. So overwhelming has been the response that I have had to call the whole thing off, as no self-respecting ghost would do other than imitate Achilles and sulk in his tent, before such a multitude. I must, however, take this opportunity of thanking my correspondents, for it would be quite impossible to reply individually to them, as Mr. Isaacs refuses to direct the necessary number of stenographers to help me.

Fortunately, however, my would-be helpers needn't be disappointed as one correspondent has very kindly sent me a cutting from the *Suffolk and Essex Free Press* of February 5th from which it would appear that the Borley manifestations have moved themselves three miles to "The Bull" at Long Melford. This is certainly a very sensible thing to do, as one could hardly think of a more comfortable place in which to investigate such matters.

I certainly intend to go to "The Bull," but on my own for reasons already explained. I do hope, however, that some of you will find your way there. Should you see anything which causes you to feel that spirits of a more tangible kind would revive drooping morale, you can charge it up to the Editor's account, that is if the manager is naïve enough to think he can get the money out of him.

Disastrous results

Among my correspondents I want particularly to mention an earnest Scotsman who casts some doubt on the truth of some of Queen Elizabeth's nocturnal activities to which I referred in May, 1946. I can only conclude that bitter memories of the disgraceful way in which Elizabeth treated Scotland's Queen at Fotheringay Castle must have so roused his national feelings as to cloud his better judgment. Another correspondent tells me that Mr. Harry Price, the psychic investigator, has stated that my remarks about nobody having had the gumption to adopt modern scientific methods is without foundation, and for this statement I sincerely apologize.

I am rather afraid that I annoyed the poltergeists, as they somehow or other made me appear to write psycheurlator (presumably a ghost worshipper) when I thought I wrote psycheuretor (a ghost hunter); as if the verb ἑυρισκω weren't irregular enough already. In any case, as one very learned psychist tells me, it actually isn't the "Psyche" at all but the "Phantasma" which is responsible for all this sort of thing; that being so, I can't think why he continues to call himself a psychist instead of a phantasmist.

World Radio History

Atlantic City

Summary of the Findings of the International Telecommunication Conferences

WE have now had an opportunity of studying the "Final Acts" of last year's Atlantic City International Telecommunication and Radio Conferences, to which a brief reference was made in last month's Editorial. It is proposed to outline in this article some of the major changes introduced in the regulations and findings in so far as they differ from those of the last conference (Cairo, 1938).

Before dealing with these, however, it is worth looking into the constitution of the conferences and the objects of each of the four which, together, lasted twenty weeks. As mentioned last month, the volume embodying the "Final Acts" is divided into three sections: International Telecommunication Convention; Radio Regulations; and Recommendations adopted by the Radio Conference. The plenipotentiaries of the seventy-eight participating countries signed the Convention on October 2nd. It is effective from January 1st, 1949. Its forty-nine articles cover the composition, functions and structure of the International Telecommunications Union, including the establishment of the International Frequency Registration Board, and general and specific provisions relating to telecommunications and radio.

Conference Objectives

The four conferences, the first of which opened in Atlantic City on May 15th last year, were: the *Radio Conference*, to revise the radio-communication regulations and replan the frequency allocation; the *Plenipotentiary Conference*, to revise the international telecommunication convention; the *High-Frequency Broadcasting Conference*, originally planned to re-allocate frequencies for long-distance broadcasting stations, but actually restricted to preparatory work for conferences to be held in Mexico City from October 22nd this year; and a preliminary *European Broadcasting Conference*, which, although not originally scheduled, was decided upon in view of the number of European delegates present.

The British delegation totalled nearly 30, and included representatives of the G.P.O., the three Fighting Services, B.B.C., British Joint Communications Board responsible for Services communications, the Foreign Office and scientific advisers from the Ministries. The G.P.O. representatives included A. J. A. Gracie, assistant secretary, Overseas Telecommunications Dept.; S Horrox, principal, Telecommunications Dept.; Col. A. H. Read, inspector of wireless telegraphy; and A. H. Mumford, staff engineer, Radio Development Branch. The B.B.C. was represented by Sir Noel Ashbridge, director of technical services, and L. W. Hayes, head of overseas engineering and information department. The leader of the delegation was Sir Stanley Angwin.

To turn now to the actual findings of the conferences.

Comparing the Atlantic City and Cairo Regulations, from the point of view of frequency allocation, a writer in the January issue of *The Post Office Electrical Engineers' Journal*, states: "the changes that have been introduced fall broadly into three categories, namely:—

"(a) The formulation of service definitions to cover new types of service;

"(b) the introduction of new regional boundaries for allocation purposes;

"(c) changes in the frequency allocation table itself."

Summarizing the first of these, the writer states that: "in addition to the services to which bands were allocated under the Cairo Regulations, specific provision is now made for radio navigation systems, for radio aids to meteorology, and for the transmission of standard frequencies of high accuracy. In addition, certain limited bands have been designated for industrial, scientific and medical equipment. . . ." In the summary of allocations published in November (p. 439) one frequency assigned to I.S. and M. was omitted; the complete list is 13.56, 27.12, 40.68, 2450 and 5850 Mc/s.

New Regions

In the Cairo Regulations the world was divided into the "European Region" and "Other Regions," but is now split into three for the purpose of frequency allocations; the boundaries of the regions are defined as:—

Region 1 is limited on the West by line B (see accompanying map) and on the East by line A, except that it includes that part of Turkey and the U.S.S.R. outside this limit, the territory of the Mongolian Republic and the area to the North of the U.S.S.R. between lines A and C. It does not, however, include any part of Iran.

Region 2 includes the area between line B in the East and C in the West.

Region 3 is limited on the East by C and the West by A but excludes Turkey, the U.S.S.R. and Mongolia, which are incorporated in Region 1. Iran is included in this region.

In our earlier reference to frequencies allocated at Atlantic City we erroneously implied that Region 1 was the "European Region." This is not so. Within Region 1 is the "European Area," the boundaries of which are: West, line B, East, the meridian 40° E, and South, the parallel 30° N. The parts of Arabia and Saudi-Arabia coming within these boundaries are excluded from the "Area."

Under the Cairo Regulations the "European Region" was, as stated above, one of the fundamental geographical areas for allocating frequencies to all services throughout the spectrum 10 kc/s to 200 Mc/s, whereas the

World Radio History

European Area is now included only for the purpose of controlling the frequencies of long- and medium-wave broadcasting stations in that area.

Tropical Broadcasting

It has also been found necessary to re-define and extend the Tropical Zone for the allocation of frequencies for tropical broadcasting —defined as "broadcasting for international use"—in countries within this zone which now girdles the earth. As will be seen from the map, it lies between the tropics of Cancer and Capricorn with extensions in certain areas.

The bands allocated for broadcasting in the Tropical Zone are: —

2.3—2.498 Mc/s
3.2—3.4
4.75—4.995
5.005—5.06

The upper limits of the 2-Mc/s band are reduced to 2.495 in Regions 2 and 3. The band 3.95 4.0 Mc/s included in our previous list as allocated for tropical broadcasting is for use by broadcasting stations generally.

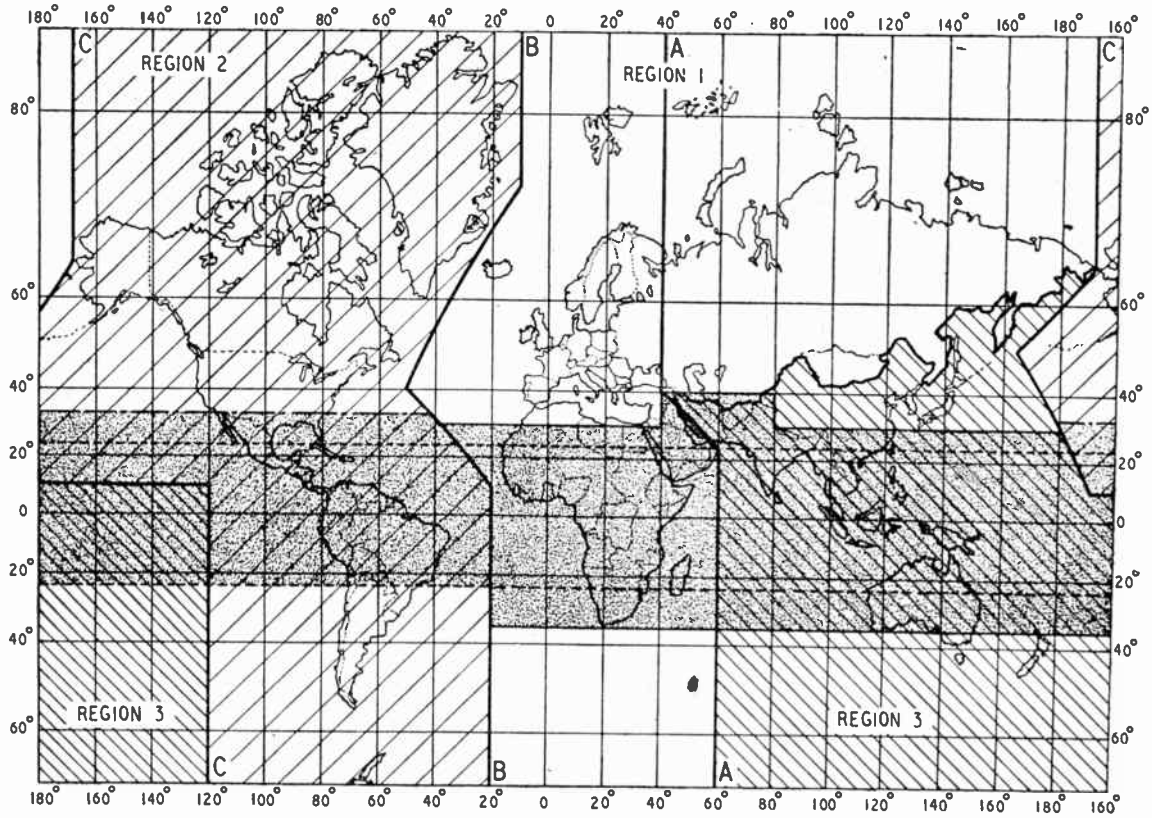
The writer in the *P.O.E.E.J.* points out that the principal changes in frequency allocation involve increases for aeronautical and broadcasting services and amateurs with a reduction of some 10 per cent in the allocations for maritime and fixed services; the reduction—almost to elimination —of shared bands; and the use of harmonic relationship for the ship-to-shore sections of the maritime mobile bands.

The table of frequency allocations, which now extends from 10 kc/s to 10,500 Mc/s, has been accepted without reservation by all the countries represented. This covers block allocations to the various services, and it now remains for agreement to be reached regarding allocations for individual countries in the broadcasting bands. So far as Europe is concerned, a preliminary plan for the long- and medium-wave broadcasting bands is being prepared by a committee consisting of representatives of Belgium, France, Great Britain, Holland, Sweden, Switzerland, the U.S.S.R. and Yugoslavia. This plan is being prepared in readiness for the European Broadcasting Conference to be held in Copenhagen in July.

Frequency Registration

It has already been stressed in *Wireless World* that one of the most important outcomes of the Atlantic City conferences is the decision to set up an International Frequency Registration Board whose task it will be to examine all notifications of the proposed use of frequencies, and if approved, they will be included in the Master International Frequency Register. A list of registered frequencies will be published from time to time by the Bureau of the International Telecommunication Union.

The I.F.R.B. is composed for the first five years of representa-



The three Regions into which the world is divided for the purpose of frequency allocation are shown on this map. The Tropical Zone which now girdles the earth, is shaded.

World Radio History

Atlantic City—
tives of each of the following countries, who were elected by secret ballot: Argentina, Australia, China, Cuba, Czechoslovakia, France, Great Britain, India, South Africa, U.S.A. and U.S.S.R. By a division of the world's surface into four, the conference ensured an even distribution of membership. The same procedure was adopted for the election of members to the Board of the I.T.U. The U.K. representative on the I.F.R.B. is A. J. A. Gracie (see this month's "World of Wireless").

The preparatory draft of an International Frequency List covering the assignments to fixed service stations, tropical broadcasting transmitters and mobile land stations, within the band 10 kc/s to 30 Mc/s, is being undertaken by the Provisional Frequency Board. This consists of members of the I.F.R.B. and representatives of countries desirous of participating in this work. The P.F.B. aims at completing the draft by November 15th. It will be studied at a special conference to be called in March next year.

It is recommended that the provisions of the International Frequency List become effective by September 1st, 1949.

New Definitions

Among the definitions laid down in the first chapter of the Radio Regulations are some which were unheard of when the Cairo regulations were drawn up. They include "facsimile"; defined as a system of telecommunication for the transmission of fixed images with a view to their reception in permanent form. The exclusion of "phototelegraphy" points to the general use of "facsimile" for all systems for the transmission of "fixed" images as opposed to "transient" images of fixed or moving objects which is, of course, defined as television. Radiolocation is included, and is defined as "determination of a position or of a direction by means of the constant velocity or rectilinear propagation properties of Hertzian waves." The employment of radiolocation solely for the purpose of "the determination of position or direction or for obstruction warning in navigation" is termed "radionavigation."

Radar is defined as a "radiolocation system where transmission and reception are carried out at the same location, and which utilizes the reflecting [primary radar] or retransmitting [secondary radar] properties of objects in order to determine their position."

Transmissions Classified

The revised classification of the various types of transmission includes the three types of modulation; amplitude, frequency (or phase) and pulse, the symbols for which are A, F and P, respectively.

The digits used to define the type of transmission have been increased. They are now: 0, unmodulated; 1, keyed C.W.; 2, keyed audio-frequency modulated waves (M.C.W., I.C.W.); 3, telephony; 4, facsimile; 5, television; and 9, composite transmissions.

The classification of transmissions includes, in addition to the types of modulation and transmission, a third symbol denoting supplementary characteristics. They are:—

a, single side-band, reduced carrier (double side-band, full carrier, no symbol).
b, two independent side-bands, reduced carrier.
c, other emissions, reduced carrier.
d, pulse, amplitude modulated.
e, pulse, width modulated.
f, pulse, phase (or position) modulated.
B, damped waves.

The bandwidth occupied by the transmission is indicated, where necessary, by a prefixed number giving the width in kc/s.

As an example of this classification, A.M. telephony (3,000 c/s max. modulation) on single side-band with reduced carrier is designated 3 A3*a*.

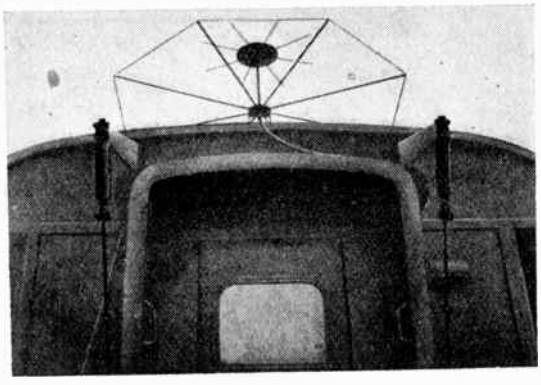
It is regrettable that whilst classifying frequency bands a break-away was not made from the use of the superlatives "very," "ultra," "super," etc. The new classification which, so far as wavelength is concerned, follows the metric system employed in the British Standards Glossary (B.S.204) except that the range is extended down to 0.001 metres which are classified as millimetric waves. In the frequency classification this band is designated "extremely high," so that we now have V.L.F., L.F., M.F., V.H.F., U.H.F., S.H.F., and E.H.F.

International Call-signs

Considerable changes have been made in the international list of call signs consequent upon the geographical changes as a result of the war. Germany's "D" allocation is to be divided between Germany, Belgian Congo, Bielorussia and the Philippines. Japan's "E" will in future be used by the U.S.S.R. and its "J" is to be shared with Mongolia and Norway. The previous list of calls began at CAA and ended at ZZZ. The new list includes "A" and "B" allocations and terminates with a series using a numeral and two letters. The first of these is 2AA-2ZZ and the series continues to 4WZ.

The "Q" code has been amended and now includes a number of new abbreviations, most of which relate to movements of ships and aircraft, search and distress, meteorology and D.F.

It has not been possible within the limitations of this article to deal with the "Final Acts" *in extenso*, and it is therefore hoped to give further details of specific items in future issues.



RAILWAY RADIO. Successful radio-telephone transmissions between a train on the Rome-Tivoli line and the chief railway office in Rome were conducted towards the end of last year. F.M. on 2-3 metres was employed. The aerial mounted on the roof of one of the coaches is shown here.

World Radio History

New Books

Electronic Circuits and Tubes. By the War Training Staff of the Cruft Laboratory, Harvard University. Pp. 948 + xxiv, with 759 illustrations. McGraw Hill Publishing Co., Ltd., Aldwych House, London, W.C.2. Price 45s.

IT is stated in the foreword that that "This book has developed from the lecture notes of a special wartime training course given in the Graduate School of Engineering, Harvard University," that "the material of the course was fundamental in nature and not exclusively applicable to wartime training," and that "it is hoped that the text will be as valuable for peacetime courses as it was successful in its intended purpose." "A knowledge of mathematics through calculus, and of electricity and magnetism is assumed."

Starting with Alternating Current Theory, the book covers Circuit Response, Circuit Elements (and their measurement), Networks and Impedance Matching, Transients, Coupled Circuits, Filters, Fourier Analysis, Electron Emission and the Diode, Multi - element Tubes, Cathode Ray Tubes, Amplifiers, Class A and Class B, Power Tubes, Oscillators, Gas-Filled Tubes, Rectifiers and Power Supplies, Signal Analysis, Principles and Methods of Modulation, Detection, Test Instruments, Radio Receivers and Tuning Circuits.

A number of different authors are responsible for different chapters and doubtless it is because of this that there is some patchiness in treatment. Some chapters are extremely detailed and very thorough, others are much more elementary and of a rather superficial character. The chapter on coupled circuits, for instance, is extremely good and in addition to the usual resonance curves there are photographs of space models showing the response three-dimensionally. Detection is also well done and the importance of keeping a high ratio of A.C./D.C. loads is well brought out by oscillograms of the output waveform.

The treatment of power amplifiers is good, including the class C types so widely used in transmitters. The section on frequency multipliers, however, is very disappointing; it comprises only 1½ pages. In view of their widespread use it is to be regretted that the authors did not see fit to treat them adequately.

Another important subject which is dealt with in only a superficial fashion is the superheterodyne receiver. Frequency-changers occupy some nine pages of largely descriptive material. There is no mention of oscillator tracking methods nor of the mechanism of production of spurious responses, apart from the image response, which is only one among many. Later in this same chapter under the heading "Interference" (two pages) there are brief references to more of them, but there is little indication of their magnitude or practical importance, and little is said about methods of avoiding or reducing them.

The chapters on measurements and test instruments are very elementary and well below the general standard of the book. Common methods are briefly described, but little or nothing is said about their accuracy.

Rectifiers and power supplies are unusually fully treated and the emphasis is on apparatus of fairly high power. This high-power stress applies also in large measure to the treatment of oscillators and amplifiers. It is noticeable throughout the book that the high-power aspects are given more attention than the low-power, and this does make the book of greater value to those interested in transmission than to those primarily concerned with reception.

On this latter side, another omission is any adequate treatment of receiver noise. Even more surprising is the fact that wideband amplifiers, in the usual sense of the term, are not mentioned at all. A wideband amplifier is defined as an amplifier in which the bandwidth is large compared with the mean frequency and is applied to A.F. and V.F. amplifiers. No reference is made to wideband R.F. amplifiers, such as those in television and radar, where the bandwidth is an appreciable fraction of, but is not large compared with, the mean frequency. The problems involved in these are in some ways more difficult of solution than those in V.F. amplifiers and demand special methods, such as stagger tuning, which are not treated.

A.F. transformers are dealt with very inadequately, and so are valves with more than three electrodes. Diodes and triodes are very well treated, but valves with more electrodes are dismissed in some seven pages.

Chapters are divided into numbered sections and the figure numbering starts afresh in each section and is prefixed by the section number but not the chapter number, so that there are many illustrations with the same number. This incon-

The following figures are the pass figures on final test for Model QA12/P AMPLIFIER

FREQUENCY RANGE
± 0.3 db 20 — 20,000 c.p..
SENSITIVITY
1.5 millivolts for full output
(without boosts)
15 millivolts for full output
(with boost:)
BASS CONTROL RANGE
— 12 db to + 16 db at 30 c.p..
relative to 600 c.p...
TREBLE CONTROL RANGE
— 30 db to + 18 db at 15,000
c.p.. relative to 600 c.p.s.
DISTORTION CONTENT
(up to 12 watts output)
2nd Harmonic <0.2%
3rd Harmonic <0.3%
Higher orde. <0.03%
Total <0.4%
BACKGROUND NOISE
better than — 66 db at full gain
DAMPING FACTOR 12
INPUT IMPEDANCE
1.5 megohms
SOURCE IMPEDANCE
Up to 50,000 ohms
OUTPUT IMPEDANCE
7 and 15 ohms.

226-

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World Radio History

New Books—

venient system has led to the omission of the proper Fig. 4.1 from Chapter II (p. 27) and to the repetition, in its place, of Fig. 4.1 of Chapter I (p. 7). It is surprising that this has not occurred more often! In Fig. 7.1, p. 14, a blocking capacitor has been omitted and the diagram shows a short-circuit on the H.T. supply. In Fig. 13.7, p. 518, of a transitron oscillator, the grid leak to G_3 has been omitted; as shown, the circuit cannot work. The use of a comma, instead of a product sign, in the last equation on p. 95 makes it meaningless.

These are minor points in a book of which some two-thirds is excellent and deserves the highest praise. One-third of it is disappointing, not because of errors, but because of a superficiality of treatment.

W. T. C.

Theory and Application of Microwaves. By A. B. Bronwell and R. E. Beam. Pp. 470+vii with numerous illustrations. McGraw-Hill Publishing Company, Aldwych House, London, W.C.2. Price 36s in U.K.

THIS book is not an elementary text and is presumably intended for the reader who has already had considerable acquaintance with electromagnetic theory. In the reviewer's opinion there is a tendency, which is to be deplored, for writers of books on new fields of application of electromagnetic theory to devote far too much space to needless recapitulation of standard and basic work, already dealt with admirably. Whilst there is not a great deal to quarrel with in the actual treatment of the matters included in this book, in view of the title it may be said that it contains much that is superfluous, and also unfortunately, insufficient information relating to microwave technique. The authors excuse the omission of a discussion of some aspects of radio circuit theory on the grounds that "there are a number of excellent textbooks dealing with such matters." One is inclined to ask, therefore, why they have not shown the same sense of discrimination with respect to the rest of the material.

The general process of development is as follows. After several introductory sections on the behaviour of charges in electric fields; current, power and energy relationships, and the physical basis of equivalent circuits, we come to three chapters devoted to a discussion of oscillators. These include a treatment of transit-time oscillators in general with particular reference to the klystron and the magnetron. We then have three further chapters on various aspects of transmission lines, both from the theoretical and experimental point of view. Transmitting and receiving systems are considered in Chapter 11, and pulsed systems, particularly radar systems, briefly in Chapter 12.

The chapters on Maxwell's equations and the solution of electromagnetic-field problems might well have been condensed into a mere introduction to the subject of waveguides as considered in Chapter 16. This chapter contains a satisfactory and quite concise treatment of the phenomena associated with propagation in waveguides. The last five chapters are concerned with the applications of waveguides and resonators, linear antennæ and arrays, the impedance of antennæ, and finally other radiating systems such as the biconical antenna and horn radiators.

There are one or two errors which must be pointed out. One page 427 the figure which is supposed to indicate the nature of the current distribution in a centre-fed aerial relates in fact to an end-fed antenna.

Then, on page 216, the equivalent absorption area of an ideal short doublet receiver is actually attributed to a half-wavelength dipole.

There is a quite inadequate section on propagation characteristics. This fundamental matter is here dismissed in two or three short paragraphs. In Chapter 10 there are some references to impedance and power measurement at microwave frequencies, though not in any detail, and this is a further example of a matter on which the authors could profitably have expanded the treatment.

The book is well produced, and liberally illustrated. The authors have justified their claim that: "throughout the engineering point of view has been stressed, and that, wherever possible, the analytical results have been expressed in a form convenient for engineering use." A good feature is the number of illustrative examples included in the text; there is also a wide selection of problems suitable for students.

J. A. S.

Radio Engineering (Volume 1). By E. K. Sandeman, Ph.D., M.I.E.E. Pp. 775+xxiv. Chapman and Hall, Ltd., 37, Essex Street, London, W.C.2. Price 45s.

THIS work claims to be "a textbook for beginners" and "a reference book for experienced engineers." According to its author, it "assumes complete ignorance on the part of the reader and develops the required terminology as it goes along." And "The reader should have a working knowledge of elementary algebra, and should preferably understand logarithms. The necessary elements of trigonometry are stated, while complex algebra is developed from first principles. With these qualifications, it is true to say that in the main body of the book information is imparted in a logical sequence so that a novice who conscientiously reads the book from the beginning always finds the subject matter within his grasp."

It is doubtful whether anybody, working on this basis, could successfully write for novices and experienced engineers at the same time. Certainly the author has not succeeded. What he has done is to produce a notable and important work on broadcast transmitters, with particular reference to B.B.C. practice. This volume has 775 pages, and there is another volume to come. The fact that subject matter which is irrelevant to broadcast transmitters is almost entirely left out means that there is room for a quite exceptionally thorough treatment of everything that does concern broadcast transmitters. This treatment is based on the unsurpassed experience of the B.B.C. in that field; and, as the author acknowledges in detail, his work has had the full co-operation and authority of the B.B.C. technical staff. It provides a vast amount of data on the practical design, operation and maintenance of fixed transmitters for broadcasting sound on carrier frequencies between 200 and 20,000 kc/s. The basic principles, especially impedance, are treated very thoroughly, and can be applied more generally. Diagrams and charts are consistently clear, and the text is well printed and comparatively free from errors.

As a textbook for beginners, it cannot be so highly recommended. The author does not seem to have been able to look at his writing through the eyes and mind of someone reading it for the first time. He persistently uses technical terms, and—worse still—ordinary words used in a technical sense, long before he defines or explains them. Many important terms and concepts are explained casually somewhere in a sub-section devoted mainly to something else. The explanations, when they do come, are often expressed in the language of one who knows it already. A beginner, stumbling over the first ocurrence of a mysterious word, is unlikely to find what he wants in the Index, or may be referred by it to the unpublished Vol. 2. In the absence of any guidance as to what is for him and what is for the experienced engineer, he repeatedly finds himself

World Radio History

up against illustrations drawn from techiques which he, if he really started in complete ignorance, must find completely beyond him. From the very start he is faced with such terms as "normal" (meaning perpendicular), "sense" (meaning polarity or sign), "bridge" (the network), "shunt" (parallel), "programme" (meaning alternating currents corresponding to sounds in a broadcasting studio), "bandwidth," "C.C.I.," "C.C.I.R.," "quarter-wave choke," "class C.," "Miller capacity," "balanced" (to earth). If at the start he knows nothing of the nature of electromagnetic waves, so much the worse for him; he will not be enlightened, unless he persists as far as p. 669, where a few casual lines about polarization (under "Short-Wave Transmitting Aerials"!) might give him a clue.

It is difficult to see a "logical sequence" in the order of Chaps. III, IV and V, devoted respectively to the sine wave and vectors, D.C., and A.C. Difficult sections of text are often placed with no clue to their significance or why one ought to make a special effort to learn them.

Although the author admits that to him there is no point in reading mathematical descriptions (whether one understands them or not) he imposes many such descriptions on his readers. And he does not always keep faith with them by explaining any mathematics beyond elementary algebra, but slips in a bit of calculus here and there without warning. At other times he stands by strict rule of thumb and refuses to say *why* Litz must not be used above 2 Mc/s or sharp points are more likely to provoke discharge than rounded surfaces. But generally a proper use of mathematics for practical engineering is well maintained.

If a restrictive sub-title is added, and the invitations to the ignorant are expunged, most of the foregoing criticisms lose most of their force. With these mental adjustments this book can the more readily be welcomed as a valuable contribution to the literature. M. G. S.

LETTERS TO THE EDITOR

V.H.F. for Quality ✦ Locating Clandestine Stations ✦ Magnetophon Tape

Frequency Modulation

THE almost constant appearance, in advertisements, of the words "high fidelity," lead me to surmise that there must be, even now, a considerable demand for such reproduction. This demand cannot be met, in spite of Mr. Cazaly's assertion in your March issue, while the medium waveband is used for propagation. Technicians appear to be unanimous in their opinion that a move to higher frequencies is necessary and inevitable. Although such change will obviously be delayed by present economic circumstances, the necessary experimental and pioneering work should be carried out as rapidly as possible.

S. G. BARRELL.

Ashtead, Surrey.

Symbol of Inconstancy?

I ACCEPT D. K. McCleery's challenge (your March issue).

He has failed to distinguish between the symbol for *variability* (a "filled-in" arrowhead with curved outlines) and that for *direction* an open arrowhead with straight sides. The symbol should be like this in a normal year:

and this in a leap year:

L. BAINBRIDGE-BELL.

Haslemere.

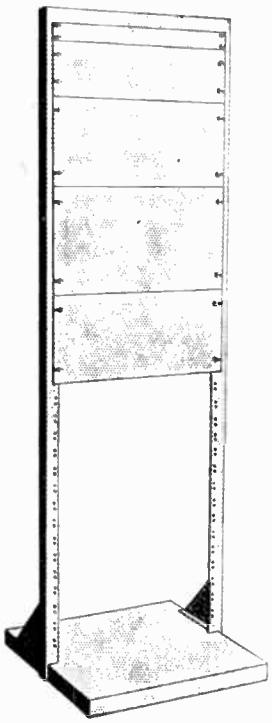
"Micro-waves and Waveguides"

IN your March issue there is a review of my recent book which I feel cannot be allowed to pass without comment. The general opinion expressed by the reviewer differs so markedly from the assessment of the many engineers who have read the book and subsequently sent me appreciative remarks that it is clear his verdict cannot be regarded as a representative one.

The development of the characteristics of waveguide modes on

2506

And now the STANDARD RACK



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,,	19" x 5¼"	...	...	5s. 7d. ,,
,,	19" x 1¾"	...	...	3s. 2d. ,,

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Letters to the Editor—

the basis of what the reviewer calls a thin analogy with propagation along parallel wire transmission lines is now recognized as a most valuable means of approach to this subject, and in fact has presented to the engineer for the first time that physical picture of the mechanism involved for which he has been searching so long. Obviously such an approach has limitations, but provided that these are kept in mind they do not detract from the value of the device.

In restricting the mathematical analysis to wave modes of particular engineering significance the treatment becomes more objective and attention is focused on specific problems of importance. In this way much more is gained than lost since a wider discussion would not really help most engineers, and would be more difficult to follow.

An examination of the problem of attenuation in general is beyond the scope of this book, but a typical case was deliberately chosen for simplification in such a way as to enable the change to be followed from normal wave propagation to evanescent conditions.

The reviewer does not appear to have any real conception of what this book sets out to achieve, nor the least understanding of the essential ideas behind the chosen form of presentation.

H. M. BARLOW.

London, W.C.1.

Clandestine Radio Transmissions

THE article published in your January issue about clandestine radio reception in Holland was of especial interest to me. During my work in an Intelligence Section in that country I had some opporunity of learning how such listening was often carried on.

It was, indeed, a source of much annoyance to the Germans; but nothing like the clandestine radio transmissions, which were carried on by the Resistance movements through all the occupation years. There were a number of these small (and usually highly mobile) stations throughout Holland, Belgium, and France, and they by no means all came to an untimely end. It is *not* easy to locate an A.M. station with pin-point accuracy by purely D.F. means, even when these transmissions always take place on the same frequency—and often at pre-advertised times. In at least one case two and a half years were insufficient for German investigators to track down a transmitter operating more or less daily for long periods within a small area of Central Holland.

C. D. SIMMONDS.

Maryport, Cumberland.

Magnetic Recording

MR. L. G. WOOLLETT seems to suggest in your March issue that alternative widths of magnetic tape were standardized in Germany for use with the Magnetophon system, one of 0.254 inch, and the other of 1 cm. So far as we are aware, the only standard width was 6.5 mm. (= 0.256 in). We do not know what manufacturing tolerances were permitted.

The width adopted by British manufacturers at the meeting convened by the B.B.C. in May, 1947, was 0.245 in, with a tolerance of ±0.005 in, the intention being to standardize on a round figure in British units (¼ in) for the maximum tape width. The width of the tape guides was not specified at the meeting, but it is the intention to make these wide enough to accept tape made to the German standards, the whole background to the discussion being a desire on the part of the B.B.C. to ensure that equipment manufactured in Britain should be capable of playing recordings made with tape or machines using the German standards.

It may be appropriate here to say that attempts are about to be made to obtain agreement in a wider field on the standardization of those parameters of the system which governs the interchangeability of tape recordings.

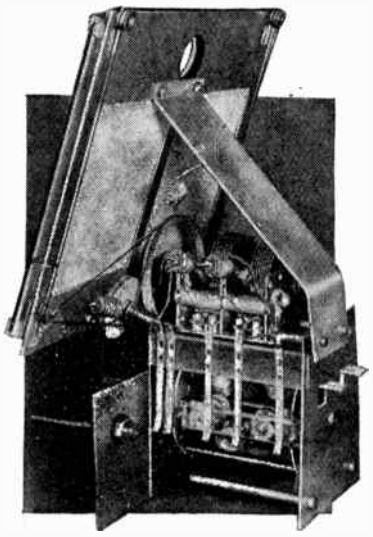
H. BISHOP,

Chief Engineer, B.B.C.

Manufacturers' Products

Five-band Coil Turret

THE Denco coil turret Type CT6 is designed for use in a broadcast superhet receiver having a triode-hexode frequency changer as the first valve. It includes coils for five wavebands giving a continuous coverage of from 30 Mc/s to 530 kc/s, and a long-wave range of 400 to 150 kc/s. The oscillator padders are for an I.F. of 465 kc/s.



Denco five-range coil turret assembly for a superhet receiver. The large tuning scale is calibrated in frequency and with the names of the principal broadcasting stations.

In the form shown, the turret includes a two-gang condenser and a large rectangular black-glass dial with five clear vertical scales calibrated in frequency and with the names of prominent medium- and long-wave stations; the principal short-wave broadcast and amateur bands are indicated.

The turret is constructed from sheet aluminium with brass bushes for all bearing surfaces. Polystyrene is used for supporting the switching contacts, and also for the coil formers; these have adjustable dust-iron cores.

Rotation of the coil turret is checked positively at each position by a ball-ended plunger locking into a circular indentation in the back plate. Provision is also made for short-circuiting the oscillator coil for the frequency band below the one in use, to prevent any harmful effects of resonance in the coil.

Accompanying each coil turret is a circuit diagram for a superhet receiver and instructions for assembling and lining up the circuits.

The price of the Type CT6 turret,

World Radio History

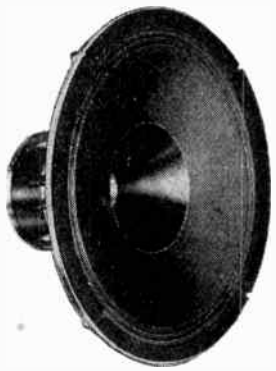
as illustrated, is £4 10s and the makers are Denco, Ltd., 355-359, Old Road, Clacton-on-Sea, Essex.

Improved Twin Diaphragm Loudspeaker

BEFORE the war Goodmans "Auditorium" twin-diaphragm loudspeakers were widely used by quality enthusiasts on account of their wide frequency range, which extended to at least 12,000 c/s.

The post-war "Axiom 12" series, while bearing a superficial resemblance to the "Auditorium" range, is of entirely new design and incorporates several interesting features. The centre pole diameter has been increased from 1½ to 1⅞in and a magnet of higher energy has been fitted. The total flux is 145,000 maxwells and the density 13,000 gauss.

Increased power-handling capacity has been achieved at low frequencies by the larger magnet, and at high frequencies by reinforcement of the edge of the inner cone by a light beading. This prevents the formation of "bell-tone" modes of vibration within the normal range of volume levels. It is stated that the maximum power capacity is 12 watts peak A.C., and the frequency coverage is 40 to 15,000 c/s.



Goodmans "Axiom Twelve" loudspeaker. The coil impedance is 15 ohms at 400 c/s.

The quality of reproduction is excellent and is maintained to much higher levels than in the earlier twin-diaphragm units. With the extended frequency range it is, of course, necessary to take more than usual care to eliminate harmonic and intermodulation distortion in the preceding amplifier, but when this is done the full power of which the Axiom Twelve is capable can be enjoyed with complete satisfaction. A bass reflex cabinet measuring approximately 30in x 23in x 16in has been specially designed for this particular loudspeaker and working drawings are available.

OUR COVER

The illustration on our cover shows the control console of the television transmitter at the works of Pye Ltd., Cambridge. This console enables test transmissions to be monitored both before and after passing through the transmitter.

The makers are Goodmans Industries, Lancelot Road, Wembley, and the price is £8 8s.

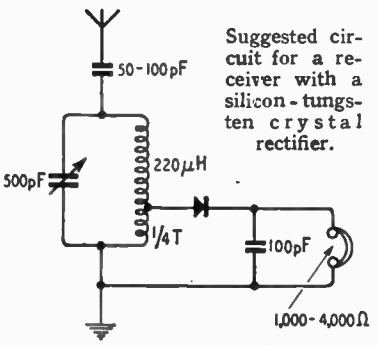
Crystal Sets—New Style

THERE seems to be a revival of interest in the crystal receiver for broadcast reception, and particularly in the adaptation of the wartime "crystal valve" to this purpose. These crystal valves, as is well known, are vastly more stable than the most "permanent" of the old-time crystal detectors; they comprise a silicon-tungsten junction sealed in a cartridge.

The British Thomson-Houston Company recommends the Type CS7A crystal rectifier. Though a series-tuned receiver circuit is best in the interests of good sensitivity and acceptable selectivity, it involves permeability tuning, and so the parallel-tuned circuit will generally be preferred for general use. A circuit arrangement suggested by B.T.-H. is shown in the diagram below.

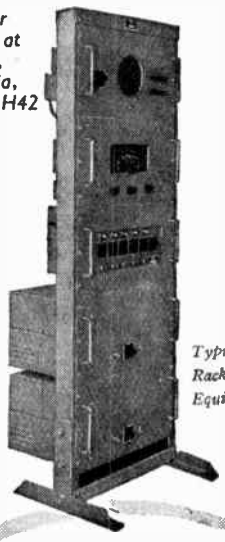
For a rectified current of about 20μA, which provides good signals with 2,000Ω phones, the impedance of the rectifier is about 10,000 ohms. With average circuit constants the rectifier output circuit should therefore be tapped down on the coil to include about one-quarter of the total number of turns, as shown.

The CS7A crystal rectifier, made by the B.T.-H. Company, Rugby, costs 7s 6d; it is obtainable from Webbs Radio, 14, Soho St., London, W.1.



Suggested circuit for a receiver with a silicon-tungsten crystal rectifier.

See our Exhibit at B.I.F., Olympia, Stand No. H42



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Random Radiations

By "DIALLIST"

Television a la Russe

IT IS MY WONT to skim through as many of the foreign wireless magazines as I can get hold of each month. In case you should start thinking "what a linguist the fellow must be," hold your horses and let me give you a tip. Do you want to gain a reputation as a linguist? Nothing easier. Take a copy of the Danish *Dansk Radio Industri*, or the Spanish *Radio y Electrotechnia* with you to the office, open it and, after some minutes of apparent absorption in its contents, remark brightly, "Jolly interesting, this Danish (or Spanish) article on pickups." If some disagreeable fellow suggests that you don't know a word of Danish, you probably won't have much difficulty in confounding him by a fluent translation of any paragraph he cares to name. With the drawings and circuit diagrams to help, it's often as easy as easy. The Danish (as well as the French and probably the Czech and the Magyar) for pickup is just pickup! Hosts of other key technical words are common to most civilized tongues and the illustrations help you to fill in many gaps. Russian is beyond my powers, but I lit a day or two ago on a French translation of an article on television from the Soviet magazine *Radio* in the *U.I.R. Bulletin*. Russia is going ahead with television in a big way. Stations at Moscow and Leningrad have been operating for some time and two others with a 25 kW power output rating for vision are to open in the near future. The present standard is the 625-line, but higher definition is contemplated with a view to big-screen displays and research. But Russia is a vast country, large areas of which are populated by folk living in widely separated small towns and villages. To attempt anything like nation-wide coverage by means of medium-power relays would entail enormous expense and huge amounts of materials. In the article in question a particularly bright idea is outlined. Calculations show that a simple aerial system 50-60 metres high should provide a field-strength of 1mV/m over an area with a radius of 5 to 10 miles, even if the transmitter is rated at only a few hundred watts. Such transmitters, it is suggested, can be put together, largely from standard components, by enthusiastic amateurs all over the country. Presumably the municipality pays for the bits and pieces, for the transmitter is handed over, when finished, to the local authorities, who run it for the common entertainment. I can't think of any better way of getting television services of some kind (the standard proposed for these amateur-built stations is 240-line, 25 frames a second) going as quickly as possible in thinly populated areas. But having set up your transmitter—and, one imagines, provided a reasonable number of receivers—what are you going to transmit? Relaying is out of the question in view of the enormous distance and one doubts whether local talent could provide more than an occasional programme. Still, the construction of local low-powered transmitters by amateurs is a novel idea with some possibilities. It might be worth thinking about in other countries as well.

Spread of the H-shaped Dipole and Reflector

AS I WRITE, the erection of television aerials, suspended willy nilly during the spell of gales, frost and snow, is proceeding apace in my locality. Springtime is here, good and proper, and just to let "Free Grid" see that I can quote Latin too when roused,

Ecce iterum gelidus canis de montibus humor Labitur

which the schoolboy translated: *ecce iterum*, lo! again; *gelidus canis*, a cool dog; *labitur*, slides; *de montibus*, down the mountains; *humor*, by way of a joke. Seriously, have you observed the rate at which television aerials are going up in and near London? I notice fresh ones nearly every time I journey to Town by train or Green Line. The little place in which I live has become very television minded. Like the inhabitants of most small towns we take the greatest interest in one another's doings. In our walks abroad we keep an eye on the chimney stacks for the appearance of new H-shaped collectors and tell one another that the Soandsos and the Thingmebobs have just installed a televisor. In fact, unless you live near enough to the Alexandra Palace to be able to use an indoor aerial, you can't help letting the world know it when you join the ranks of the televiewers. Most of those I talk to seem very satisfied not only with the entertainment but also with the size of the images provided by their 9-inch cathode-ray tubes. One good sign is that television receivers don't stay long in the windows or the showrooms of the radio shops. Actually, if there's one there at all it is usually on the point of being delivered to a customer and if you ordered one of well known make you'd probably be told that you'd be some way down on the waiting list.

News from the Clubs

Basingstoke.—A course of instruction including morse has been started for members of the Basingstoke and District Radio Society at their weekly meetings on Tuesdays at 7.45 in the Assembly Rooms, Potters Lane, Basingstoke. Sec.: L. S. Adams, 16, Bramblys Drive, Basingstoke, Hants.

Bexley.—The North Kent Radio Society now meets on Mondays at 7.30 at its new headquarters, Freemantle Hall, Bexley, Kent. Sec.: J. L. Bowes, G4MB, 20, Bloomfield Road, Bexleyheath, Kent.

Birkenhead.—Membership of the Wirral Amateur Radio Society now totals 68, of which number 25 hold transmitting licences. Meetings are held on the first and third Wednesdays of each month at the Y.M.C.A., Whetstone Lane, Birkenhead, at 7.30. Sec.: B. O'Brien, G2AMV, 26, Coombe Road, Irby, Heswall, Cheshire.

Gloucester and District Amateur Radio Society now meets on alternate Thursdays at the Spread Eagle Hotel, Market Parade, Gloucester. Next meeting on April 1st. Sec.: J. W. Dean, G2AZT, 100, Stanley Road, Gloucester.

World Radio History

Loughborough.—Membership of the Beaumanor Amateur Radio Society is limited at present, but visitors are welcome at the weekly meetings on Sundays at 6.30 at the Club's temporary headquarters, 24, Brand Hill Camp, Woodhouse Eaves, Loughborough. Sec.: E. T. Pethers, Beaumanor Park, Loughborough, Leicestershire.

Newcastle-on-Tyne.—Meetings of the North-East Amateur Transmitting Society are now held on the last Monday of each month at 8.0 at the British Legion Rooms, 1, Jesmond Road, Newcastle-on-Tyne. Sec.: J. W. Hogarth, G3ACK, 4, Fenwick Avenue, Blyth, Northumberland.

Peterborough.—The annual general meeting of the Peterborough and District Radio and Scientific Society will be held on April 1st in the Technical School, Broadway, Peterborough. Weekly meetings are held on Thursdays. Sec.: R. S. Snell, 15, Buckle Street, Peterborough.

Sidcup.—Membership of the Cray Valley Radio Transmitting Club is limited to holders of G.P.O. transmitting licences. Meetings are held on the third Thursday of each month at the Adult Education Centre, Lamorbey Park, Halfway Street, Sidcup, Kent. Sec.: G. Miles, G2CXO, "Cotswold," Mottingham Lane, London, S.E.9.

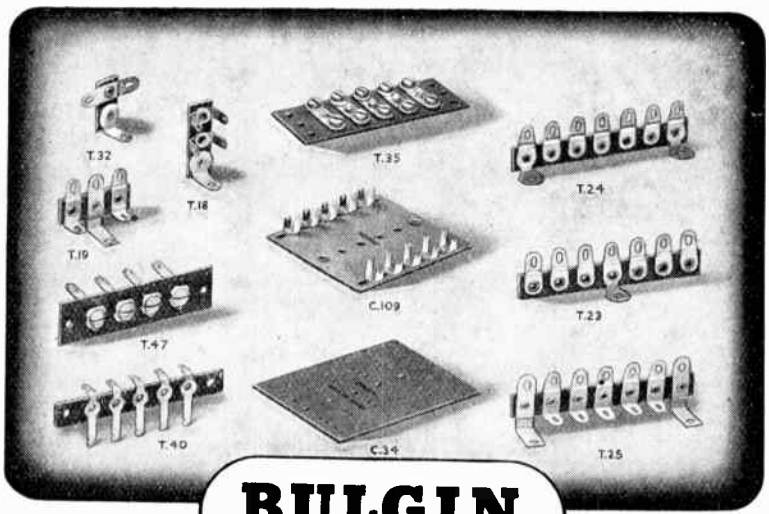
Southend.—The Southend and District Radio Society now meets on alternate Fridays at 7.45 at the Art School, Victoria Circus, Southend. A series of lectures covering the syllabus for the Radio Amateurs' Examination is being given. The next meeting is on April 9th. Sec.: J. H. Barrance, M.B.E., G3BUJ, 49, Swanage Road, Southend-on-Sea, Essex.

Warrington.—Fortnightly meetings of the Warrington Radio Society, previously known as the Warrington and District Radio Society, are held on Mondays at 7.30 at the Junior Technical School, Arpley Street, Warrington. Sec.: J. F. Thomas, 510, Stockport Road, Thelwall, nr. Warrington, Lancs.

West Cornwall.—Meetings of the West Cornwall Radio Club are held each month in three centres. On the first Thursday at the Railway Hotel, Penzance; on the second and fourth Thursdays at the Railway Inn, Redruth, and on the third Thursday at the "Fifteen Balls" Inn, Penryn. All meetings begin at 7.30. A link between the three sections is maintained in the 3.5-Mc/s band one night a week. Sec.: R. V. A. Allbright, G2JL, Greenacre, Lidden, Penzance, Cornwall.

Wolverhampton.—An amateur radio exhibition is being organized by the Wolverhampton Amateur Radio Society and will be held from April 5th to 10th in the Co-operative Society Hall in Stafford Street. The event is being arranged in connection with the town's centenary celebrations. Sec.: H. Porter, 221, Park Lane, Fallings Park, Wolverhampton, Staffs.

Worthing.—At the meeting of the Worthing Group of the R.S.G.B. on April 1st at 7.30 at Oliver's Café, 32, Southfarm Road, Worthing, a representative of the Mullard Educational Service will give a lecture on "An Introduction to Electronics—the Radio Valve." Sec.: G. W. Morton, 42, Southfarm Road, Worthing, Sussex.



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RECENT INVENTIONS

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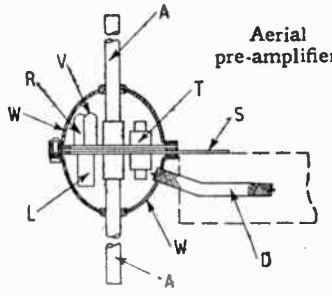
MINIMIZING INTERFERENCE

IN short-wave reception, the down-lead from an elevated dipole to the set is responsible for most of the interference experienced. By amplifying the signal voltage actually developed across the aerial, before feeding it into the down-lead, a better signal-to-interference ratio can be applied to the main receiver.

As shown in the diagram, a small amplifying unit is enclosed in a waterproof casing W, which is mounted at the centre of the dipole A on the supporting bracket S. The unit consists



Aerial pre-amplifier.

of an amplifier valve V, with tuning coil L, and a mains transformer T feeding a rectifier R. Power is fed to the transformer through the inner and outer conductors of the screened down-lead D. The inner conductor also carries the amplified signal, which passes through isolating condensers to protect both the aerial unit and the main receiver from the supply voltage.

D. Jackson and Pye, Ltd. Application date September 9th, 1944. No. 587627.

RELAYING SYSTEMS

WHEN transmitting television or other signals covering a wide frequency band from point to point over a series of relay stations, serious departure from linearity is likely to arise unless the relay circuits are carefully designed and supervised. But as such stations are usually unmanned, and carried on high masts, it is highly desirable that they should be as simple in character and operation as possible.

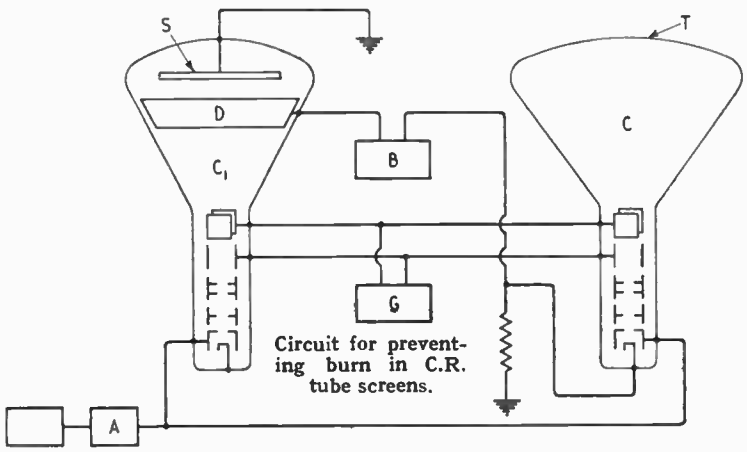
According to the invention, this is accomplished by the alternate use of positive and negative modulation. In other words, the incoming signals at one relay station are rectified and passed through a phase-inverter before being applied to modulate the outgoing carrier wave from that station. In television, for instance, the synchronizing signals are re-radiated at maximum amplitude, whilst for high-light signals the reverse holds good. The successive changes in polarity serve automatically to check the normal progressive error in linearity. It also prevents "crossfire" between the transmitter and receiver at each relay, since any feedback will be negative.

The General Electric Co., Ltd., and D. C. Espley. Application date November 6th, 1944. No. 587498.

RADAR DISPLAYS

PERSISTENT echo signals from the ground, or from a relatively fixed object, are liable to burn or damage the sensitive screen of the cathode-ray indicator. Moreover, such images serve little useful purpose, except possibly after each change of view or alteration in range.

According to the invention, an auxiliary tube C1 is used in parallel with the indicator tube C, the control grids of both tubes being fed from the signal amplifier A, whilst their deflecting plates receive identical scanning voltages from a generator G. The tube C1 is fitted with a mosaic screen S of known type, together with a signal-collecting anode D, whilst the indicator tube has a sensitive dark trace



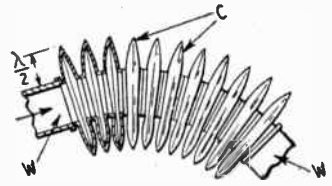
Circuit for preventing burn in C.R. tube screens.

screen T. After the first few scanning cycles, the charges created by the fixed traces on the mosaic screen S will be sufficient to induce signals on the anode D. These are applied through an amplifier B, in the same phase, to the cathode of the indicator tube, where they can be used either to eliminate or reduce the intensity of the same signals on the screen T.

Standard Telephones & Cables, Ltd. (assignees of R. E. Rutherford). Convention date (U.S.A.) December 20th, 1943. No. 588155.

WAVE GUIDES

THE energy transmitted by a wave guide will not normally pass through a bend in the guide without



Flexible wave guide joint.

attenuation. Some reflection occurs whenever the waves come to a section of the guide that is out of alignment with the main axis, and this interferes with the steady flow of power.

It is now common practice in radar to use a wave guide for feeding centimetre waves to the rotating aerial scanner. The diagram shows a construction suitable for this purpose, since it allows the guide to be flexed in any direction without interfering with the efficiency of transmission. The concertina-like elements C consist of a series of resilient discs, each having a central aperture equal to the diameter of the wave guide W, so that they form a continuation of it. The discs are soldered together in pairs along their outer edges, which extend beyond the periphery of the central channel for a distance equal to half the transmitted wavelength. They therefore act as an impenetrable series of high-impedance "chokes," and maintain a constant flow of energy through the central channel.

The British Thomson-Houston Co., Ltd. Convention date (U.S.A.) August 30th, 1943. No. 586458.

The British abstracts published here are prepared with the permission of the Controller of H.M. Stationery Office, from specifications obtainable at the Patent Office, 25, Southampton Buildings, London, W.C.2, price 1/- each.

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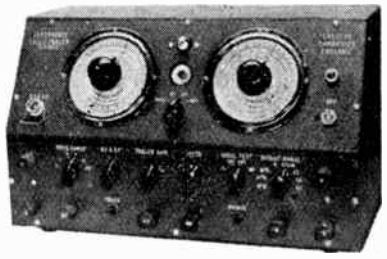

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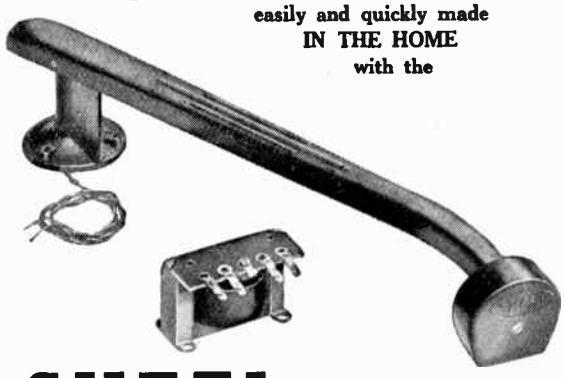

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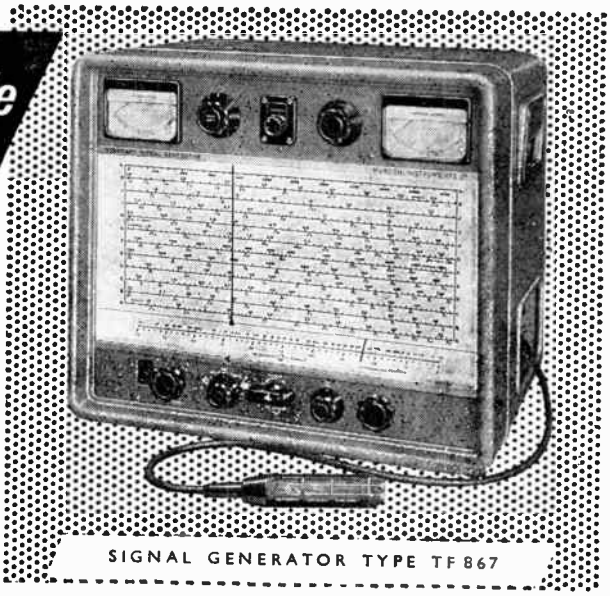

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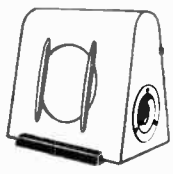

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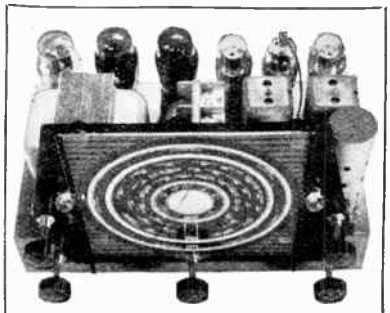

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FRITH RADIOCRAFT, Ltd., 69-71, Church Gate, Leicester. Tel. 58927. [9572

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W.W. television coil formers feet and slugs, 7/6 for 9; 1-1 trans. for frame T.B., 3/6; 100 ma 15h chokes, cast case, 8/-; speakers, 10in P.M., 37/6; 8in P.M., 19/6; 5in P.M., 15/-; 5in 750a field+O.P. trans., 25/-; valves 6A7, new, 14/-; postage extra under £1.—Taylor, 24, Enmore Rd., Putney, S.W.15. [9392

COPPER wires, enamelled, tinned, Litz, cotton, silk covered, all gauges; B.A. screws, nuts, washers, soldering tags, eyelets; ebonite and laminated bakelite panels, tubes, coil formers; Tufnol rod; headphones, flexes, etc.; list s.a.e; trade supplied.—Post Radio Supplies, 33, Bourne Gardens, London, E.4.

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THE LONDON TELEVISION Co., Ltd., 694, Lea Bridge Rd., London, E.10. [9425

GEE ELECTRIC, 15, Little Newport St., London, W.C.2. Tel. Ger. 6794.—Variable condensers ceramic insulated, single gang 0.0005, 2/6, 2-gang ditto 7/6, 3-gang ditto 8/6, 4-gang ditto 9/-; all standard ¼in spindle; 0.001 5 kVw condensers, 1/6; 0.5 HFD 2.500 VW condensers, 5/-; Varley P/P input heavy duty transformers, ratio 2.5:1+2.5:1, 12/6; G.P.O. type sockets, 3-way, all metal, 10/6 doz.; new 230v 50 cycle mains transformers, 280-0-280, 120 m/a, 5v 3 amp, 6.3v 7 amp, with fixing feet, 38/6; good quality s/screened wire, 9d yd; T/screened, 1/- yd; and 5-core 1/- yd, 7-core 1/3 yd, as previous advert.; also very large and comprehensive range of all types of new valves in stock; special prices quoted for large quantities to the trade. [9381

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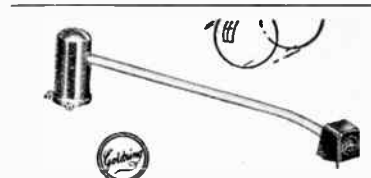
MATT RADIO SERVICE, 29, Castle St., Kingston-on-Thames, Surrey. Kingston 8353. [9545



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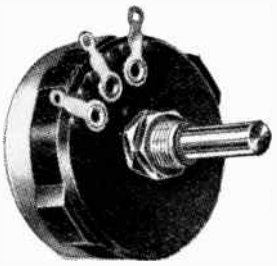

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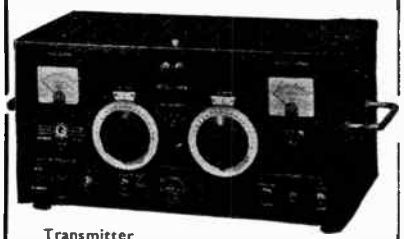

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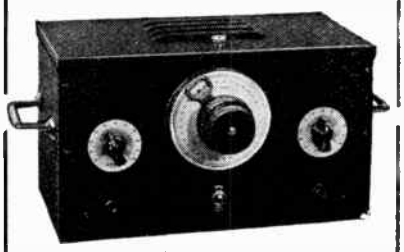

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RADIO CLEARANCE, Ltd., 27, Tottenham Court Rd., London, W.1.—10-valve s.w. reg. R.1481, range 65-86 m/cs, R.F. (VR65), Osc. (VR66), mixer (VR65), 3 I.F.s (VR53), det. and A.V.C. (EB34), A.F. (VR57), output (VR67), 6in s.m. dial, B.F.O., tuning meter, R.F. and L.F. gain controls, requires P.P. 250v h.t., 6.3v l.t., all brand new, in wooden transit cases, as our previous lot, and we are now able to offer these sets, which lend themselves readily to modification for 5 mtes., F.M., etc., at £7/19/6; circuit diagram supplied with each receiver, carriage paid; power packs, type 3, these are for the above sets, 19in rack fitting, input adjustable by switch, 200-250v a.c., 50 c/s, with volt and milliammeters, we have a few available for sale only with sets at £2/19/6; R.F. units, type 24 and 25, these units have 3 valves (VR65s), R.F., mixer, osc., and 5-position ceramic switch (3-bank), giving 5 freqs. approx. between 35-55 m/cs (type 24 slightly lower), I.F. output 7.3 m/cs, make useful converters, supplied complete with valves, 17/6, post paid; meters, all moving coil, 0-1 ma, 2in square, 7/6; 0-10 ma, 2in square, 7/6; 0-30ma, 2½in circular, 7/6; 0-50ma, 2in square, 6/-; 0-150ma, 2in square, 8/6; 0-500 micro amp, 2½in circular, 19/6; 0.3a R.F. ammeters, 2in square, 6/-; all these are flush mounting; 0-750 micro amp, 2½in circular, plug-in, calibrated for use with thermo couple as radiation meter, 7/6; Mansbridge condensers, 0.1, 5,000v (6½in×3½in×2½in), 5/6; 4mf, 1,000v, 4/6; 10mf, 500v, 5/6; 1mf, 1,000v, 1/-; 2mf, 300v, 10d; 0.25mf, 2,000v, 1/9; 0.5mf, 1,200v, 1/-; all wkg voltages; smoothing chokes, 5h, 200ma, res 90Ω, 8/-. [9665

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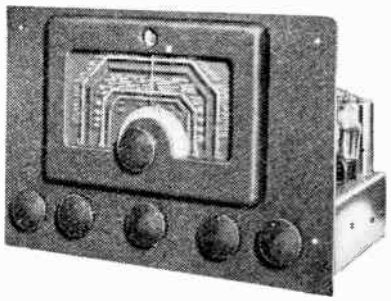

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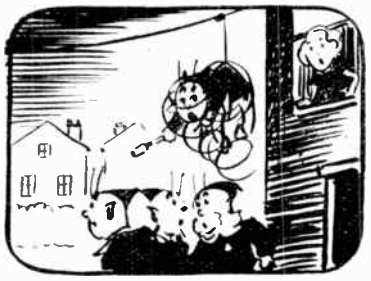

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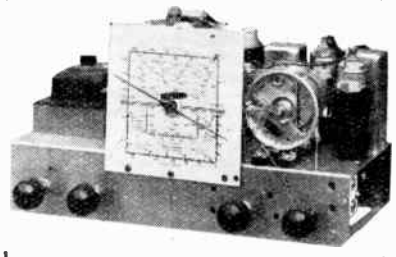

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ASSISTANT physicist, preferably with some electronic knowledge, required for work on waveguide systems; mathematical and academic qualifications essential, practical experience and mechanical ability an advantage, age 20 to 30; salary £350 to £450 per annum.—Write Box N5864, A.K. Advg., 212a, Shaftesbury Av., W.C.2.

SUPERINTENDENT required to take charge of radar and radio assembly dept. electronic equipment company, Manchester area; must be familiar with A.I.D. requirements and capable of controlling labour on track and bench assembly.—Reply, giving full particulars of age, experience, qualifications and salary required, to Box 6259. [9477

DRAUGHTSMAN with some experience in light electrical engineering is required for work on prototype equipment in connection with television transmitters.—Apply by letter only to the Director, Research Laboratories of the General Electric Co., Ltd., North Wembley, Middx., stating age, experience and academic qualifications. [9605

ENGINEERS required for employment on development of Radar, communication and electronic equipment; applicants must possess a degree in engineering or its equivalent; salary £400 to £600 per annum according to qualifications.—Reply, stating age, experience, training and qualifications, etc., to Cossor Radar, Ltd., Wren Mill, Chadderton, Nr. Oldham, Lancs.

RADIO manufacturers, West London district, have vacancies for senior development engineers and laboratory assistants for work on design and development of telecommunication equipment and broadcast receivers; for the senior posts, at least 5 years' practical experience in this class of work is essential.—Write, stating age, qualifications, experience and salary required, to Box 6268. [9504

PHILIPS ELECTRICAL, Ltd., require engineers in the Birmingham and Manchester area to deal with public address equipment and installations; a good standard of technical knowledge and commercial experience in public address or other allied trade is essential; successful applicants must be prepared to reside in London for several months for preliminary training, and possession of a car is essential; write, giving full details as to age, previous experience and salary required, to: Box 5522. [9213

E.M.I. ENGINEERING DEVELOPMENT, Ltd., Hayes, Middlesex, invite applications from junior and intermediate engineers, age 25 to 30, with engineering degree or the equivalent, and practical design experience; specific vacancies on radar development include the following work. (a) design of 30-100 Mc I.F. amplifiers. (b) transformers for higher frequency power supply. (c) special problems on radar presentation; there are several other interesting vacancies for physicists and engineers; inclusive salary £400 to £550, according to age and qualific.—Write, giving full details and interests, to Personnel Dept.

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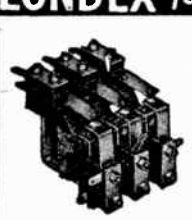

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MARCONI/OSRAM.—U10, U14, U16, U17, U18/20, U30, U32, U31, U74, U76, VMP4G, MS4B, MSP4- 5- and 7-pin, D41, MHD4, ML4, MKT4, 5- and 7-pin, KT41, DA30, VMS4B, H30, X65, KTW63, KTZ63, KTW61, H63, L63, DL63, KT44, KT66, KT61, Y63, KT71, X61M, KT74, KT76, KT33C, W21, Z21, HD24, LP2, KT2, P2, QP21, Z22, Z62, Z66, GT1C, GU50,

MAZDA.—UU6, V914, ACP, ACPen, 5- and 7-pin HL41DD, 8P41, VP41, P41, DD41, HL42DD, TH2321, Pen3520, VP133, Pen383, Pen453DD, HL133DD, HL21DD, QP230, TP22, TP25, TP26, Pen225, QP25, DD207, HL23, HL23DD, VP23, D1, CCH35, DAF91, DF51, DF91, DK91, EA50, EB34, EBC3, EBC33, ECC31, ECC32, ECC34, ECH33, ECH35, EF9, EF36, EF39, EK32, EL2, EL32, EL33, EL35, EL37.

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.05	500	350	1⅛	⅜	CP45S	2/1d.
.1	350	200	1⅛	⅜	CP45N	2/1d.
.1	500	350	2¼	⅜	CP46S	2/2d.
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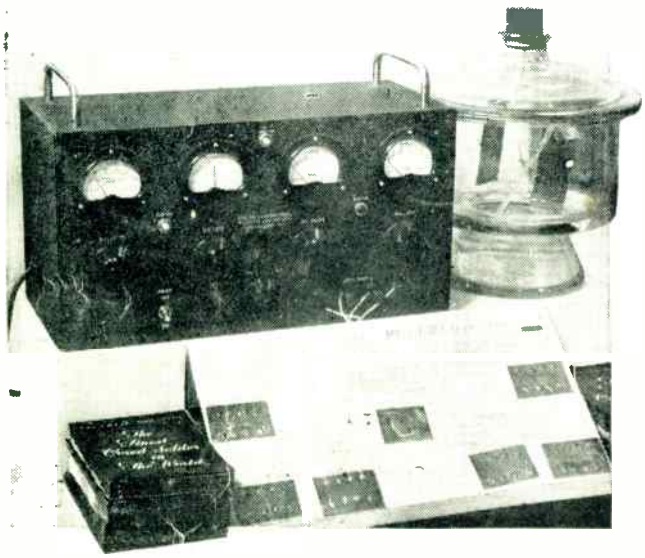

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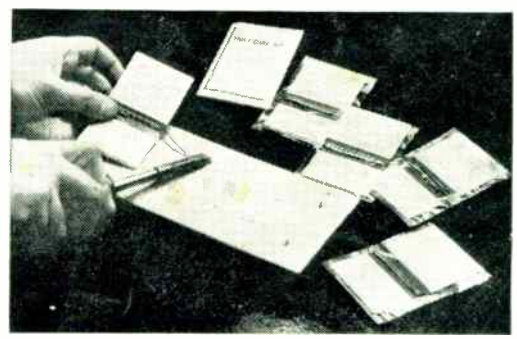

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